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Nanomatériaux pour les Systèmes Sous Sollicitations Extrêmes
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**Toward Particle Size Reduction by
Spray Flash Evaporation
the case of organic energetic crystals and
cocrystals**

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«Qui a dit que la science désenchant le monde ? Assurément un ignorant, car toutes les peurs se nourrissent de l'ignorance et des ignorances entretenues.»

Pascal Pic, *Darwin et l'évolution expliqués à nos petits-enfants* (2009).

“SCIENCE: A way of finding things out and then making them work. Science explains what is happening around us the whole time. So does RELIGION, but science is better because it comes up with more understandable excuses when it is wrong.”

Terry Pratchett, *Wings* (1990, 2007), 147.

since we are living in a so-called modern age where PR and economic interests seems to have won against science.

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Extended Abstract

The development of nano-technology took off with the invention of the Scanning Tunneling Microscopy (STM) and the Atomic Force Microscopy (AFM) in the early 80's at the IBM Zurich Research Laboratory (Binnig et al. 1986, 1983, 1982). By providing accurate and advanced characterizations on nanoparticles, those two crucial microscopy techniques allowed a control of the physicochemical properties of materials down to the atomic scale. Since then, the outstanding properties of new nano-materials led the research in energetic material to embrace this trend. The nano-structuration of classical explosives, such as 2,4,6-trinitrotoluene (TNT) or 1,3,5-trinitroperhydro-1,3,5-triazine (RDX), can enhance their safety but also their reactive properties (critical diameter, tunable detonation velocity etc.).

Organic energetic materials release their intrinsic energy under an external stimulus such as a strong mechanical impulse, a great heat or an electrostatic discharge. This initiation is facilitated by the formation of hot-spots coming from the presence of impurities, open pores, entrapped gases or other inhomogeneities within the explosive matrix. Therefore, void free crystals have been an extensive research subject, but the mastering of crystallisation can be enhanced by the formation of particles smaller than the critical size of a hot spot. Moreover, achieving a controlled crystallisation enables further tailoring of the nanoparticles and thus of the physicochemical properties.

The continuous formation of nanosized energetic material is a long-standing challenge. From wet productions methods to dry crystallisation processes, Spray Flash Evaporation (SFE) is a major technique for continuously producing energetic materials at submicron or nano scale. It relies on the superheating of a solvent sprayed into vacuum and thus flashing. The versatility of the SFE internally developed (Doctoral Thesis Risse 2012; Risse et al. 2012) and patented ("Method for producing cocrystals by means of flash evaporation" 2016; "Préparation de nanoparticules par évaporation flash" 2013) allows the continuous engineering of nano-crystals and nano-cocrystals for oxides (Klaumünzer et al. 2015), medical and energetic applications (Spitzer et al. 2014).

This present research project aims to understand and control the crystallisation occurring in the SFE process, in order to reduce further the particle size of energetic crystals. 1,3,5-trinitroperhydro-1,3,5-triazine (RDX) is chosen as a reference material for its wide use for civilian and military applications. Cocrystals -two or more molecules that form a unique crystalline structure- are also relevant in energetic materials in order to decrease the sensitivity

without losing reactivity; for instance a low sensitive compound could be cocrystallised with another one having a high sensitivity and a high reactivity. Therefore, the cocrystal CL-20:HMX 2:1 was studied as proof-of-concept but also to overcome the limited *in situ* characterizations. Crystallisation depends on the supersaturation; in SFE, the supersaturation is a function of time and space as it is linked to the size distribution and velocity of droplets. Since those measurement was first out of reach, supersaturation was raised with an anti-solvent and the enhancement of the SFE with a dual nozzle system. Later, a Phase Doppler Analysis (PDA) was used to elucidate the question of supersaturation.

Another route to control the crystallisation is the addition of chemical agent. PolyVinylPyrrolidone (PVP) and PolyEthylene Glycol (PEG) were used to alter the two steps of the crystallisation, namely the nucleation and the growth. PEG 400 triggers the early nucleation of RDX with low nucleation rate leading to bigger particles up to 5 μm . PVP 40K acts as a nucleation and growth inhibitor, forming RDX spherical particles with a mean size of 160 nm. Additionally, the synthesized RDX samples were less sensitive, especially toward electrostatic discharge.

During this work, many standard analytical methods have been found to be impossible or difficult to apply on energetic material, due to their sensitivity toward heat, or toward vacuum, or their organic nature; the nano scale and so the high specific surface area worsen those phenomena. The relevancy of the sensitivity tests is also questionable when reaching the nano scale.

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Contents

Bibliography	5
Contents	7
Résumé étendu français	11
Bibliographie	29
1 Explosives and Characterization	31
1.1 Overview	31
1.2 Organic Secondary Explosives	32
1.2.1 1,3,5-trinitroperhydro-1,3,5-triazine (RDX)	32
1.2.2 Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)	34
1.2.3 2,4,6,8,10,12-hexanitro-2,4,6,8,10,12-hexaazaisowurtzitane (CL-20)	35
1.2.4 Cocrystal CL-20:HMX 2:1	36
1.3 Analytical Methods	36
1.3.1 Classic Material Characterization Methods	36
1.3.2 Explosive Specific Characterization Techniques	42
1.4 Submicron and nano explosives	45
1.4.1 Properties and Challenges	46
1.4.2 Challenges of the characterization of energetic materials	49
1.4.3 Specific health and safety hazards	53
1.5 Summary of the Chapter	55
Bibliography	57
2 Production of Nano Explosives	61
2.1 Wet production methods	61
2.1.1 Crystallisation from solution	61
2.1.2 Solvent substitution using reverse micelles	63
2.1.3 Sol-Gel	63

2.1.4	Melting	64
2.1.5	Milling	65
2.2	Dry production methods	66
2.2.1	Physical Vapor Deposition (PVD)	66
2.2.2	Electrospray	66
2.2.3	Plasma	67
2.2.4	Supercritical/Gas Anti-Solvent precipitation	68
2.2.5	Aerosol Solvent Extraction System (ASES) process	68
2.2.6	Solution Enhanced Dispersion by Supercritical fluids (SEDS)	68
2.2.7	Particles from Gas-Saturated Solutions (PGSS)	69
2.2.8	Rapid Expansion of Supercritical Solutions (RESS)	69
2.2.9	RESS-AS (or RESOLV)	70
2.2.10	Light Amplification by Stimulated Emission of Radiation (LASER) Ablation	70
2.2.11	Ultrasonic Spray Pyrolysis	70
2.2.12	Spray Drying	71
2.2.13	Spray Flash Evaporation (SFE)	71
2.3	Discussion on production methods	72
2.4	The Spray Flash Evaporation Technique	75
2.4.1	Theoretical Insights on the SFE technology	75
2.4.2	Comprehensive description of SFE	78
2.4.3	Versatility of the SFE	79
2.5	Scientific goals of the thesis	81
2.5.1	Particle Size Reduction	81
2.5.2	SFE understanding	82
2.6	Summary of the Chapter	82
	Bibliography	85
3	Particle Size and Shape	95
3.1	Size Measurement	95
3.1.1	Sensitivity of nano-organic energetic particles	95
3.1.2	AFM	96
3.1.2.1	Methodology	96
3.1.2.2	Effect of the concentration on the particle size	98
3.1.2.3	Reliability and accuracy	103
3.1.2.4	Conclusion on the AFM pellet method	107
3.2	One Technique, One Size	111
3.2.1	XDR	111
3.2.1.1	Determination of the apparent volume weighted domain size	111

3.2.1.2	Rietveld refinement	112
3.2.2	Smallest observable object	117
3.3	Summary of the Chapter	119
Bibliography		121
4	Crystallisation study and comprehension of the SFE process	123
4.1	Crystallisation, Nucleation and supersaturation	123
4.1.1	Increasing Supersaturation in SFE with an Anti-solvent . .	126
4.1.2	Supersaturation Determination	130
4.2	CL-20:HMX 2:1 Cocrystal as a Tool for Understanding Crystalli- sation by SFE	134
4.2.1	Cocrystallisation	134
4.2.2	CL-20:HMX 2:1 Cocrystallisation from SFE	137
4.3	Summary of the Chapter	141
Bibliography		143
5	Tunable Particle Size	147
5.1	Material & Methods	148
5.2	Results & Discussion	149
5.2.1	Quantification by Nuclear Magnetic Resonance (NMR) Spectroscopy	149
5.2.2	RDX processed with PEG 400	152
5.2.2.1	Particle Size and Morphology	152
5.2.2.2	X-Ray Diffraction (XRD)	153
5.2.2.3	Thermal Analysis	156
5.2.2.4	Infrared (IR) Spectroscopy	157
5.2.3	RDX processed with PVP 40K	157
5.2.3.1	Particle Size and Morphology	157
5.2.3.2	Thermal Analysis	160
5.2.3.3	IR Spectroscopy	161
5.2.4	Sensitivity	162
5.2.5	Comparison with mechanically mixed samples	164
5.3	Summary of the Chapter	164
Bibliography		167
Related Work		169
SFE innovations		169
Published Work		170

Conclusion	173
Bibliography	177
Appendices	178
A Rietveld refinement	179
A.1 Calibration	179
A.2 Sample of n-RDX processed pure at 2 wt% in acetone	206
A.3 Sample of n-RDX processed pure at 3 wt% in acetone	229
A.4 Sample of n-RDX processed with 0.1 wt% of PEG	239
A.5 Sample of n-RDX processed with 10 wt% of PVP	254
A.6 Sample of n-RDX with 1 wt% of PVP through a 80 micron nozzle .	265
Glossary	277
List of Figures	280
List of Tables	284

Résumé étendu français

Réduction de la taille des particules par Spray Flash Evaporation : le cas des cristaux et cocristaux organiques énergétiques.

Le développement des nanotechnologies a réellement décollé avec l'invention des microscopies par effet tunnel (STM) et à force atomique (AFM), au début des années 80 à l'Institut de Recherche IBM de Zurich (BINNIG et al. 1986, 1983, 1982). Ces deux techniques permettent l'analyse directe de nanostructures jusqu'à l'échelle atomique, et sont donc devenues indispensables pour contrôler finement les propriétés physicochimiques des matériaux. Depuis quelques décennies, les nouveaux nanomatériaux ont pris leur essor dans notre société grâce à des propriétés remarquables pour de nombreuses applications, et aux coûts de production maîtrisés. Le développement des nanotechnologies a aussi permis la création et l'amélioration de technologies connexes. Contrairement à la révolution numérique, les secteurs scientifique et industriel des matériaux énergétiques sont restés bien longtemps en marge de cette vague technologique, et ne s'engagent que depuis peu dans l'exploration des propriétés de nanostructures énergétiques. Parmi les attentes, la nanostructuration d'explosifs classiques comme le 2,4,6-trinitrotoluène (TNT) ou le 1,3,5-trinitroperhydro-1,3,5-triazine (RDX) peut améliorer leur sensibilité et donc faciliter leur manipulation, mais aussi nombre de leurs propriétés réactives (diamètre critique, vitesse de détonation, homogénéité...).

Les explosifs étudiés ici sont les matériaux énergétiques organiques ; ils libèrent leur énergie intrinsèque suite à un stimulus tel qu'une sollicitation mécanique importante, une forte chaleur ou une décharge électrostatique. Cette initiation est facilitée par la formation de points chauds, hot-spot, qui proviennent d'impuretés, de cavités et autres défauts dans la matrice cristalline. Ainsi, la production de cristaux à haute pureté et haute cristallinité fut un champ de recherche privilégié pendant des décennies, mais la maîtrise de la cristallisation peut être poussée encore plus loin par la formation de particules plus petites

que la taille critique d'un point chaud. De plus, atteindre une cristallisation contrôlée permet de façonner avec précision les nanoparticules et donc d'ajuster leurs propriétés physicochimiques.

L'étude des nanomatériaux énergétiques organiques commence par leur formation ; le retard pris par la communauté pyrotechnique en nanotechnologie s'explique en partie par la difficulté de produire des nanoparticules d'explosifs. Ainsi la cristallisation en continu de matériaux énergétiques à une échelle au moins submicronique est un défi de longue date. Parmi les méthodes de production de la voie humide à la voie sèche, le procédé Spray Flash Evaporation (SFE) est une technique émergente majeure pour la production continue d'explosifs nanométriques ou de compositions énergétiques nanostructurées. Cette méthode se base sur la surchauffe d'un solvant pulvérisé dans un vide primaire/moyen, provoquant alors une évaporation quasi instantanée, flash. La polyvalence du SFE, développé en interne (Thèse de Doctorat RISSÉ 2012) et breveté ("Method for producing cocrystals by means of flash evaporation" 2016 ; "Préparation de nanoparticules par évaporation flash" 2013), permet la formation d'oxydes (KLAUMÜNZER et al. 2015) ainsi que de nanocristaux et co-cristaux pour des applications énergétiques et médicales (SPITZER et al. 2014).

Le présent projet de recherche vise à comprendre et contrôler la cristallisation au sein du procédé SFE, afin de réduire la taille des cristaux énergétiques. Le 1,3,5-trinitroperhydro-1,3,5-triazine (RDX) a été choisi comme matériau énergétique de référence du fait de son utilisation large pour des applications civiles et militaires. La cristallisation dépend du degré de sursaturation ; dans le SFE, la sursaturation est fonction du temps et de l'espace car liée à la distribution en taille des gouttes et à leur vitesse. La caractérisation *in situ* des gouttes requiert l'utilisation de techniques avancées d'interférométrie optique acquises à la fin du projet. Pour palier cette absence, la sursaturation a été augmentée par l'ajout d'un anti-solvant et la mise en place d'un système d'injection à double buses. Finalement, un appareil d'interférométrie optique, Phase Doppler Analysis (PDA), est utilisé pour déterminer les tailles et vitesses des gouttes.

Pour déterminer la persistance des gouttes, le co-cristal CL-20:HMX 2:1 sera employé avec le système d'injection à double buses. L'utilisation de co-cristaux (deux molécules ou plus dans un même réseau cristallin unique) pour étudier la cristallisation au sein du SFE est d'autant plus pertinente que la formation de co-cristaux énergétiques est une autre stratégie actuellement explorée pour réduire la sensibilité de l'explosif sans sacrifier sa réactivité.

La cristallisation au sein du SFE peut aussi être maîtrisée par l'ajout d'agents polymériques. Le PolyVinylPyrrolidone (PVP) et le PolyEthylene Glycol (PEG) ont été employés pour modifier les conditions de cristallisation donc les étapes de nucléation et de croissance. Le PEG 400 provoque la nucléation anticipée du RDX

amenant à la formation de particules de 500 nm à 5 μ m. La PVP 40k s'adsorbe en surface et agit comme agent inhibiteur de nucléation et de croissance : le RDX cristallise en nanoparticules sphériques avec une taille moyenne de 160 nm. Les échantillons de RDX synthétisés ainsi sont également moins sensibles, tout spécialement à la décharge électrostatique.

Lors de ce travail de recherche, de nombreuses méthodes de caractérisation ont été testées et bien peu se sont avérées être applicables de manière fiable sur les nanomatériaux énergétiques. En effet, ces derniers –des cristaux moléculaires– sont sensibles à la chaleur et au vide ; cette sensibilité est encore exacerbée pour les nanomatériaux du fait de leur grande surface spécifique. De plus, la pertinence des tests de sensibilité à cette échelle est critiquable.

Cristaux et cocristaux organiques énergétiques

Les matériaux énergétiques regroupent tous types de matériaux (composite, polymère, organiques...) qui peuvent libérer rapidement de l'énergie par une violente réaction d'oxydo-réduction. Un stimulus externe comme un choc, un frottement ou une décharge électrostatique peut initier localement la réaction de décomposition ; cette dernière se propage à travers le matériau via le front de réaction. La vitesse de ce front de réaction dépend du matériau et du mode de décomposition.

On distingue trois modes de décomposition : la combustion (mm/s - m/s), la déflagration (m/s - km/s) et la détonation (> km/s). La combustion requiert un apport extérieur d'oxygène alors que la déflagration est auto-entretenu. Lors d'une détonation, la réaction se propage par une onde de choc supersonique. Par la suite, on peut classer les matériaux énergétiques selon leur mode normal de décomposition et leurs autres propriétés pyrotechniques. Les poudres propulsives brûlent de manière contrôlée avec une importante génération de gaz afin de produire la poussée nécessaire aux engins autopropulsés. Les explosifs détonent et sont également classés selon leurs sensibilités et puissances : les explosifs primaires, très sensibles, servent à l'initiation par onde de choc des explosifs secondaires, tels que le RDX ou le 2,4,6-trinitrotoluène (TNT). On retrouve parfois des matériaux comme le nitrate d'ammonium et le perchlorate d'ammonium classés comme explosifs tertiaires du fait de leur grande stabilité. D'un point de vue chimique, les explosifs organiques sont des cristaux moléculaires dont la cohésion est assurée par des forces faibles (Van der Waals : π stacking, liaison hydrogène ...).

Un co-cristal est un cristal comprenant plusieurs molécules électriquement neutres au sein de la même maille cristalline, avec un ratio stœchiométrique défini. La définition est toujours en débat (SUN 2013) mais les hydrates et

solvates sont généralement exclus. BOLTON et al. (2012) furent les premiers à rapporter la formation et la caractérisation du co-cristal CL-20:HMX avec un ratio molaire de 2:1.

Procédés et Intérêt de la nanocristallisation

Ces matériaux hautement explosifs peuvent être accidentellement initiés, engendrant malheureusement nombre de victimes et ce bien trop souvent comme nous le rappellent les lettres de l'Inspecteur de l'armement pour les Poudres et Explosifs. Outre cet aspect, la désensibilisation du matériaux entraîne fréquemment des traitements supplémentaires (enrobage, mises en forme...) voire une perte de performances. Des inclusions, des défauts cristallins ou un habitus cristallin trop rugueux sont différents paramètres physico-chimiques pouvant fragiliser et sensibiliser le matériau; une cristallisation contrôlée à une échelle nanométrique permet d'éviter ce type de défauts micrométriques et de réduire le nombre d'étapes aboutissant au produit fini.

De nombreux procédés de recristallisation existent et ont été appliqués aux matériaux organiques énergétiques. Les méthodes par voie liquide permettent d'atteindre des tailles nanométriques et des morphologies contrôlées, deux caractéristiques intéressantes qui sont par la suite perdues lors du séchage : les processus de séchage les plus performants tels que le séchage supercritique réduisent la dégradation des cristaux mais fonctionnent par lot et non en continu. Les méthodes en voie sèche les plus abouties actuellement sont le Spray drying (BROADHEAD et al. 1992; STEIN 1973) et le Rapid Expansion of Supercritical Solutions (RESS) (KRUKONIS 1984; MATSON et al. 1987a,b) : le premier fonctionne en continu mais ne permet pas d'atteindre l'échelle nano ni le submicron, alors que le second permet d'atteindre de telles tailles mais opère séquentiellement. De plus le RESS est un procédé industriel coûteux du fait de l'utilisation de fluides supercritiques (faible solubilité, pression importante) rarement utilisés dans l'industrie (SHETH et al. 2012).

Le procédé Spray Flash Evaporation (SFE) permet la production en continu et en voie sèche de particules nanométriques ou submicrométriques ou de composites nanostructurés. Il se situe entre le RESS et le Spray drying en terme de pression et de température. Inventé (Doctoral Thesis RISSE 2012; RISSE et al. 2012) et breveté ("Method for producing cocrystals by means of flash evaporation" 2016; "Préparation de nanoparticules par évaporation flash" 2013) au sein du laboratoire NS3E, le SFE a été précédemment optimisé grâce à la thèse de RISSE (2012); cependant seuls cinq paramètres ont été étudiés, chacun dans une certaine mesure. Il apparaît nécessaire qu'afin de contrôler et de réduire encore la taille des particules cristallisées par SFE, une bonne compréhension

de la cristallisation au sein du SFE doit être acquise soit directement par une métrologie en ligne, soit par des variations induites dans la cristallisation.

Spray Flash Evaporation : principe et cristallisation

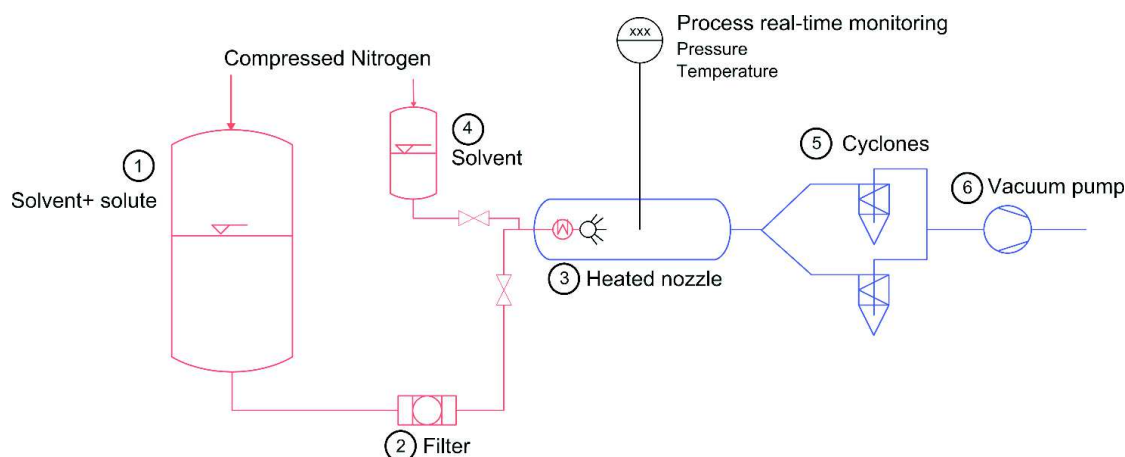


FIGURE 0.1 – Schéma du procédé de Spray Flash Evaporation (SFE)

Le procédé SFE consiste à pressuriser et surchauffer un solvant contenant un ou plusieurs composés organiques dissous, puis à pulvériser cette solution dans une enceinte sous vide. Le SFE repose alors sur le principe thermodynamique de flash évaporation : lorsqu'un liquide possède une énergie interne importante (ici d'origine thermique) et est soumis à un déséquilibre thermodynamique important (notamment lorsque la température du liquide est bien supérieure à sa température d'ébullition une fois sous vide), cette énergie est convertie en chaleur latente. Les gouttes se désintègrent et s'évaporent quasi instantanément.

La cristallisation est gouvernée par le degré de sursaturation dans chaque gouttelette ; la conjonction de nombreux phénomènes thermodynamiques mène à une taille nanométrique. La fission des gouttelettes diminue le volume de chaque réacteur, le niveau de surchauffe du liquide influence la solubilité du(des) composé(s) dans le solvant mais aussi la méta-stabilité des gouttes avant le flash... A cela s'ajoute une composante temporelle essentielle où on peut distinguer deux plans d'évolution en fonction du temps : le moment de l'évaporation flash avec le taux d'évaporation d'un côté, et de l'autre le début de la nucléation primaire avec le taux de nucléation (Figure 0.2).

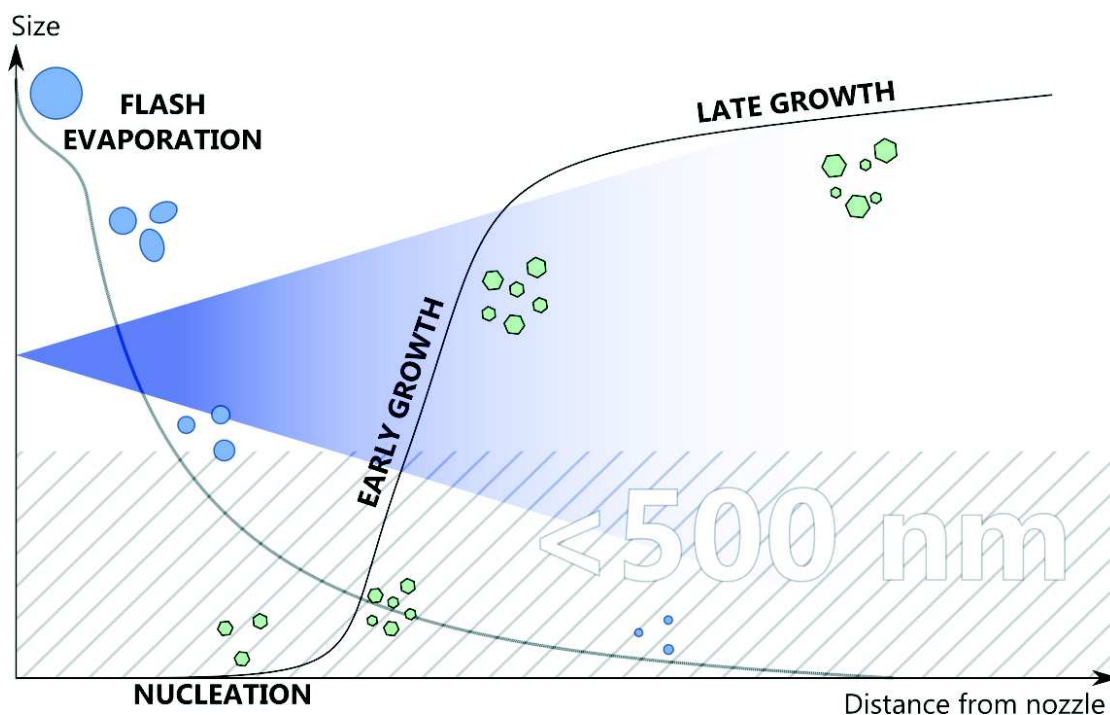


FIGURE 0.2 – Illustration schématique des phénomènes d'évaporation et cristallisation en jeu dans le SFE. La limite de 500 nm correspond à la limite actuelle de détection possible par mesure directe en ligne en anémo-granulométrie Phase Doppler

Compréhension du SFE

Peu de techniques sont à même de mesurer des aérosols à haute vitesse et de l'ordre du micron. L'interférométrie Phase Doppler est une méthode de mesure optique avancée qui, couplée à la vélocimétrie LASER, permet la mesure *in situ*, simultanée et en temps réel de la taille et de la vitesse d'objets quasi sphériques et microniques. Elle a été pour la première fois adaptée à la technologie SFE : la mesure des tailles dans l'espace du cône de pulvérisation permettra le calcul de la sursaturation. Dans un premier lieu, il s'agit de caractériser le phénomène de flash évaporation : les Figures 0.3 et 0.4 montrent les premiers résultats obtenus avec un appareil optimisé et calibré sur l'acétone. Il est remarquable d'observer trois distributions modales centrées en 2.1, 2.8 et 3.8 μm à toutes les températures ; comme attendu, la taille moyenne chute vers la limite de détection proche du micron lorsque la température augmente. En revanche, l'étude montre alors que le phénomène de flash évaporation est transitoire et commence dès 100 °C et semble ne pas être unique à 160 °C du fait de la présence persistante de deux distributions à 2.1 et 2.8 μm .

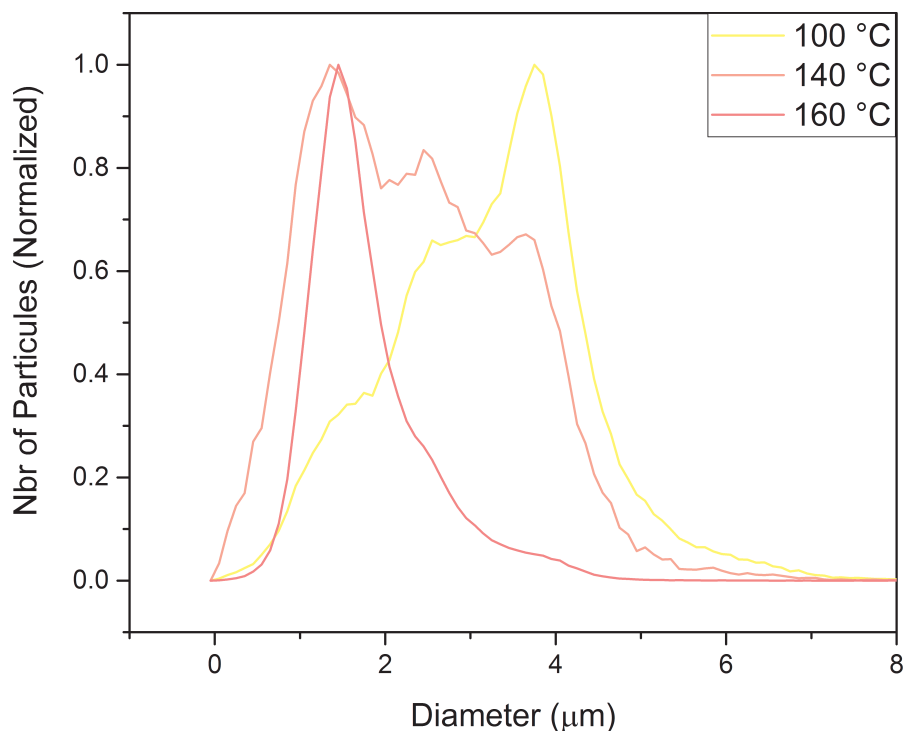
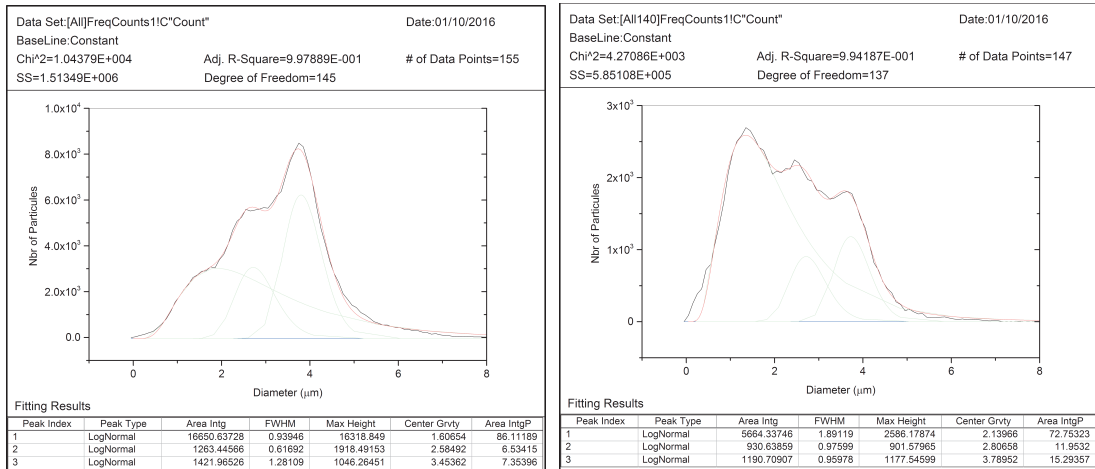


FIGURE 0.3 – Distribution en taille des gouttes pulvérisées à 100, 140 et 160°C.

Définition d'une particule

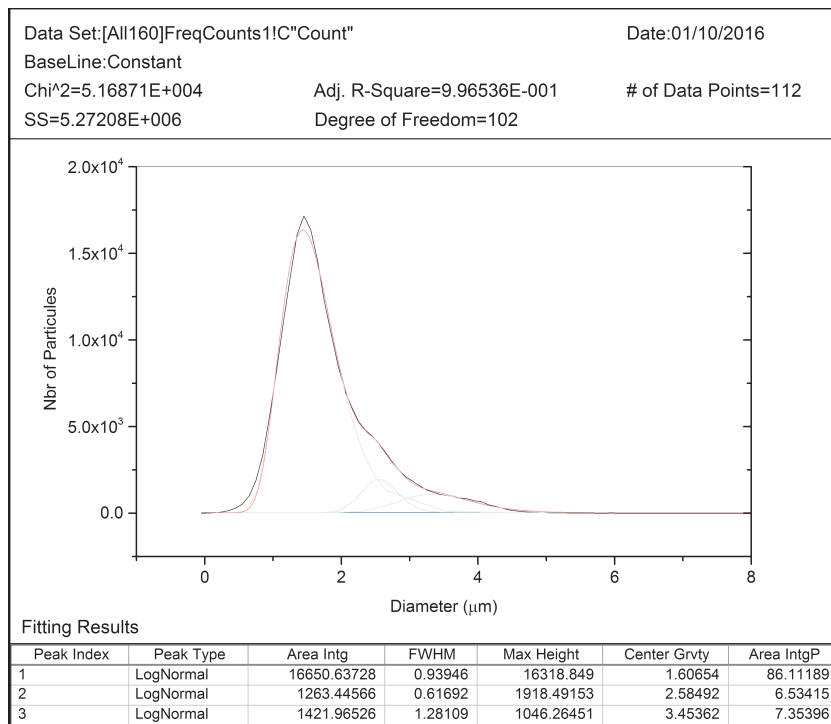
La première année de recherche fut menée sur l'étude des paramètres du SFE influençant la taille et la morphologie des cristaux. Ces derniers ont été observés en suivant une méthode développée précédemment au sein du laboratoire : il s'agit de compresser la poudre obtenue et de lisser la surface par micro coupe pour imager par Microscopie à Force Atomique (AFM). L'AFM n'apporte aucune énergie à l'échantillon, contrairement à la Microscopie Électronique à Balayage (MEB) dont le faisceau d'électrons dégrade le matériau énergétique. La méthode par AFM souffrait en revanche d'une analyse des images longues et fastidieuses, ce qui fut tout d'abord amélioré. Une méthode semi automatique a été mise en place avec le logiciel Gwyddion et la technique Watershed. Elle est composée des étapes suivantes :

Processus de localisation des grains La surface est inversée – les particules deviennent des creux – puis de l'eau virtuelle est déposée en chaque point. Ces gouttes d'eau glissent le long des pentes et la répétition de cette pluie virtuelle forme ainsi des lacs dans les minimum locaux. Ces lacs, ces ensembles virtuels, délimitent alors la position des grains.



(a) 100 °C

(b) 140 °C



(c) 160 °C

FIGURE 0.4 – Régression des profils de distribution en taille des gouttes pulvérisées à 100, 140 et 160°C.

Segmentation Précédemment si deux lacs se touchaient lors d'une pluie virtuelle, ils étaient fusionnés. Dans l'étape de segmentation, deux lacs adjacents seront notés comme différents et une bordure sera définie. La qualité des frontières entre les grains s'améliore avec des gouttes plus fines, mais le temps de calcul augmente fortement avec la diminution de la taille de goutte.

Inspection visuelles et corrections mineures Le logiciel permet l'affichage en surbrillance, le marquage et l'édition manuelle des grains ainsi que plusieurs améliorations du contraste pour permettre une vérification visuelle efficace et une correction des défauts. Les autres canaux de données tels que la phase ou l'amplitude peuvent aider à déterminer la validité d'une frontière de grain.

Distribution en taille et régression Le logiciel permet l'affichage de la distribution en taille des particules mais, grâce à l'export des données, une régression des profils de distributions peut être appliquée par un logiciel tiers. Ici le diamètre est défini comme celui d'un disque d'aire équivalent à la particule mesurée. La distribution en taille semble suivre une loi log normale et non une loi Gaussienne ce qui signifie que les particules sont générées par l'effet de nombreux effets aléatoires et multiplicatifs comme le sont souvent les aérosols (LIMPERT et al. 2001).

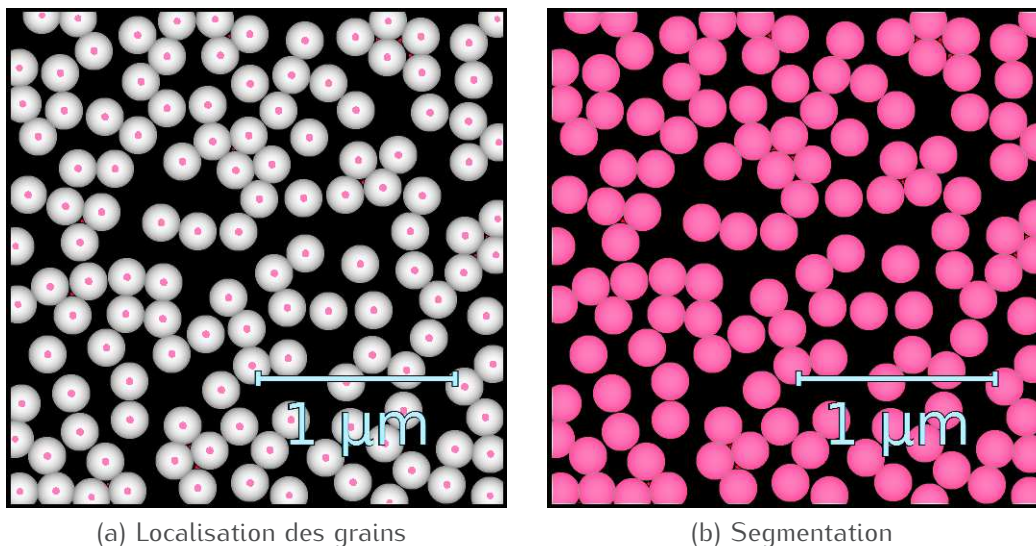


FIGURE 0.5 – Analyse Watershed illustrée sur une simulation de sphères de 200 nm.

Une étude de la méthode a été entreprise pour déterminer sa fiabilité et sa robustesse. Deux facteurs prépondérants sur la taille de particules ont été dégagés :

L'effet de la pression La presse utilisée pour la compression des matériaux énergétiques consiste en un levier supporté par un piston hydraulique ; à l'extrémité du levier, des masses sont accrochées, puis le piston est actionné pour descendre doucement le levier et donc former le comprimé dans des conditions adiabatiques. La pression appliquée est calculée en fonction du poids employé ; les valeurs utilisées sont affichées en Figure 0.1.

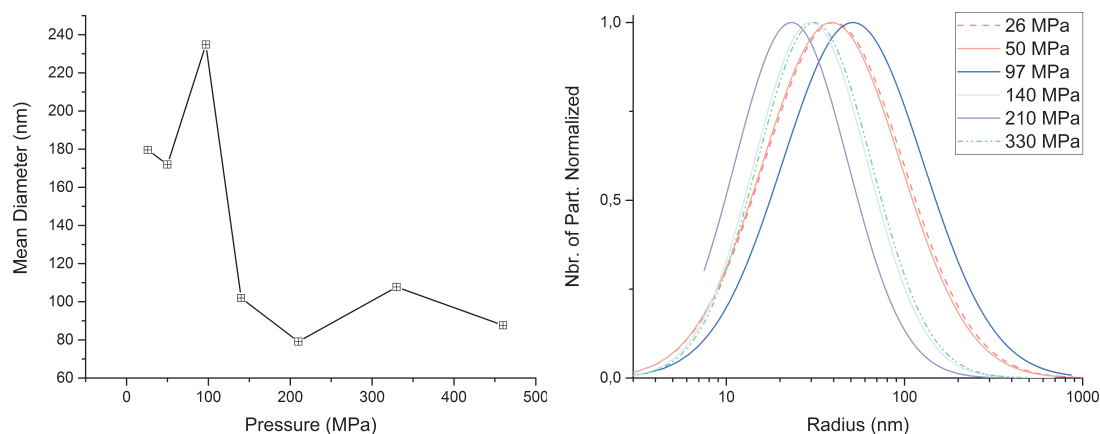
Poids (kg)	Pression (MPa)
2	12
5	26
10	50
20	97
30	140
45	210
70	330
97	460

TABLE 0.1 – Poids utilisé et pression correspondante calculée : l'effet de levier suit la loi $P = 6 \cdot \frac{M}{A} + 31$ où $A = \frac{\pi}{4} \cdot \varnothing^2$ avec M la masse du poids.

L'effet de la pression peut s'observer en Figure 0.6, où la même face de comprimé a été analysée par AFM et aucune micro coupe n'a été réalisée. Dans la Figure 0.6a une chute brutale de la taille de particule est clairement observable dès 1140kg puis la valeur se stabilise autour de 90 nm : ce changement est aussi visible en Figure 0.6b. Dans les Figures 0.6c et 0.6d, les particules sont difficilement identifiables.

Les résultats provenant de comprimés micro coupés en Figure 0.7 montrent à encore que la pression joue un rôle crucial sur la taille de particule mesurée par AFM. La réduction de taille est progressive avec l'augmentation de la pression. Au delà de 97 MPa (20 kg), les comprimés sont bien trop cohésifs pour pouvoir être usinés par micro coupe ; leur grande dureté du fait d'un comportement quasi vitreux les rend cassants sous la lame.

Le RDX micronique (M5 Eurenco) utilisé pour la recristallisation a également été analysé selon cette méthode ; les comprimés obtenus sont friables à un tel point qu'aucune micro coupe n'a pu être effectuée. Cependant, alors que la taille moyenne reste de l'ordre du micron, à la pression maximale de 97 MPa



(a) Taille moyenne en fonction de la pression (b) Influence de la pression sur la distribution en taille

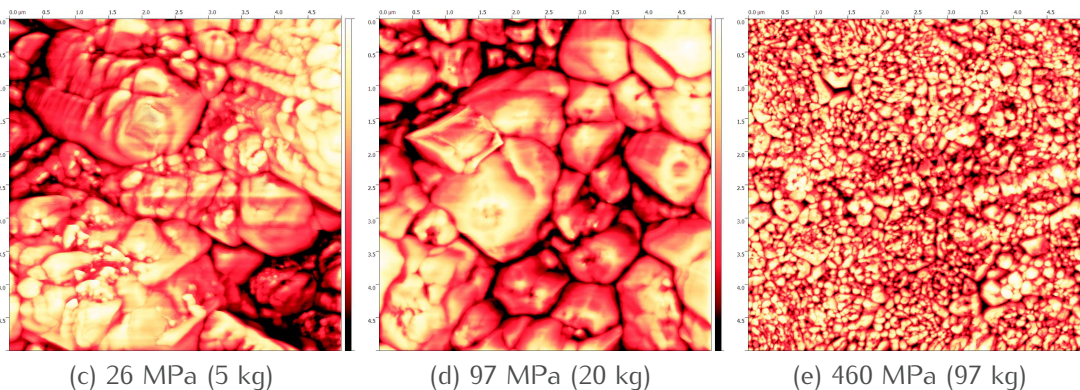
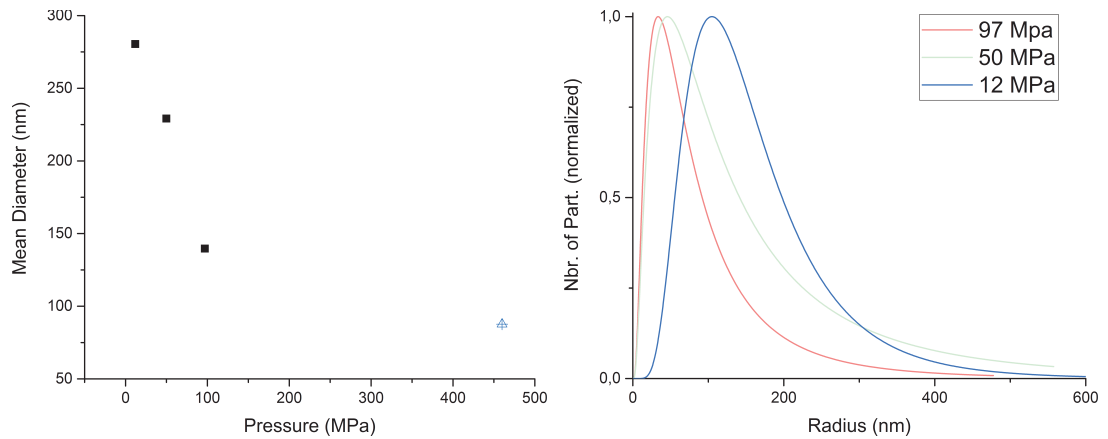


FIGURE 0.6 – Effet de la pression, sans micro coupe, $5\mu\text{m} \times 5\mu\text{m}$ pour $1024\text{px} \times 1024\text{px}$, contraste amélioré.

une chute de la taille moyenne est observée de la même manière que le RDX recristallisé par SFE. Ainsi il apparaît clairement que le nano RDX est broyé à des contraintes plus faibles et donc plus facilement : cet effet de casse ou de désagrégation doit être étudié plus en profondeur car les explosifs sont utilisés notamment en charges pressées.

Effet de la micro coupe D'après les résultats en Figures 0.7a et 0.6a, la micro coupe réduit la taille moyenne et l'effet de la pression précédemment mis en évidence est accentué. Cet effet s'explique par la dureté accrue des comprimés avec la pression : la force de micro coupe doit être plus élevée donc l'effet de broyage en surface est accru.



(a) Taille moyenne en fonction de la pression (b) Influence de la pression sur la Distribution en taille

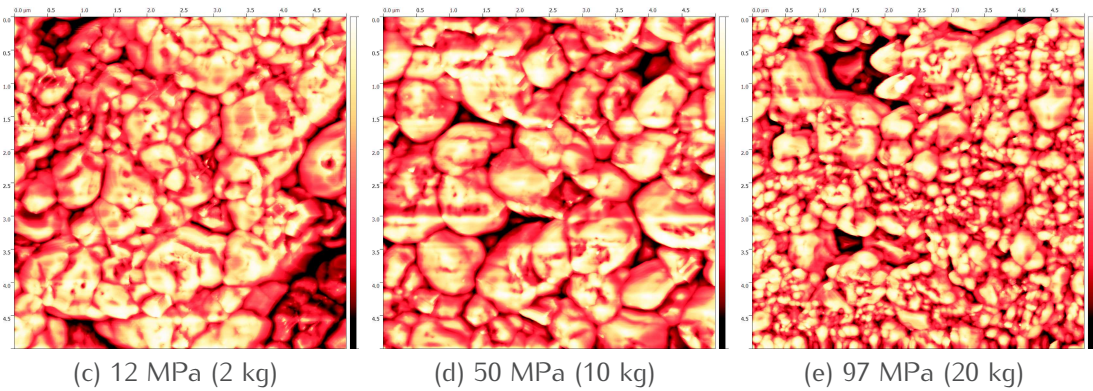


FIGURE 0.7 – Effet de la pression, avec une micro coupe, $5\mu\text{m} \times 5\mu\text{m}$ pour $1024\text{px} \times 1024\text{px}$, contraste amélioré.

Pression (MPa)	Brut	Avec micro coupe
12		280
26	180	
50	170	230
97	235	140
140	100	
210	80	
330	110	
460	90	

TABLE 0.2 – Diamètre moyen en nm selon la pression appliquée et le pré traitement par microtome; par MEB, la taille moyenne est de 500 nm.

Découplage des phénomènes au sein du SFE et contrôle des tailles

La cristallisation se déroule principalement en deux étapes successives : la nucléation et la croissance cristalline, qui peuvent être contrôlés par l'ajout d'additifs. La PolyVinylPyrrolidone (PVP) est un additif polymérique notamment utilisé dans l'industrie comme émulsifiant et stabilisant, et est enregistré comme l'additif alimentaire E1201. Il est également utilisé comme inhibiteur de croissance et promoteur de nucléation grâce à sa propriété d'adsorption autour de cristaux organiques (OZAKI et al. 2013 ; PATEL et al. 2015 ; POSTERARO et al. 2015). De même, le PolyEthylène Glycol (PEG) est un additif polymérique utilisé comme promoteur de croissance ou comme enrobant et est enregistré comme l'additif alimentaire E1521. L'effet stérique du PEG est principalement utilisé pour déclencher et permettre la croissance de cristaux de protéines (BHAT et al. 1992).

Du PVP 40k sous forme solide et du PEG 400 sous forme liquide ont été utilisés avec succès pour la cristallisation du RDX par SFE. Outre l'extension de la polyvalence du SFE en permettant la cristallisation de composés organiques avec additif polymérique sous forme solide ou liquide, la taille moyenne et la morphologie de particules ont été contrôlés. Le RDX produit avec ajout de PVP a été réduit jusqu'à 160 nm avec une morphologie sphérique ; de plus la stabilité dans le temps des tailles et morphologies ainsi que les sensibilités sont améliorées par la présence de PVP. Cette diminution de taille s'explique par la nucléation retardée par la PVP au delà du moment flash du solvant. L'ajout de PEG induit une nucléation très tôt dans des volumes de goutte plus importants ainsi qu'un taux de nucléation faible. Les cristaux croissent jusqu'à des tailles micrométriques comparables à celles du RDX commercial mais avec des sensibilités grandement réduites notamment pour la décharge électrostatique.

Innovations du SFE comme outil de recherche

Au cours de ce projet, de nombreuses améliorations et changements ont été apportés au procédé SFE et ses appareils. Parmi les innovations majeures, se trouve être l'utilisation de plusieurs buses pour étudier la cristallisation par SFE.

L'hexane est un antisolvant parfait du RDX et est thermodynamiquement compatible avec le SFE. Le mélange acétone-hexane présente aussi un azéotrope permettant une température d'évaporation plus basse que les deux solvants purs : la force motrice du SFE réside dans le degré de surchauffe du fluide, ainsi une température d'ébullition plus faible permet d'atteindre plus rapidement

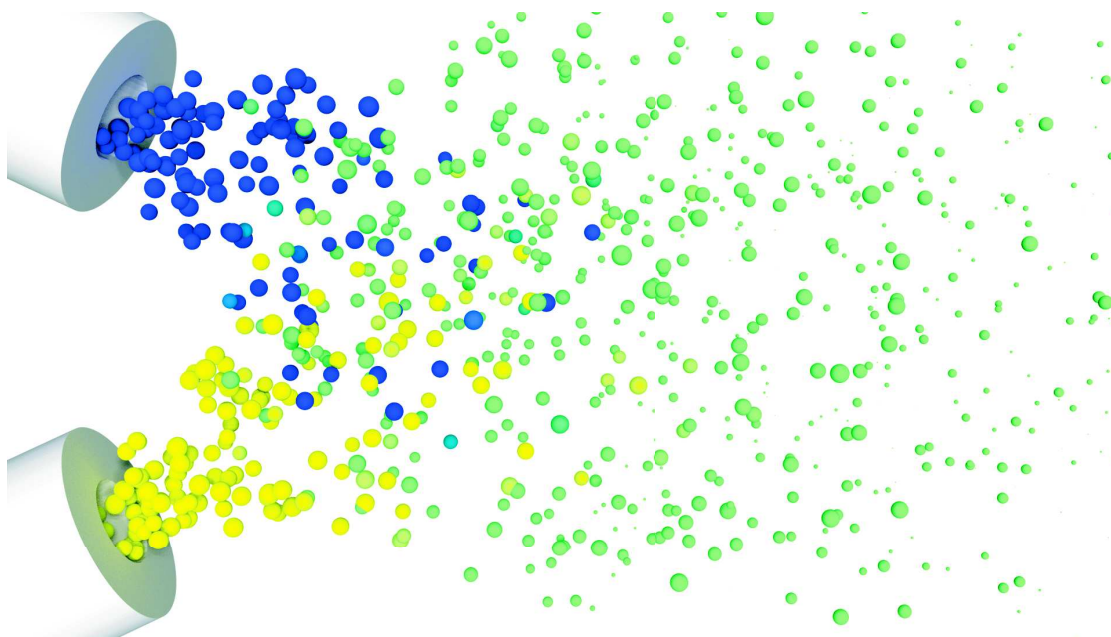


FIGURE 0.8 – Illustration du principe de cristallisation *in situ* via multi-buses

un degré de surchauffe élevé. Tous ces avantages sont étudiés en mono buse selon divers ratio solvants/anti solvants ; l'abaissement du point d'ébullition et l'augmentation de la sursaturation réduisent effectivement la taille des cristaux de RDX. Dans la continuité, un système multi-buses a été mis en œuvre pour la première fois sur le SFE afin d'augmenter brutalement le degré de sursaturation, quelques instants après le début du spray alors que les gouttes sont dans un état méta-stable. Ce système a été protégé dans l'extension d'un brevet à l'internationale ("Method for producing cocrystals by means of flash evaporation" 2016). Les avantages de passer d'un système de mono buse à plusieurs buses sont nombreux. Ainsi pour des applications industrielles du SFE, l'ajout d'un anti solvant présente l'immense désavantage de réduire la solubilité du composé et donc de réduire la productivité du procédé : le multi-buse permet alors de conserver la haute solubilité du produit dans son solvant de prédilection, mais agir sur le nuage de gouttelettes permet également plus de flexibilité et autorise les réactions chimiques *in situ*.

De part la pulvérisation de l'anti solvant par une seconde buse, se pose alors la question de savoir dans quel état l'anti solvant arrive : est il gazeux ou liquide sur le nuage de gouttes de la première buse ? La cocrystallisation est alors étudiée en multi-buses avec des débits contrôlés et des solvants différents. Ce système multi-buse, à débit contrôlé par débitmètres de précision à effet Coriolis avec vanne intégrée, découple alors l'éternel triptyque suivant : solubilité, débit

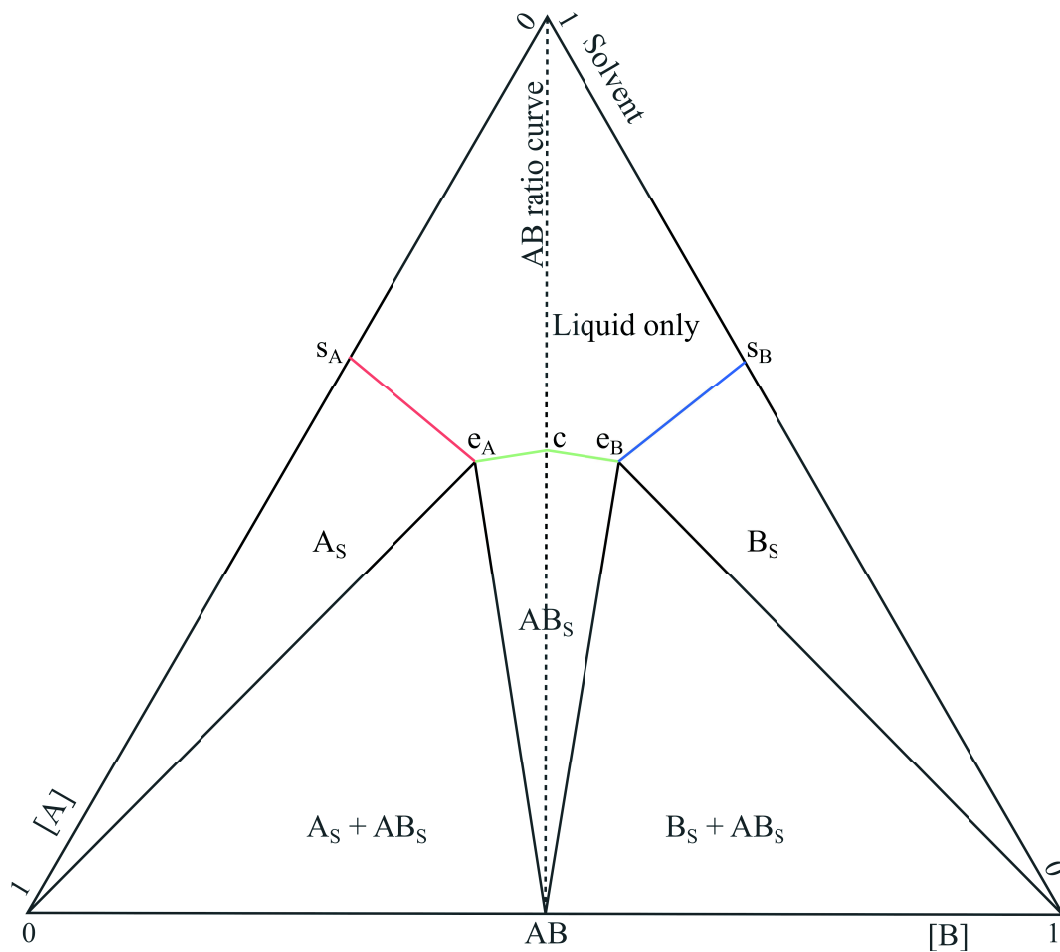


FIGURE 0.9 – Diagramme ternaire d'un cocrystal 1 :1 AB

des buses et ratio du cocrystal. La co-cristallisation à partir de deux réservoirs et buses différents a été réalisée avec succès pour la première fois au sein du SFE. En revanche, des études complémentaires sont à mener afin de déterminer les diagrammes de solubilité du cocrystal dans l'acétone-héxane.

Toutes ces études préliminaires ont posés les bases d'une étude complète et précise de la cristallisation par SFE et ont débloquent de nouvelles voies de recherche telles que les réactions *in situ*.

Liste des publications et communications

Communications

- Europyro 2015, 41^e International Pyrotechnic Seminar (Toulouse).

- 4^e ISL Budding Science Colloquium (Saint Louis, 2015).
 - European Congress and Exhibition on Advanced Materials and Processes EUROMAT 2015, B1.3 Section Nanocrystallisation (Varsovie).
 - Material Weekend Warsaw; un atelier de travail pour doctorant alliant présentations orales et cours.
 - Exposant stand DGA à l'Eurosatory 2016, Defence and Security International Exhibition (572 exposants de 56 pays, 213 délégations officielles de 94 pays)
 - 5^e ISL Budding Science Colloquium (Saint Louis, 2016).
 - Junior EUROMAT 2016 (Lausanne).
 - 6^e NANOstructures and nanomaterials SElf-Assembly (NanoSEA) (Giardini Naxos (ME), Italie 2016).
-
- 1 poster : 3^e ISL Budding Science Colloquium (2014).

Publications

- Blas, Lucia, Martin Klaumünzer, **Florent Pessina**, Silke Braun, and Denis Spitzer. "Nanostructuring of Pure and Composite-Based K6 Formulations with Low Sensitivities." *Propellants, Explosives, Pyrotechnics* 40, no. 6 (2015) : 938–44.
- **Florent Pessina**, Fabien Schnell, and Denis Spitzer. "Tunable Continuous Production of RDX from Microns to Nanoscale Using Polymeric Additives." *Chemical Engineering Journal* 291 (May 1, 2016) : 12–19. doi :10.1016/j.cej.2016.01.083.
- Martin Klaumünzer, **Florent Pessina**, and Denis Spitzer. "Indicating Inconsistency of Desensitizing High Explosives against Impact through Recrystallisation at the Nanoscale." *Journal of Energetic Materials*, July 1, 2016, 1–10. doi :10.1080/07370652.2016.1199610.
- Denis Spitzer, Vincent Pichot, **Florent Pessina**, Fabien Schnell, Martin Klaumünzer, and Lucia Blas. "Continuous and Reactive Nanocrystallization : New Concepts and Processes for Dual-Use Advances." *Comptes Rendus Chimie*, July 2016. doi :10.1016/j.crci.2016.06.009.

- **Florent Pessina** and Denis Spitzer. “The longstanding challenge of the nano crystallization of 1,3,5-trinitroperhydro-1,3,5-triazine (RDX)” Beilstein Journal of Nanotechnology *Under Review*.

Formations scientifiques suivies

- Sensibilisation à la pyrotechnie 3PSC17C, Centre de Formation de la Défense (Bourges 2013)
- Advanced Functional Materials and Characterization, CNRS-EWHA Winter School (Strasbourg 2014)
- Nano-OptoMechanics, School in Physics (Strasbourg 2014)

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Chapter 1

Explosives and Characterization

1.1 Overview

The term “energetic material” encompasses any type of material (composite, polymer, organic...) which can rapidly release energy by a violent reduction-oxidation reaction. A stimulus like shock, friction, heat or electrostatic discharge triggers the local reaction; then it propagates through the material creating a reaction front. That decomposition usually produces large amount of gas and heat, and three modes of decompositions can be identified mainly from the velocity of the redox reaction front.

The **combustion** is the slowest mode of decomposition (mm/s - m/s), and is characterized by the complete oxidation of all intermediate products. The combustion requires so large amounts of oxygen, that oxygen is mainly provided by the environment. Faster than the combustion, the **deflagration** (m/s - km/s) occurs when the released heat propagates beyond the reaction front and so facilitates the redox reaction. Deflagration can be considered as a form of burning, but in contrast to pure combustion, the phenomena is self-propagating and does not require an external source of oxygen. Supersonic explosions created by high explosives are known as **detonations** which travel via supersonic shock waves ($> \text{km/s}$); that wave, and not the thermal front of reaction, propagates the reaction. Transition from one mode to another can happen intentionally or not; without compaction or enough ignition energy, the material may only burn (1,3,5-trinitroperhydro-1,3,5-triazine (RDX) in the C4 composition burns at 2 cm/s whereas it detonates at 8.75 km/s), or when accidentally confined, a propellant detonates.

Therefore, depending on their decomposition mode and their pyrotechnic properties, energetic materials can be sorted in three classes: propellants, primary explosives (or initiating explosives) and secondary explosives (or base

charge). Materials such as Ammonium Nitrate (AN) or Ammonium Perchlorate (AP) are sometimes classified as tertiary explosives, which are even less sensitive and energetic. From a chemical point of view, explosives are intrinsic energetic materials in which usually nitro or nitramine groups react with the closest carbon available inside the same molecule; on the contrary, thermites are a physical mix of an oxidizer (e.g.: Fe_3O_4) and a reducing agent (e.g.: Al) (Comet et al. 2016).

Used in gunpowder, solid-fuel rockets and mining industry, **propellants** are deflagrating explosives with the specificity of producing high amount of gases, usually to get a thrust. **Primary explosives** detonates through the influence of a moderate external stimulus; less sensitive detonative ones are called secondary explosives. The initiation of **secondary explosives** generally requires the shock wave energy from a primary explosive: such succession of explosive event is called explosive train involved in detonators for instance. All explosives having a higher sensitivity than pentaerythritol tetranitrate (PETN) can be considered as primary, and the less sensitive ones as secondary explosives. The sensitivity to impact and friction of PETN is 3 J–4 J and 60 N, respectively. The notion of sensitivity for energetic materials is discussed in Section 1.3.2.

1.2 Organic Secondary Explosives

This work was focused on a very few organic explosives, in order to carefully study the crystallisation parameters independently from the chemical compound. The first one, RDX, is widely used in civilian and military applications, and serves as a reference energetic material in scientific studies. Both octahydro-1,3,5,7-tetra-nitro-1,3,5,7-tetrazocine (HMX) and 2,4,6,8,10,12-hexanitro-2,4,6,8,10,12-hexa-azaisowurtzitane (CL-20) are studied here due to their ability to cocrystallise; a cocrystal is simply a multicomponent molecular crystal, owning a unique crystalline structure with each compound included in the unit cell. The following short overview presents their structural characteristics and their physical and pyrotechnical properties.

1.2.1 1,3,5-trinitroperhydro-1,3,5-triazine (RDX)

The 1,3,5-trinitroperhydro-1,3,5-triazine is also found under the following denominations cyclo-1,3,5-trimethylene-2,4,6-trinitramine, 1,3,5-trinitrohexahydro-s-triazine, cyclotrimethylenetrinitramine, hexahydro-1,3,5-trinitro-s-triazine, trimethylenetrinitramine, T 4, cyclonite, hexogene, and RDX. The most common and widely accepted one is the acronym RDX whose origin is surprisingly not known for sure; probably from its first secret code "Research Department

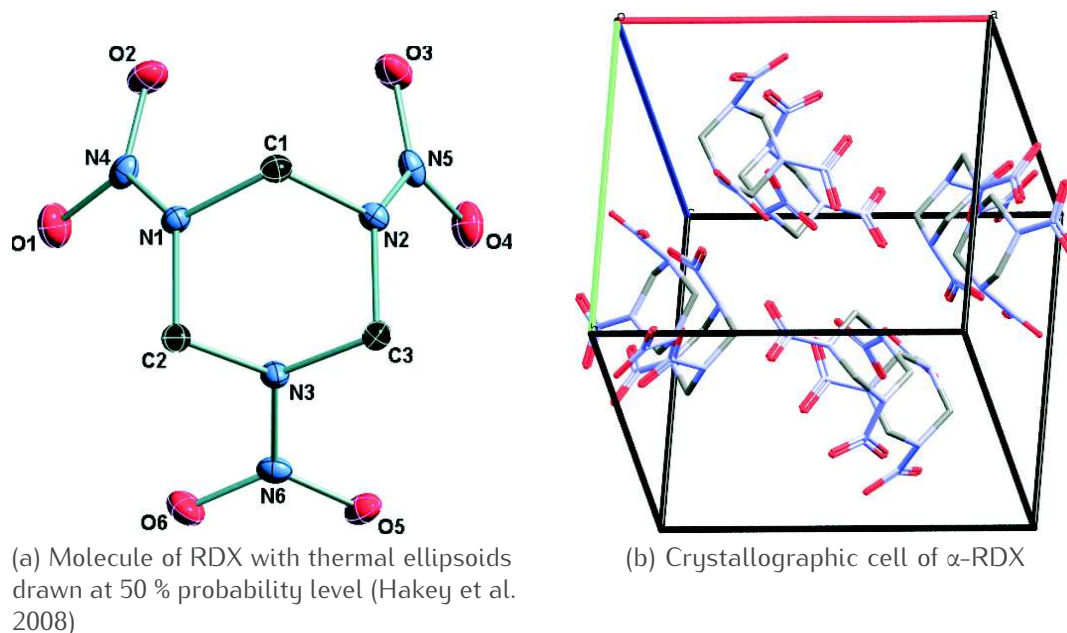


Figure 1.1 – RDX visual representations. H atoms have been omitted for clarity.

Explosive”. RDX is probably the most important high-brisance explosive from the Second World War to nowadays.

α -RDX is the stable form of RDX for all temperatures at 1 atm; however, at high pressures, several polymorphs of RDX exist and have been recently discovered : γ -RDX is stable above 3.8 GPa between room temperature and 225 °C, and above that temperature β -RDX lies from 2.5 GPa–7 GPa (Hakey et al. 2008). A δ form has been reported but not resolved (Ciezak et al. 2007), and the dense ϵ -RDX formed at 3.6 GPa can be recovered at 1 atm at 150 K–220 K (Millar et al. 2010).

RDX is soluble in acetone, dimethylsulfoxide (DMSO), DiMethylFormamide (DMF), N-Methyl-2-pyrrolidone (NMP) etc. (Sitzmann et al. 1973), sparingly soluble in ether and ethanol, almost insoluble in water (16, 35-52 and 123 mg/L at 5, 20 and 40 °C (Boyer et al. 2007)) and totally insoluble in n-hexane (PANT et al. 2013). Cyclohexanone, nitrobenzene and glycol are solvents at elevated temperatures (Sitzmann et al. 1973).

The RDX used in this work is provided by Eurenco, labelled as M5 and used as is, without further purification; the mean particle size is 6.8 μm .

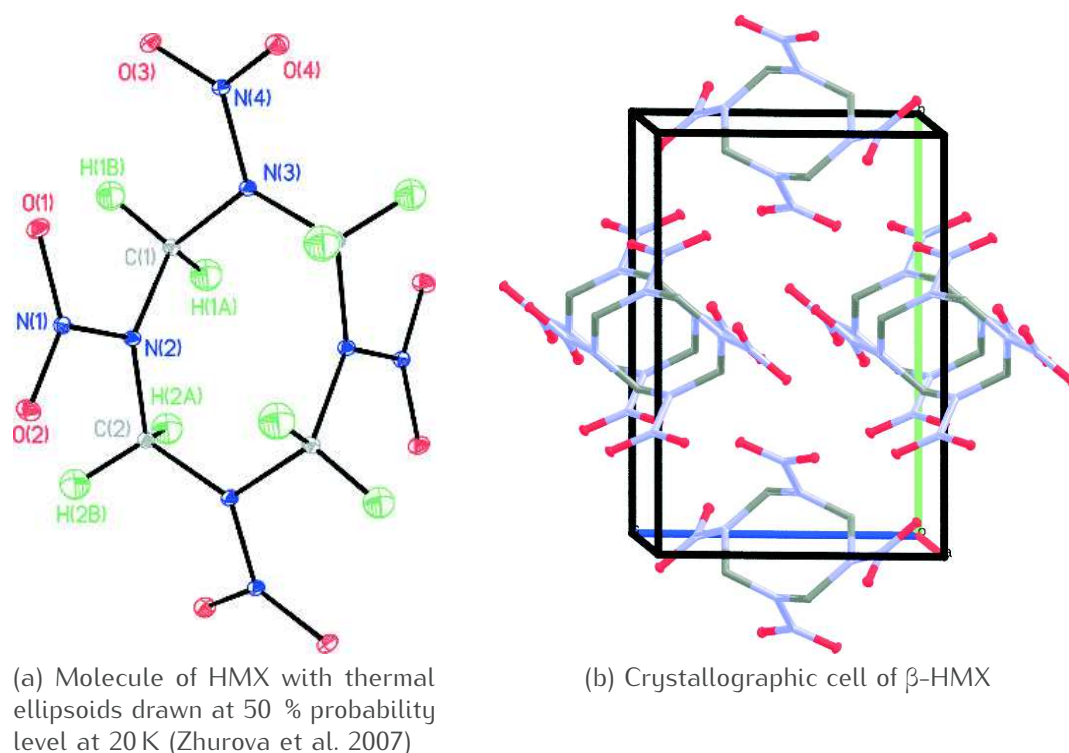


Figure 1.2 – HMX visual representations. H atoms have been omitted for clarity.

1.2.2 Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)

The octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine is also found under the following denominations cyclotetramethylene tetranitramine, homocyclonit(e), octogen but is commonly named HMX. HMX was first discovered as a by-product of RDX by the Bachmann process (Bachmann et al. 1949). Therefore, like RDX, the HMX acronym may refer to High Melting eXplosive, Her Majesty's eXplosive, High-velocity Military eXplosive, or High-Molecular-weight RDX. Due to the high density of its stable β phase, its high melting point and its detonation performances, the HMX is a prime secondary explosive. HMX exhibits three distinct polymorphic forms – α (105 °C–160 °C), β and δ (160 °C–m.p.) – and a γ hydrated form metastable existing at all temperatures at 1 atm.

HMX solubilities are even worse when compared to RDX; HMX is soluble in DMSO but not in DMF nor NMP, and is slightly soluble in acetone (2.8 wt% at Standard Ambient Temperature and Pressure as a temperature of 298.15 K and an absolute pressure of 100 kPa (1 bar) (SATP)).

1.2.3 2,4,6,8,10,12-hexanitro-2,4,6,8,10,12-hexaazaisowurtzitane (CL-20)

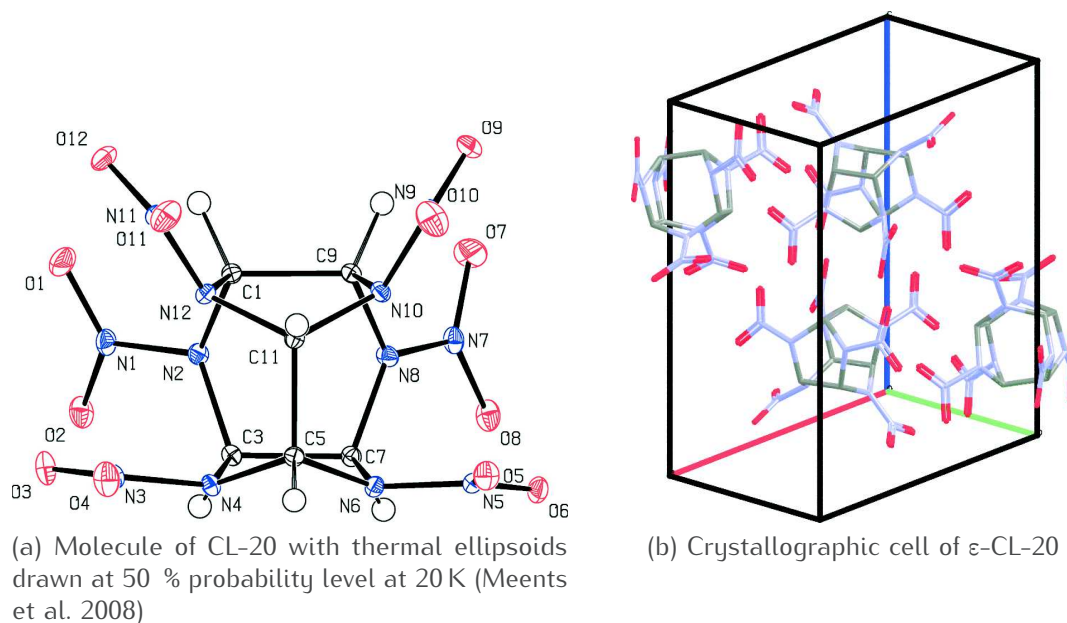


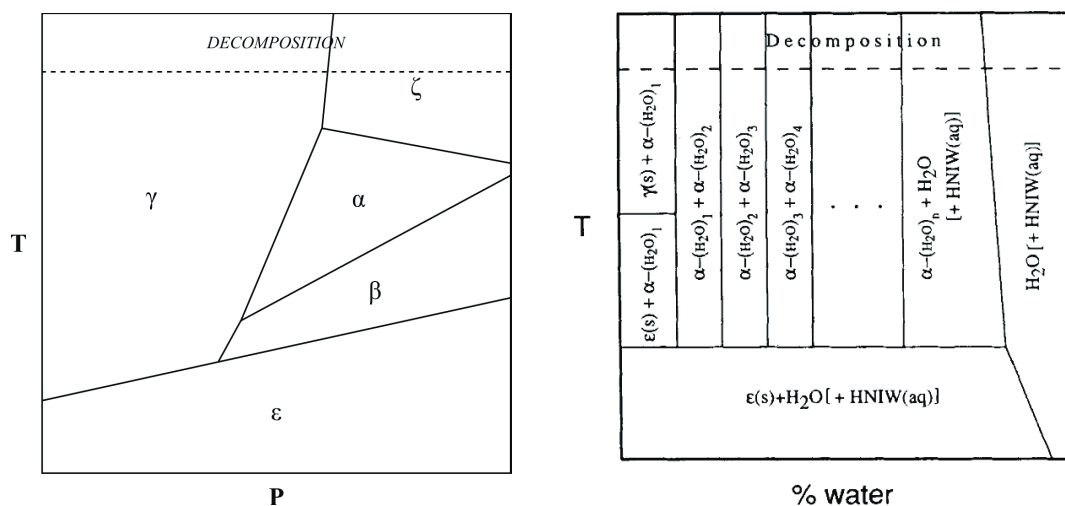
Figure 1.3 – CL-20 visual representations. H atoms have been omitted for clarity.

2,4,6,8,10,12-Hexanitro-2,4,6,8,10,12-hexaazaisowurtzitane is also found under the following denominations hexanitrohexaazaisowurtzitan(e), 2,4,6,8,10,12-(hexanitro-hexaaza)-tetracyclododecane, HNIW or CL-20. CL-20 is the most widely used acronym and comes from the Naval Air Weapons Station (NAWS) China Lake facility where it was first produced by Nielsen (1997). CL-20 can be considered as a potent explosive due to its high density and high detonation velocities, but the difficult detection of the decomposition gas and the high oxygen balance place the CL-20 as a remarkable propellant too.

CL-20 exhibits also a high degree of polymorphism: four forms (α , β , γ , ϵ) have been observed at SATP conditions (Foltz et al. 1994; Russell et al. 1993) and two (δ , ζ) under pressure. The ζ -CL-20 comes from the $\gamma \rightarrow \zeta$ transition at 0.7 GPa. The stability of different phases can be sorted as $\epsilon > \gamma > \alpha > \beta$ and is schematically described in Figure 1.4a p. 36. However, the hydration of CL-20 plays an important role at intermediate pressures and temperatures in the stability of the α form as described in Figure 1.4b p. 36.

The solubility of ϵ -CL-20 is good at SATP in acetone (100 wt%), ethyl acetate (45 wt%) and tetrahydrofuran (THF) but slight in aromatic or organochloride

solvents (von Holtz et al. 1994). The ε -CL-20 is the phase of interest due the highest density ($\rho_\varepsilon = 2.04 > \rho_\beta = 1.98 > \rho_\alpha = 1.97 > \rho_\gamma = 1.92 \text{ g/cm}^3$) and the highest detonation velocity ($v_\varepsilon = 9660 > v_\beta = 9380 \text{ m/s}$ (Dumas 2003)).



(a) Pressure-Temperature schematic diagram of CL-20 crystallographic phases.

(b) Dependency in hydration and temperature of CL-20 polymorphs.

Figure 1.4 – CL-20 polymorphism adapted from Foltz et al. (1994).

1.2.4 Cocrystal CL-20:HMX 2:1

Bolton et al. (2012) first reported the crystallisation and characterization of the cocrystal CL-20:HMX with a molar ratio of 2:1. An impact sensitivity as low as β -HMX was measured while a higher detonation velocity than β -HMX was predicted. Those results are representative of the advantage of crystallisation as a solid state engineering strategy for improved energetic material. This approach is well known for pharmaceutical compounds (Fleischman et al. 2003; Schultheiss et al. 2011; Vishweshwar et al. 2006) and is also emergent for optic (Sun et al. 2006; Yan et al. 2011) and semiconductors (Sato et al. 2012).

1.3 Analytical Methods

1.3.1 Classic Material Characterization Methods

X-Ray Diffraction (XRD) The periodicity of a crystal can be investigated by using a X-ray beam. In X-Ray Diffraction (XRD), the incident beam penetrates through the matter within several hundreds of microns; the photons interact

Characteristics	α -RDX	β -HMX	ϵ -CL-20
Colour	colourless	colourless	colourless
Molecular formula	$C_3H_6N_6O_6$	$C_4H_8N_8O_8$	$C_6H_6N_{12}O_{12}$
Molecular weight	222.1	296.2	438.19
Space Group	$Pbca$	$P2_1/c$	$P2_1/c$
CCDC IDs	CTMTNA, 03, 08-12	NA	PUBMUU 02, 05, 12-22
COD IDs	5000148, 2019354-9, 2219089	4110146	2300020-4
Stability range at 1 atm	RT to 222.1	RT to 102-150°C	RT to 56.5°C
Energy of formation	+401.8 kJ/kg	+353.6 kJ/kg	+1005.3 kJ/kg
Enthalpy of formation	+301.4 kJ/kg	+253.3 kJ/kg	+920.5 kJ/kg
Oxygen balance	-21.6%	-21.6%	-10.95%
Nitrogen content	37.84%	37.83%	38.3%
Volume of explosion gases	903 l/kg	902 l/kg	NA
Heat of explosion (H ₂ O liq.)	5647 kJ/kg	5249 kJ/kg	6314 kJ/kg
Heat of explosion (H ₂ O gas)	5297 kJ/kg	5599 kJ/kg	6084 kJ/kg
Heat of detonation (H ₂ O liq.)	6322 kJ/kg	6197 kJ/kg	NA
Specific energy	1375 kJ/kg	1367 kJ/kg	1323 kJ/kg
Density	1.82 g/cm ³	1.91 g/cm ³	2.04 g/cm ³
Melting point	204 °C	280 °C	> 195 °C (decomposition)
Detonation velocity, confined	8750 m/s at 1.76 g/cm ³	9100 m/s at 1.9 g/cm ³	9660 m/s (Dumas 2003)
Impact sensitivity	7.4 N.m	7.4 N.m	4 N.m
Friction sensitivity	120 N	120 N	48 N

Table 1.1 – Characteristics of the most common crystalline forms of RDX (Krause 2005; Meyer et al. 2008; Miller et al. 2001), HMX (Krause 2005; Meyer et al. 2008; Miller et al. 2001) and CL-20 (Krause 2005; Meents et al. 2008; Meyer et al. 2008; Nair et al. 2005)

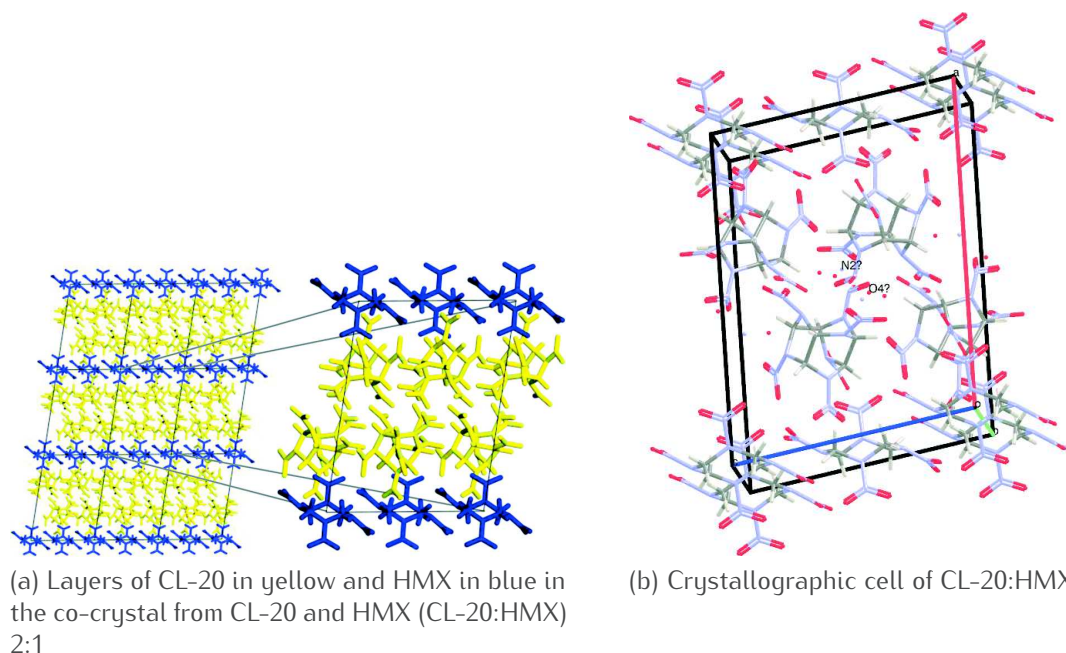


Figure 1.5 – CL-20:HMX visual representations (Bolton et al. 2012). H atoms have been omitted for clarity.

with the electrons of the material which oscillate at the same frequency and scatter the electromagnetic waves. Waves scattered from different points in space travel different paths and consequently exhibit a phase shift, therefore causing destructive interferences. The detectable X-ray emissions in a crystalline sample come from the resonance of ordered atoms in the crystallographic cell at a specific angles. The Bragg's law determines those specific directions where the interferences are constructive: $2d \sin \theta = n\lambda$ where d is the spacing between diffracting planes, θ the incident angle, n an integer, and λ the wavelength of the incident beam. The rotation of both the emitter and detector allows the recording of the diffracted signal depending on the angle θ in a unique diffractogram. The powder diffraction pattern provides various information of the crystalline structure as summarized in Figure 1.6 p. 39.

Powder X-Ray Diffraction was obtained on a D8 Advance (Bruker), with a LynxEye detector and a copper source with no filtering of the second wavelength. Please note that hkl indexes mentioned in this work are made according to the standardization of the IUCr; so previous publications mentioning abc indices are quoted here as cab. Figure 5.7 p. 155 and crystallographic studies have been made using the open-source software VESTA (Momma et al. 2011).

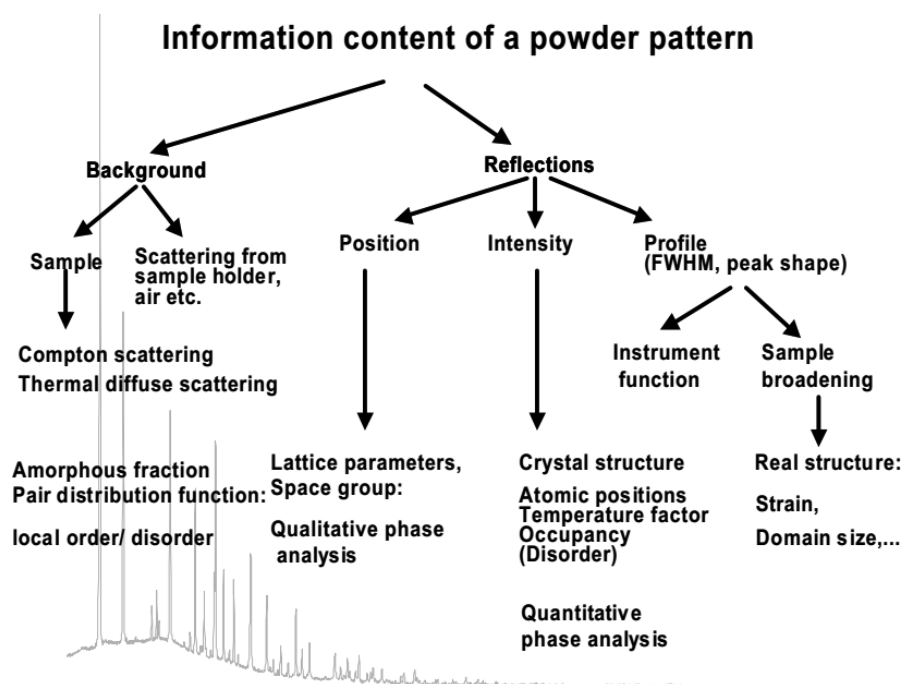


Figure 1.6 – Diagram highlighting the information available from the interpretation of an XRD pattern (Dinnebier 2001).

Scanning Electron Microscopy (SEM) allows the direct imaging of a sample at micron or nano scale with a focused beam of electrons. When interacting with the sample, both photons and electrons are emitted giving various information from the sample: X-rays for thickness and also qualitative and quantitative chemical information, secondary electrons for topology, Auger electrons for chemical information, catholuminescence for electrical information and primary backscattered electrons to determine the atomic number and the topography. Secondary electron detector and back-scattered detector are standard equipments for a Scanning Electron Microscopy (SEM). To avoid noisy interactions with gaseous molecules, the imaging occurs under vacuum. For conventional imaging in the SEM, the sample's surface must be electrically conductive and electrically grounded to prevent any accumulation of electrostatic charges.

Sizes measurements were made manually over at least one thousand particles per sample within the software Gwyddion (Nečas et al. 2012) then a log-normal fit was applied on the particles size distribution (PSD): geometrical mean and multiplicative standard deviation (dimensionless) (Limpert et al. 2001) are reported here and written as “mean(SD) unit”. Gaussian fitting is in poor accordance; droplets size distributions of aerosols usually have a log-normal shape (Zender 2008) and colloids can be found also to follow a log-normal

distribution (Limpert et al. 2001).

Brunauer–Emmett–Teller theory (BET) Brunauer–Emmett–Teller theory (BET) theory explains the multilayer adsorption of gas molecules on solids. The BET apparatus measures the amount of gas adsorbed across a wide range of relative pressures at liquid nitrogen temperature (77 K) and applies the BET theory to calculate the specific surface area, the pore size distribution and the pore volume. The adsorption and desorption isotherms also return some information about the type of porosity of the sample. Decreasing the molecular size of the adsorbed gas used – for instance from nitrogen to krypton– increases the precision but limits the measurement to lower surface area ($\sim 1 \text{ m}^2/\text{g}$ for krypton).

Atomic Force Microscopy (AFM) The development of nano-technology started with the invention of the STM and quickly followed by the Atomic Force Microscopy (AFM) in the early 80's at the IBM Zurich Research Laboratory (Binnig et al. 1986, 1983, 1982). Specifically, AFM allows the visualization at the atomic scale of non-conductive samples by a vibrating cantilever with a tip at its end. When the tip is interacting with the surface of the sample (Van der Waals forces, dipole-dipole interactions, electrostatic forces, etc.), the amplitude of the cantilever oscillation decreases. Therefore, this change is used to detect the proximity of the surface: the altitude of the cantilever is regulated to keep a constant amplitude oscillation thus to give the topographic image of the sample surface. This mode of acquisition is called tapping mode and the phase of the cantilever oscillation is also recorded. Phase changes occur when heat is dissipated by the cantilever, allowing the detection of variation in hardness or adhesive properties.

Dynamic Light Scattering (DLS) When a light source passes through a colloid, particles with a size smaller than the wavelength scatters the light in all direction. Just as in XRD, the diffraction comes from different positions in space and exhibits constructive or destructive interferences. Due to the Brownian motion, the optical path length is constantly changing in time, so the resulting noisy diffracted pattern changes in time and with the size of the particles. The intensity fluctuations from this motion, namely the computed intensity correlation function, is analysed to provide the diffusion coefficient of the particles. Then an hydrodynamic radius is calculated from the Stokes-Einstein equation

$$D = \frac{k_B T}{6\pi \eta r} \quad (1.1)$$

where η is the dynamic viscosity, r the radius of the assumed spherical particle, k_B the Boltzmann's constant, and T the absolute temperature.

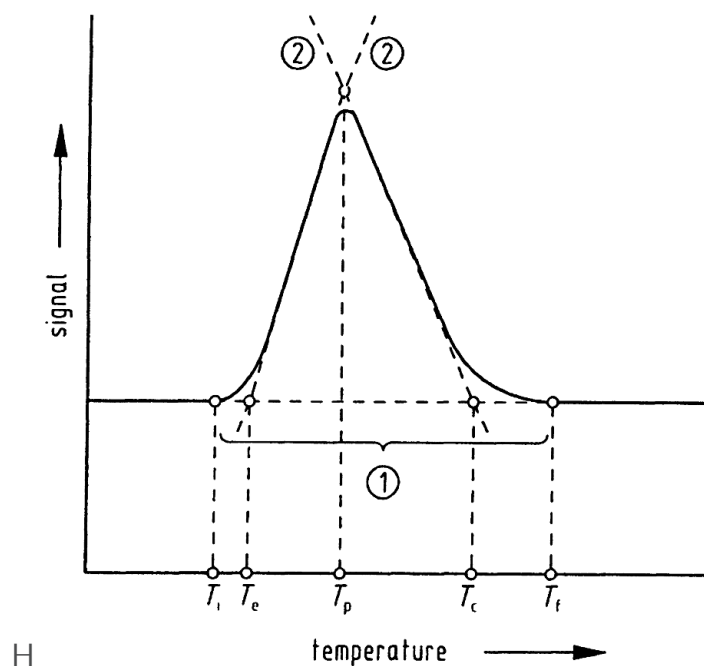


Figure 1.7 – DSC peak analysed from Höhne et al. (2003): (1) baseline (interpolated), (2) auxiliary lines, T_i initial peak temperature, T_e extrapolated peak onset temperature, T_p peak maximum temperature, T_c extrapolated peak offset temperature, T_f final peak temperature.

Differential Scanning Calorimetry (DSC) Differential Scanning Calorimeters measure the change of the differential heat flow rate between the sample and the reference while regulating the temperature. A few milligrams of the sample are placed in a hermetically closed gold crucible. An identical empty pan is used as reference. The rate of heating heavily influences the peak shapes and resolutions; keeping a small rate is of interest to separate peaks, especially for energetic materials having the melting point close to their decomposition (e.g. RDX), but too small rate will result in broad peaks of small intensities overlapping each others. So the position of the peak maximum changes with the heating rate but also with the thermal conductance and the mass of the sample. Only the extrapolated peak onset temperature is relatively independent of experimental parameters (Höhne et al. 2003).

Differential Scanning Calorimetry (DSC) was performed with a Q-1000 DSC, from TA instruments, under N_2 flow of 50 ml/min at 2 °C/min ; the low thermal ramp is a compromise between peak separation and intensity. Extrapolated temperatures were obtained using the tangent technique as described by Höhne

et al. (2003) in Figure 1.7. The exothermic energy released by the decomposition is calculated from the integration of the heat flow over the temperature range of the peak.

Infrared (IR) Spectroscopy Bonded atoms in molecules are in motion between each other; each motion is periodic with a unique frequency and different modes of molecular vibration can be distinguished such as stretching and bending. When a molecule is hit by a radiation having the same energy of the transition energy of a vibration –the resonant frequency–, that radiation is absorbed. Since the related wavelengths are in the middle-infrared, between 10 et 4000 cm^{-1} , the technique is named infrared spectroscopy (IR). The energy from the resonant frequency depends on the molecular potential energy surfaces, the masses of the atoms involved and the associated vibronic coupling, therefore allowing the identification of the chemical groups of the compounds and their interactions. However, the transition has to change the dipole moment of the molecule to be “IR active”, unlike the stretching of C-C bond in ethane for instance. Furthermore, the greater the dipole is, the greater the absorbance intensity will be. The method used to measure infrared absorption and emission spectra is the Fourier Transform Infrared Spectroscopy (FTIR); the instrument uses a Michelson interferometer coupled with a Fourier transformation of the interferogram in order to obtain the final spectrum.

Nuclear Magnetic Resonance (NMR) Spectroscopy NMR occurs when the nucleus of certain atoms is placed in a static magnetic field and an additional oscillating magnetic field. Only some atoms can exhibit NMR: nuclei possessing a not null spin, more usually a spin of 1/2 such as in ^1H , ^{13}C , ^{19}F and ^{31}P . Schematically, the transition between the two possible energy states of such nuclei is triggered when the frequency of the oscillating magnetic field matches that transition energy: such frequencies are typically in the radio frequency range for magnetic fields or around 20 T. NMR spectroscopy detects and records that magnetic resonant absorption.

1.3.2 Explosive Specific Characterization Techniques

The determination of the sensitivity of an explosive is the prime set of characterizations. Not surprisingly, pyrotechnic scientists put safety first, especially when it comes to explore new materials based on the most devastating explosives. Various methods of evaluation exist depending on the stimuli, the mass of the studied material and the application. At the small scale of a laboratory, only

three techniques are of interest based on the three main stimuli: impact, friction and electrostatic discharge.



(a) Julius Peters Bundesanstalt für Materialprüfung (BAM) Fall-Hammer for impact test



(b) Julius Peters BAM Machine for friction test



(c) OZM Research Electrostatic Discharge (ESD) 2008 apparatus

Figure 1.8 – Apparatuses for testing the mechanical and electric sensitivity at small scale, in use at NS3E.

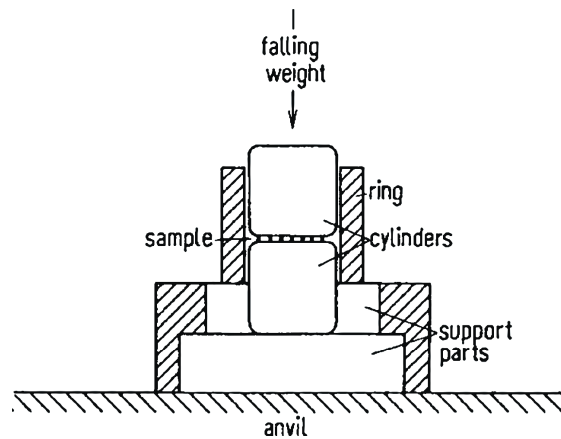


Figure 1.9 – Sample holder for BAM Fall-Hammer (Meyer et al. 2008).

Impact The small scale drop-hammer impact sensitivity test is described in the international guidelines of the UNECE (test code 3(a)(ii) (*UN Manual of*

Tests and Criteria 2016)) and in the French norm NFT 70-500. Historically the fall-hammer method was modified by the German BAM, in order to obtain better reproducible values (Meyer et al. 2008). A cylindrical spoon measures 40 mm³ of energetic material which is placed between two cylindrical pistons maintained by a ring (Figure 1.9 on the left). Those cylinders and rings are constituting the sample holder and are made of steel with controlled hardness, dimensions, surface roughness and flatness; they are renewed for each falling test procedure. If the sample is a powder or a paste, the upper cylinder is slightly pressed into the charged confinement device. The sample holder is set below a vertical rail guiding a free movable weight (Figure 1.8a p. 43). Two masses of 1 and 5 kg are available, falling from a height of 15 cm to 100 cm, allowing the measurements over a range of energy from 1.56 J to 50 J. The energy is simply calculated from the gravitational potential energy $e = mgh$.

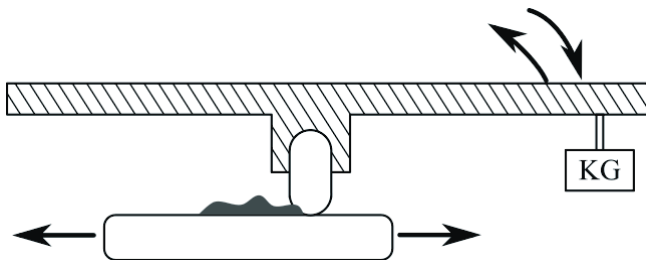


Figure 1.10 – Schematic principle of the BAM friction sensitivity test.

Friction The small scale sensitivity BAM test is described in the international guidelines of the UNECE (test code 3(b)(i) (*UN Manual of Tests and Criteria* 2016)) and in the French norm NF T70-503. Again, a cylindrical spoon measures about 10 mm³ of energetic material which is placed on the surface of a roughened 25 mm × 25 mm × 5 mm porcelain plate.

Then, on top of this plate is maintained a cylindrical porcelain peg (10 mm in diameter for a height of 15 mm), having a roughened spherical end (Figure 1.10). This peg is fasten on a rod which can be moved up and down. The pressure applied on the sample by the peg is set by a weight at the end of the lever: the nine different weights and six different mounting positions on the arm allows a measurement range from 5 N to 360 N.

Electrostatic Discharge (ESD) The sensitivity towards electrostatic discharge is a recent technique: for instance, the electrostatic stimuli are not investigated in the Manual of Tests and Criteria on the transport of dangerous goods of the UNECE (*UN Manual of Tests and Criteria* 2016). OZM Research manufactures the ESD 2008A tester used in several European laboratories. The sample is placed inside a small sacrificial plastic ring on top of the ground electrode; the volume of material is 7 mm³. The electrostatic discharge is delivered from the top

by the main electrode; see Figure 1.11 on the left. The apparatus has several capacitors and also a potentiometer to change the tension; the energy delivered through the sample is simply $E = \frac{1}{2}CU^2$, where U is the tension in Volt and C the capacity in Farad.

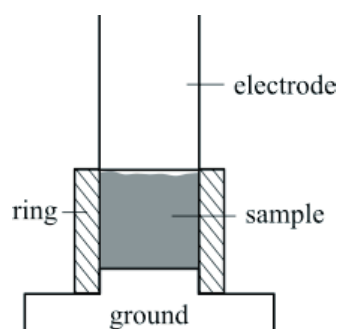


Figure 1.11 – Schematic principle of the OZM ESD 2008A tester.

Data Interpretation and Evaluation To define the reaction of a small scale sensitivity such as those mentioned above, the operator should carefully watch for any smokes, odour, sparking, popping noises, scorch marks etc. An instrumented version of the BAM fall-hammer called BIC records the overpressure and the lightening with four fibre optic detectors (Coffey et al. 1995). For instance, at the friction test, a simple odour is not significant enough to mark the event as a success full ignition, namely a Go event.

The highest stimulus level at which a predetermined number of No-Go events are observed without any Go occurring is the Threshold Initiation Level (TIL) value. For small scale (several grams) of energetic material, the predetermined number is often 6, although 10 or 20 can be used to increase the accuracy of the TIL level for hundred of grams. However, the TIL value does not refer to a zero probability of reaction. Wild and Von Collani extensively studied the statistical description of the reactivity of energetic materials; they demonstrated that the Bruceton method, which is still in use in other not-European laboratories, is lacking of accuracy and is not scientifically justified. In addition, they clearly showed that their Weibull model can discriminate and explain the sensitivity differences between coarse and fine samples (Wild et al. 2002a,b).

1.4 Submicron and nano explosives

In the past years, the outstanding properties of new nano-materials led the research in energetic materials to embrace this trend. The nano-structuring of classical explosives should enhance their properties and safety. Even if the term “nano” strictly refers to an object with at least one dimension under 100 nm, in this work on energetic material, the term “nano” will refer to nano and submicron-sized particles for the sake of readability, just like n-RDX is an abbreviation for nano or submicron particles of RDX. However, mean particle sizes are always given when available.

1.4.1 Properties and Challenges

The development of new energetic materials led to new synthesized molecules such as 1,3,3-trinitroazetidine (TNAZ), CL-20, Octanitrocubane (ONC), 1,1-diamino-2,2-dinitroethene (FOX-7), Ammonium DiNitramide (ADN) etc. Those newly available materials aim to achieve higher density, increase the processability and attain Insensitive Munitions (IM) characteristics; IM properties actually rely on the whole physic-chemistry of the system. Therefore, the development of powders with controlled particle sizes and morphologies and a well defined surface chemistry, is a whole new facet of the energetic materials largely unexplored at the submicron scale and below. Criteria that are advantageous for new energetic materials include the following:

- high decomposition temperature
- low sensitivities
- no phase transitions under compression or depression
- no autocatalytic decomposition
- no voids from solvents or gas
- mechanical behaviour independent from temperature
- good ratio availability/cost
- easy processing

Compression of gaseous inclusions, cavities and voids, deformation, frictional heating, inter-crystalline shearing and spark discharges are initiation processes which can cause areas of an energetic material to warm up to several hundred Kelvin: these areas are called hot-spots and are deflagration or detonation origins if they reach a critical temperature. Tarver (Tarver et al. 1996) calculated for HMX the critical temperature of different sized hot-spots. For a 2 μm sized hot-spot he calculated a critical temperature of 985 K, whereas the critical temperature for a 0.2 μm sized hotspot already rises to 1162 K.

Risse (Doctoral Thesis 2012) measured a noticeable desensitization towards initiation by friction and electrostatic discharge for n-RDX crystallised by Spray Flash Evaporation (SFE), compared to the raw material (Table 1.2, p. 47). The noticeably lower sensitivity towards friction can be based on the self-lubricating effect, as small particles will tend to occupy small interstices instead of breaking. Sensitivity measurements were also performed on Hexolite, which showed a clear desensitization of the nano-structured explosive (Table 1.3, p. 47).

RDX	Impact [J]	Friction [N]	ESD [mJ]
M5 (raw material)	>3.52	160	120
nano-structured	>3.52	>360	270

Table 1.2 – Sensitivity towards impact, friction and ESD of micron-sized and nano-structured RDX (Doctoral Thesis Risse 2012).

Hexolite	Impact [J]	Friction [N]	ESD [mJ]
micro	6	54	353,6
nano	25,06	72	436,6

Table 1.3 – Comparison of the sensitivity levels of micro Hexolite with those of a nano-sized Hexolite (Doctoral Thesis Risse 2012).

Using a sonocrystallisation process, Bayat and Zeynali (Bayat et al. 2011) succeeded in the preparation of n-CL-20 which was less sensitive towards friction, impact and electrostatic discharge (Table 1.4, p. 47).

Particle size [μm]	Impact [cm]	Friction [kg]	ESD [J]
15	25	6,4	45
0,095	55	No reaction	60

Table 1.4 – Comparison of the sensitivity levels of micro and nano CL-20 (Bayat et al. 2011).

Fathollahi et al. (2007) have studied the particle size effects on thermal decomposition on HMX: as the particle was getting smaller, temperature and the activation energy were decreasing.

However those trends are not always observed. Crystallised from Rapid Expansion of Supercritical Solutions (RESS), several nano RDX lots have been tested by (Stepanov et al. 2011); if both 500 nm and 200 nm RDX are less sensitive toward impact than milled 4 μm RDX, the 200 nm lot is substantially more sensitive than the 500 nm one. As it can be seen in Figure 1.12 p. 48 that minimum of sensitivity to impact is confirmed when coating the powders with a

binder; however that confirmation might reveal that the trend is more due to the intrinsic bulk properties of the particles instead of their surface.

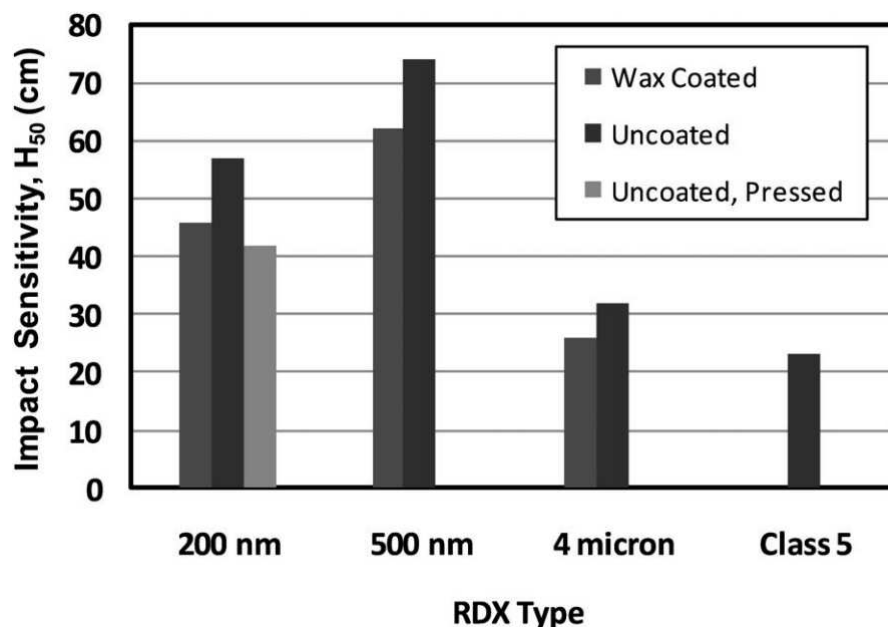


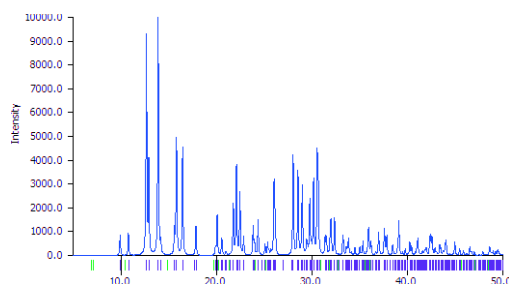
Figure 1.12 – Sensitivities of RDX with various Particle Size Distribution (PSD) (Stepanov et al. 2011).

Beside safety, other improvements can emerge from the nano scale; critical diameter, tunable detonation velocity, delay before the detonation steady state etc. may be improved by the drastic grain size reduction. Energetic nanocomposites are also promising materials improved by a more intimate mixing. Liu Jie et al. (Liu et al. 2014) show that detonation velocities of PBX composition from their milled n-RDX and n-HMX are slightly better while being significantly safer. The burning rates of nitrocellulose was also improved by Zhang et al. (2014) due to the formation of submicron spheres. Recently, Comet et al. (2015) proved that energetic nanocomposites can easily replace the hazardous primary explosives to initiate a secondary explosive: 500 nm n-RDX from SFE were mixed with a nano thermite to initiate the detonation of PETN. The Flame Propagation Velocity (FPV) of composites made of n-WO₃/n-Al/n-RDX can be tuned from 0.2 km/s to 3.5 km/s through their explosive content; in the same conditions, n-WO₃/n-Al with μ-RDX exhibit unstable regimes from 187 m/s to 733 m/s, whereas the n-WO₃/n-Al/n-RDX composite deflagrates at a constant velocity of 2529 m/s. Those results and other unpublished ones of our laboratory confirm the drastic reduction of the critical diameter with the decrease of particle size.

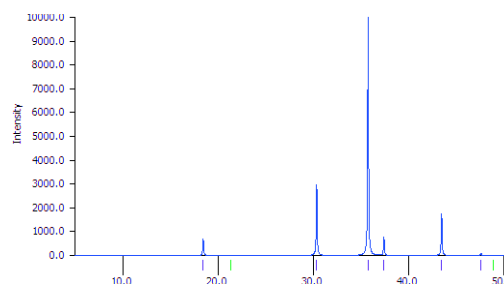
1.4.2 Challenges of the characterization of energetic materials

Some of the characterization techniques previously described in Section 1.3.1 p. 36 are difficult to apply on nano energetic material, due to their sensitivity toward heat, or toward vacuum, or their organic nature. Molecular solids are by their nature called soft matter, due to the type of bonds involved to create their crystalline structure: the dipole forces holding the molecules together are weaker than the covalent bonds in metals or the ionic bonds in ionic crystals.

XRD Solid organic explosives are molecular crystals: the crystallographic positions are occupied by the molecule and not just a single atom. XRD diffraction of molecular crystals produces much more reflections –up to thousands– for the very complex protein crystals. For instance in Figure 1.13, the XRD pattern of CL-20 exhibits much more diffraction lines than the magnetite Fe_2O_3 . Moreover,



(a) CL-20 diffraction pattern from Meents et al. (Meents et al. 2008).



(b) magnetite diffraction pattern from WH. Bragg (Bragg 1915).

Figure 1.13 – Examples of computer generated XRD patterns, both with the same broadening.

at the nano scale, the diffraction peaks are broadened. Line broadening in diffraction stems from instrumental and physical broadening; the latter is due to size effect and internal strain inside the lattice. Young and Desai (Young et al. 1989) described size broadening β_{size} as a Gaussian contribution of the Scherrer's equation:

$$\beta_{size} = \frac{\lambda K D_V}{\cos(\theta)} \quad (1.2)$$

where K is the shape factor and D_V the apparent volume weighted domain size. Stokes and Wilson (Stokes et al. 1944) defined the maximum strain definition as a dependency of the broadening:

$$\varepsilon = \frac{\beta_{strain}}{4 \tan(\theta)} \quad (1.3)$$

Therefore, the broadening from the material is simply:

$$\begin{aligned}\beta_{observed} - \beta_{instrumental} &= \beta_{strain} + \beta_{size} \\ &= 4\varepsilon \tan(\theta) + \frac{\lambda K D_V}{\cos(\theta)} \\ \Leftrightarrow \beta_{strain} \cos(\theta) &= 4\varepsilon \sin(\theta) + \lambda K D_V\end{aligned}\quad (1.4)$$

Plotting $\beta \cos(\theta)$ as a function of $\sin(\theta)$ should give an affine function where the slope is directly related to the strain: they are known as Williamson-Hall plot. However, it requires to index and fit several reflection peak. Therefore, XRD patterns were also analysed by the Full Pattern Matching (FPM) method using the software Fullprof. The peaks shape was fitted with a Thompson-Cox-Hastings pseudo-Voigt convoluted with axial divergence asymmetry function (Finger et al. 1994). When compared to mathematical fitting features in data analysis software, the FPM technique as implemented in many XRD analysis software has the great advantage to take into account the specificity of XRD patterns, such as complex shape functions and the existence of the $K_{\alpha 2}$ radiation. Indexing many peaks by FPM gives a wider understanding of the material and increase the precision of the strain extracted of the Williamson-Hall plots. However, Williamson-Hall plot were found to be not always linear thus were not used afterwards. The assumptions leading to the Scherrer's equation and the final Equation (1.4) are not satisfied. That's why the accurate and complex Rietveld refinement method with size-broadening refinement for apparent crystallites morphology based on a spherical-harmonics representation (Balzar et al. 2005; Popa 1998; Popa et al. 2008) calibrated with LaB_6 as implemented in Fullprof was used.

SEM Organic explosives are sensitive towards heat and their submicron-sized emphasizes even more that discrepancy due to a higher surface/volume ratio; under vacuum, that heat from the electron beam can not be transferred to the surrounding of the surface. The gold coating is accordingly increased to approximatively 10 nm to increment the heat transfer from the material to the sample holder. The energy from the beam can also be tuned to reduce the degradation of the sample. However, electrons has to interact with the sample surface in order to have enough contrast and so spatial resolution. Due to the low density of organic molecular crystals, the effective tension required is usually high, around 15 kV at working distances around 5 mm. The stabilization with gold deposit improves the imaging of n-RDX allowing magnifications up to 10.000x. Further magnifications alter the material and do not allow a complete and correct data acquisition.

The damages of the electron beam on sensitive organic samples can be avoided or diminished by working at higher pressures (up to 1 Torr–50 Torr

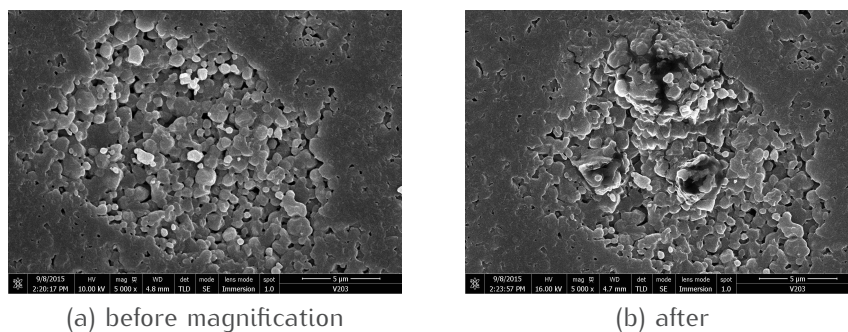


Figure 1.14 – High vacuum SEM imaging on a n-RDX pressed pellet coated with gold.

instead of 1×10^{-5} Torr to 1×10^{-7} Torr) with adjustable relative humidity up to 100%. An Environmental Scanning Electron Microscopy (ESEM) FEG FEI XL30 was tested at the CLYM laboratory (Lyon, France) showing encouraging results about the increased stabilization at 2 Torr. As it can be seen in Figure 1.15, n-RDX without any coating exhibits at 2 Torr much more contrast compared to classical SEM with gold deposit.

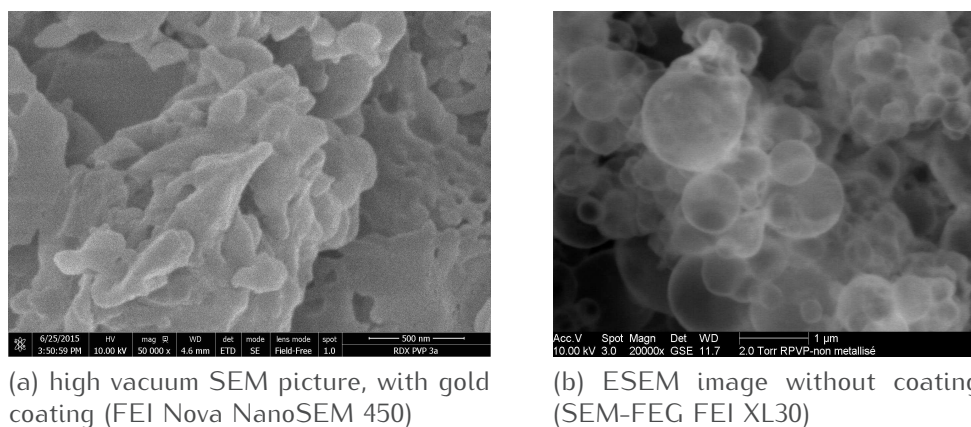


Figure 1.15 – Comparison between high vacuum SEM imaging and at 2 Torr from ESEM on the same n-RDX sample

BET Prior to the measurement by gas injection, adsorbed water or organic gas have to be removed. This can be done by heating under vacuum or under a flow of dry, inert gas. The quality of the degassing influences directly the accuracy of the surface area calculated. As previously depicted, nano energetic materials are sensitive to heat and to vacuum, thus it can be expected to degrade them at the degassing step.

While using Krypton to gain in accuracy and access to smaller pores, BET results in Table 1.5 demonstrate the inaccuracy of BET measurements on n-RDX. At 100 °C the mass loss is almost one magnitude higher which may indicate a good degassing, but the specific surface area is decreasing leading us to the conclusion that the powder is starting to be affected by sintering.

degassing	mass loss	S_{BET}	extrapolated diameter
↗ 2°C/min – 50°C 10min – – ↗ 1°C/min – 80°C 1h –	0.1%	3.28 m/g	1.0 μm
↗ 2°C/min – 50°C 10min – – ↗ 1°C/min – 100°C 1h –	0.8%	3.09 m/g	1.1 μm

Table 1.5 – BET measurements on n-RDX with Kr

DLS Depending on the anisotropy and polydispersity of the system, the data interpretation may exhibit an angular dependence. For instance, small spherical particles do not have any anisotropy hence no angular dependence; the ideal case of spherical particles is usually not effective and such samples will exhibit an angular dependence. An optimum angle of detection exists for each particle size distribution and particle morphology. For a polydisperse sample and at certain angles, the scattering intensity of some particles will completely overwhelm the weak scattering signal of other particles, thus making them invisible to the data analysis at this angle. Furthermore, even if most of the organic explosives are not soluble in water, nitro and nitramine groups trend to interact strongly; energetic colloids are not stable in water and aggregates easily with quick sedimentation. Experiments have been done using the Zetasizer from Malvern. Even if the addition of PolyVinylPyrrolidone (PVP) enhances the stabilization, no reproducible measurements could have been performed as it can be seen in Figure 1.16.

DSC When gaseous species are reactive towards the decomposing substance, it leads to the autocatalytic acceleration of the reaction rate. Therefore for energetic materials, the assumed constant pressure is not satisfied for closed crucibles; consistent kinetic analysis can be acquired only by effectively removing

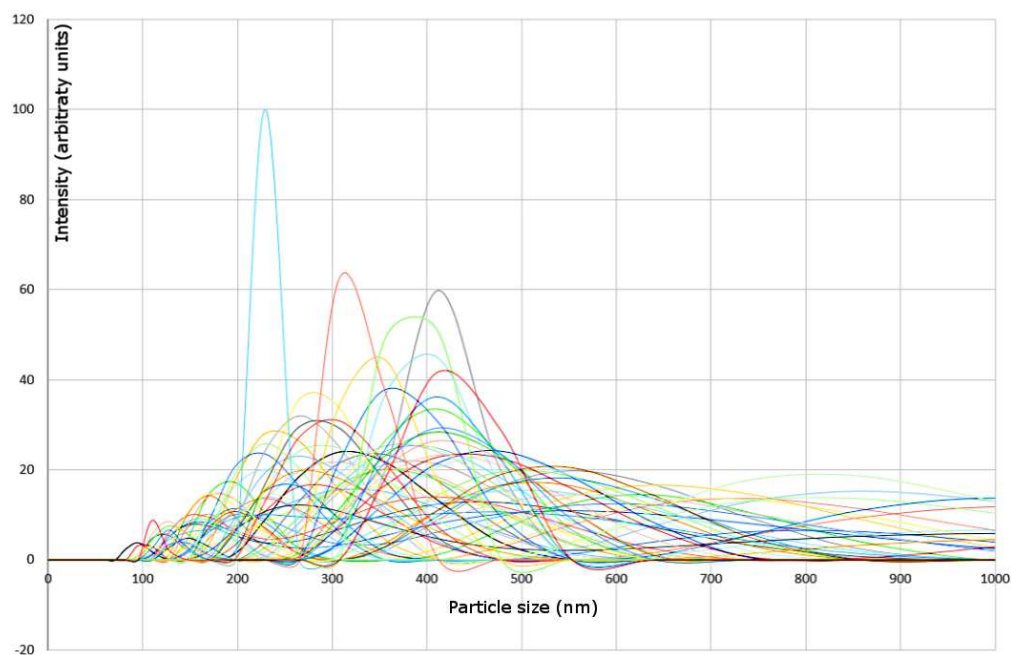


Figure 1.16 – All Dynamic Light Scattering (DLS) results acquired from *n*-RDX with 5wt% of PVP: even if this figure contains data with different experimental conditions such as duration of the ultrasonic bath or the dilution, none of the PSD could have been found reliable.

reactive gaseous products. Long et al. (Long et al. 2000) clearly demonstrated that the competition between liquid and gas phase decomposition decreases over time, the activation energy in both pierced and closed pan DSC experiments from ~ 200 kJ/mol to ~ 140 kJ/mol, whereas open pan DSC and TGA experiments showed a constant value of ~ 100 kJ/mol.

1.4.3 Specific health and safety hazards

A wide variety of nano materials is now being produced, including nanoparticles as well as nanofibers, nanowires, and nanosheets, and their range and types are continually expanding. The increase of the nanomaterial uses in every day products makes the human exposure inevitable, thus asking the question of nanotoxicology. To prevent the uncontrolled penetration of foreign substances, the human body has several barriers such as epithelial cells and mucus secretion. While the protective mucus of the lung trap micron-sized particles, nanoparticles are small enough to reach the deep lung and even further the air-blood barrier (Fröhlich et al. 2014). Epidemiological studies showed that exposure of humans to ultrafine particles ($<2.5 \mu\text{m}$) in the air increased pulmonary morbidity and

mortality. Nanoparticles can also be cleared from the bronchial epithelium and then absorbed in the gastrointestinal tract. However, particles morphology, metric-related characteristics and many other physicochemical properties largely influence their toxicity. For organic particles, the solubility of the compound in its environment is a major issue since unitary molecules can directly disturb the proteins activity. The report of Boyer et al. (2007) written for the SERDP and ESTCP –US Department of Defence’s environmental research programs– provides a comprehensive overview of the toxicity of RDX and CL-20. The toxicity of CL-20 for soil invertebrate population is quite high with only 0.02 mg CL-20/kg of soil to damage it significantly, whereas 44 mg RDX/kg soil–660 mg RDX/kg soil is harmless. For fish and aquatic invertebrates, CL-20 may be more toxic than RDX; but CL-20 is substantially less toxic than RDX to plants and birds: as little as 5.8 mg RDX/kg soil caused adverse effects for some plant species, while 10 mg CL-20/kg soil had no effect. Unfortunately, no studies on the toxicity of CL-20 in mammalian species –including humans– have been published. In contrast, the US Environmental Protection Agency (EPA) has established a reference dose (RfD) of 0.003 mg RDX/kg body weight/day for oral exposure based on the results of toxicity studies on rats; RDX has also been classified as possible human carcinogen, based on liver tumours in mice exposed for 2 years to 7 mg RDX/kg body weight per day.

About the pyrotechnic safety, the articles from R.4462-1 to R.4462-36 of the Code du Travail (Labour Code) regulates the practices of any work involving the creation, study, experimentation, control, packaging, storage or destruction of energetic compounds or any object containing pyrotechnic parts. In addition to the Document Unique, a legal document listing all actual potential risks, the employer has to redact a safety study for each pyrotechnic activity, with a validity of five years: the content of this pyrotechnic safety study is regulated by the decree from the 7th of November 2013 (modified in July 2014). The accidental potential modes of degradation of the energetic material has to be identified and their effects on human life determined. A probability of accident is estimated and the area of effect is identified then segmented according to the lethality; additional countermeasures are established to reduce the exposure (probability) and the consequences of an accident. At NS3E, each laboratory room has been evaluated to confine the risk inside it. The quantity of energetic material is also limited according to its stability and equivalence to TNT; in many cases only five grams (TNT equivalent) is allowed to be handled per room. The number of simultaneous workers is also limited while studying energetic material, with usually a maximum of two persons. The compounds processed for the first time by SFE are classified in the most restrictive class until the sensitivity has been determined: therefore, only one gram is recovered with a

conductive strap to avoid electrostatic discharge. In France and for the DoD activities, the Inspecteur de l'armement pour les Poudres et Explosifs (IPE) has the authority to control and delegates experts on pyrotechnic safety: the IPE frequently writes open letters (<http://www.defense.gouv.fr/dga/liens/poudres-et-explosifs/lettre-de-l-ipe/lettre-de-l-ipe>) to announce legislation changes, remind or dictate the good practices and list all recent pyrotechnic accidents from civilian or military uses.

1.5 Summary of the Chapter

The energetic material is a wide group which includes mixes of metals and oxides (thermites), amorphous materials (propellants) and organic or salt crystals (explosives). The present work focuses on a few organic secondary explosives: 1,3,5-trinitroperhydro-1,3,5-triazine (RDX), 2,4,6,8,10,12-hexanitro-2,4,6,8,10,12-hexaazaisowurtzitane (CL-20) and octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX). The RDX is a compound of reference still extensively used for applications but also research studies; it has only one crystalline form at ambient pressure and is soluble in acetone, sparingly soluble in ether and ethanol but almost insoluble in water. Several analysis methods were tried because the degradation of the sample is often a source of limitations when dealing with energetic organic crystals. The Dynamic Light Scattering (DLS) needs a stable suspensions without agglomeration nor Ostwald ripening. Under the electron flow in electronic microscopy, the energetic samples heat up and are decomposed. Environmental Scanning Electron Microscopy (ESEM) is a more suitable technology to investigate the particle size and shape, due to the low vacuum able to dissipate heat.

The measurement of the Particle Size Distribution (PSD) is crucial to anticipate the properties of the material and to understand their creation. In addition to the previously mentioned issues, each characterization method measures an unique size; on DLS a hydraulic diameter is determined where the particles' agglomeration and the layers of solvating are taken into account. Electron microscopy techniques provide a direct visualization of particles and are therefore favoured. Finding a suitable and accurate method to establish the Particle Size Distribution (PSD) was the first challenge of the project and is further described in the Chapter 3.

This trend to easily agglomerate, growth, decompose etc. comes from the intrinsic nature of secondary explosive: organic crystals are also called soft matter. Their crystallisation at a nano scale has been a long-standing issue over several decades, and the result depends on the chemical nature of the compound. Therefore, RDX has been extensively studied and crystallised by

almost all the known techniques from other applications in the field of chemical engineering. The following review on processes which led to reduced size of RDX is necessary to provide a global comprehension on the specificities of RDX crystallisation.

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Chapter 2

Production of Nano Explosives

The crystallisation of a compound or several ones is the phenomenon of transition between the liquid, gaseous or even solid state to the crystalline state where matter possesses long range order and symmetry. Crystallisation can be used to adjust the physical properties and the morphology of a substance. Crystallisation involves the formation of nuclei and then their growth; when a solution is supersaturated, its thermodynamic equilibrium is reached through nucleation and growth. To favour smaller particle size, the trend is to increase nucleation rate, for instance through increasing supersaturation, to reduce crystal growth and avoid any aggregation. Most of the crystallisation techniques are based from solution but crystallisation processes from the melt and from the gaseous phase are also known (van der Heijden et al. 2005). Quite a few were tested on energetic materials; the following bibliography is meant to be a comprehensive review of the crystallisation of RDX and of similar energetic compounds at submicron or nano scale.

2.1 Wet production methods

2.1.1 Crystallisation from solution

The most commonly used technique is the crystallisation from solutions. Depending on the creation of supersaturation, distinctions are made between cooling, evaporation, vacuum cooling, drowning-out and reaction crystallisation. The study of the solubility of the compound is the key to determine which crystallisation process can be used: for instance if the solubility is not very temperature dependent, evaporation will be more effective than cooling (Figure 2.1 p. 62).

Fedoroff et al. (1966) indicates that the RDX solubility in acetone is divided by 4 by cooling from 60 °C to 0 °C. PANT et al. (2013) used all standard techniques

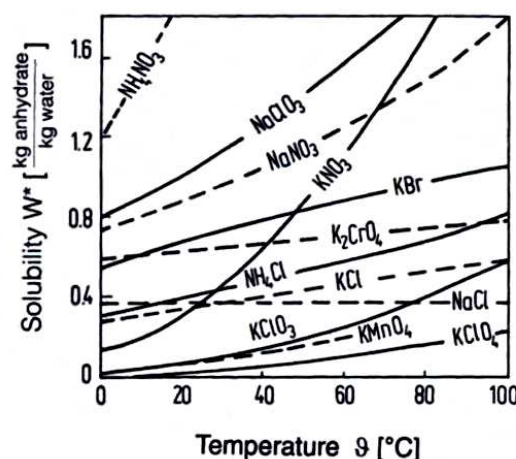


Figure 2.1 – Solubility curves for different substances (Mersmann 2001).

available to recrystallize RDX into submicrometer crystals “in a beaker”: the smallest size was obtained when the anti solvent were added to a highly supersaturated solution cooled down, while applying ultrasonication and stirring. Achieving a high level of supersaturation results in a higher nucleation rate, but aggregation rises at elevated rates; for this solvent/compound system, they produced smaller particles, and reduced the agglomeration by the sonication. Particles are finally obtained by drying. This method may be suitable for industry, however, the minimal size obtained is only 850 nm under tough condition, with a yield of 60% and rod shaped crystals.

Kumar et al. (2014) succeeded to produce finer RDX particles by quickly injecting a very small volume (100 μL) of RDX dissolved in acetone into ultra pure water: the smallest mean particle size was 38 ± 15 nm by SEM for the highest temperature (70 $^{\circ}\text{C}$) and lowest concentration of RDX in acetone (5 mM). It is worth to mention that DLS measurements were found to be not reliable when compared to SEM analysis, which can be explained by the lack of surfactant stabilizing the colloid. This technique was also applied on HMX (Kumar et al. 2015) with a particle size around 30 nm and the same conclusions were drawn out.

Bayat et al. (2015), through an optimization of the micro-emulsion process, crystallised 80 nm plate-like β -CL-20 particles. The severe agglomeration and plate-like morphology might be due to the freeze drying, then washing of the micro-emulsion. Gao et al. (2014b) recrystallized FOX-7 in ethyl alcohol within a submicrometric range: SEM pictures show an irregular plate-like morphology and therefore highlight the inconsistency of the unique mean particle size of 340 nm claimed. Particles exhibit also a certain degree of agglomeration which

can be probably explained again by the lack of a surfactant and the air-drying.

Luo et al. (2015) reached an impressive size of 30 nm of RDX. They used a surprising technique where RDX is dispersed in bacterial cellulose. The lowest particle size was obtained with 71 %RDX/gelatine mix; however, increasing the content of RDX leads to an increment of the particle size and the maximum of RDX loading tested was 91 % for a particle size of 50 nm. The sensitivity of that composite towards impact and friction is divided by two therefore asking the legitimate question of the reactivity. Nevertheless, further efforts could be done to replace the bacterial cellulose with energetic matrix.

Crystallisation in solution allows the formation of large crystal by growth, thus allowing more parametric studies about the influence of solvents ; for instance (Li et al. 2015c) has studied the importance of temperature and supersaturation for the crystallisation for HMX in γ -butyrolactone, revealing that low temperatures and highly supersaturated solutions trend to increase the defects in HMX crystals.

2.1.2 Solvent substitution using reverse micelles

Dabin et al. (1999) have developed an ingenious method to prepare nanometre RDX using a simple technique: the crystallisation is triggered by a solvent substitution, and the nanometre scale is obtained by restricting the reactor volume to such a scale with reverse micelles. NaAOT (Sodium 1,4-bis(2-ethylhexoxy)-1,4-dioxobutane-2-sulfonate) into isooctane forms reverse micelles, then RDX in DMF is added to one solution containing these micelles, and water to another solution of micelles. Both are finally mixed together to form the nano RDX with a diameter of 70 nm to 100 nm.

2.1.3 Sol-Gel

Energetic materials processed by sol-gel method, are desensitized by embedding in a matrix, usually a silica matrix. Developed by Gash et al. (2000), Tillotson et al. (2001), and Tillotson et al. (1997), the silica-explosive gel is prepared by dissolving the energetic compound, the silica precursor and a catalyst, in a co-solvent. After the gelification, an anti-solvent of the explosive is injected to replace the solvent in the pores and precipitate the explosives in that silica matrix. By drying with heating or at low pressure, a xerogel with higher density is obtained; if supercritical CO₂ is used to extract the solvent, an aerogel with low density is formed. Therefore, the nanostructuring of the explosive comes from the porous matrix: cavities of mesoporous gels are from 2 to 50 nm large, less than 2nm for microporous gels. Macroporous materials have pore diameters of greater than 50 nm (Rouquerol et al. 1994).

RDX/Resorcinol-formaldehyde (RF) nano-composite has been synthesized (GUO Qiu-xia 2006): 38 nm large nano-RDX has crystallised in an RF aerogel matrix with a surface area of $551.5 \text{ m}^2/\text{g}$ (measure taken without RDX). Wuillaume et al. (2014) trapped AP and RDX in a mesoporous low-density energetic organogel. At the impact test negligible decrease of sensitivity has been measured: 75 wt% RDX nano gels and macro gels have the same sensitivity and the 90 wt% nano gels are even more sensitive than the macroscopic counterparts. When compared to pure RDX, the 90 wt% nano gels are not desensitized. However, SSGT performed on pressed gels (95% TMD) revealed an improvement of the sensitivity for the 90 wt% RDX nano-formulation. That nano gel exhibits an uncommon micro-structure of sheets, with micron-sized particles potentially formed by nano primary particles: the lack of desensitization on the loose powder may be explained with the sensitization by the sheet-like shape counteracted by the presence of the gel coating each nanoparticles.

Li et al. (2015a) used a better energetic matrix –Glycidyl Azide Polymer (GAP)– with a maximum of 40 wt% of RDX; they noticed a lower sensitivity than the physical mix. However, the claimed nano size is only deduced from porosity without RDX and from XRD patterns which only gives a mean coherence length. They also created NitroCellulose (NC)-RDX-AP nano composites by a technique similar to sol-gel (Jin et al. 2015); the matrix consist of the NC itself solidified by micron-sized AP crystals and cross-linked with Toluene Dilsocyanate (TDI) and Dibutyltin dilaurate (DBTDL), whereas RDX is dissolved in acetone inside that template. The gel and the crystallisation of RDX is triggered by supercritical CO_2 drying. Even if the sensitivity and the density were not improved, the increase of the heat of explosion measured and the originality of the approach make promising the formation of nano-composite based entirely on energetic materials through chemical binding.

2.1.4 Melting

Many high energetic materials degrade very closely to their melting point. Therefore, only a few such as TNT or TNB can be used in their molten state, since the melting temperature is at least $100 \text{ }^\circ\text{C}$ far from the exothermic decomposition. The melt-cast process of TNT-based composition is used for shaping charges or loading them into ammunitions since WW I. Crystallisation from an emulsified molten explosive is an innovative technique used by Anniyappan et al. (2015). 2,4,6-triazido-1,3,5-triazine or cyanuric triazide (CTA) has been processed at $95 \text{ }^\circ\text{C}$ to crystallise as micron-sized agglomerates. CTA is a promising primary explosive compliant with the new REACH legislation (*Regulation (EC) No 1907/2006 on the Registration, Evaluation, Authorisation and Restriction of Chemicals (REACH) and setting up a European Chemicals Agency 2007*) forbidding the use of heavy

metal based materials. Further investigation with surfactants might lead to smaller particles by counteracting the high viscosity of molten droplets.

2.1.5 Milling

Redner et al. (2006) developed a batch wet-milling process, producing submicrometer RDX. A mixture of water, isobutanol, a dispersant and RDX is filled into a unspecified mill, resulting in a minimal mean particle size of 310 nm and a crystallite size of about 65 nm. Several milling issues were mentioned such as the yield initially of around 25% and the importance of the residence time and the drying step.

Liu et al. (2014a, 2013) studied the effect of drying nano-RDX and HMX samples under various conditions. They first obtained nano-RDX in solution from a mixture of water, ethanol, isopropanol and RDX. The suspension is put in a bi-directional rotation mill for 6h. Just as Redner experienced, the drying is the critical point to get a nano powder. They dried the RDX under different conditions: freeze drying and supercritical drying led to quite impressive results, with medians at 160 nm and 200 nm respectively from a solution containing an average particle size of 64 nm. After RDX and HMX, CL-20 was successfully processed the same way resulting in a median size of 180 nm determined by SEM (Liu et al. 2014b). For the three compounds, nano powders are less sensitive than their micron-size counterparts.

Spray drying is a less energy intensive drying method studied by Patel et al. (2015). RDX and CL-20 have been bead milled from water with addition of isobutanol and Polyvinyl alcohol (PVOH) to stabilize the colloid by dispersion and coating, and then an unknown polymeric binder is added just before drying the slurry by spray drying. Mean particle sizes down to 400 and 200 nm respectively have been measured by DLS for RDX- and CL-20-based composites after milling. However, no PSD curve has been provided nor dispersion of the results indicated. It has been noticed that for particles of CL-20 at 200 nm, the α phase is obtained. From the same team, nanoscale cocrystal of CL-20:HMX 2:1 has been prepared by bead milling an aqueous suspension of ϵ -CL-20 and β -HMX in a 2:1 stoichiometric ratio (Qiu et al. 2015a). The progressive conversion of raw materials into the cocrystal is achieved after one hour, resulting in a particle size lower than 200 nm. However, not much attention has been paid to the drying effect of large scale batch; SEM and XRD were made on a drop dried at room temperature, and it is likely that the drying of several grams of such molecular crystal will behave differently. Furthermore, the accuracy of the XRD technique does not allow to conclude that a complete conversion into cocrystal has occurred, but rather indicates that the percentage of ϵ -CL-20 and β -HMX is

lower by 10% approximatively. Full quantification by Rietveld or Full Pattern Matching methods would have been relevant to follow the conversion with time.

2.2 Dry production methods

2.2.1 Physical Vapor Deposition (PVD)

Frolov and Pivkina have developed together a vacuum condensation process for high energetic material first reported in 2002 (Frolov et al. 2002; Frolov et al. 2010; Pivkina et al. 2004). Vacuum deposition of ammonium nitrate (AN), RDX and a composite AN-RDX was performed on a cooled quartz-glass substrate. The mean particle size was directly measured from AFM: a size of 50 nm was obtained for the three materials, even after processing the nano-powder (removing from the quartz substrate and pressing into tablets).

Mil'chenko et al. (2015) went further in the Physical Vapor Deposition (PVD) process by the deposition of TATB, HMX, RDX, PETN and BTF as thin layers on several substrate such as Plexiglas and copper while changing operative parameters. Critical thickness of the detonating layer is an order of magnitude lower; the sensitivity toward impact and friction is barely mentioned as being similar to the raw materials but the sensitivity to Light Amplification by Stimulated Emission of Radiation (LASER) has been substantially increased.

Therefore, the PVD technique is greatly suitable for "pyrotechnic integrated circuits", whereas mass production of loose powder is not economically viable.

2.2.2 Electropray

Radacsi et al. (2011) crystallised submicrometer RDX using an electropray. A solution of RDX-acetone is sprayed through a nozzle electrically charged to a grounded plate: the droplet surface is charged, increasing their surface energy and so triggering their fission into smaller droplets. This Coulomb fission phenomenon and the evaporation of the solvent lead to crystallisation and the deposit of non agglomerated particles. The tweaking of the characteristics of the nozzle and the potential difference resulted in various morphology of RDX particles: for instance, micrometer hollow spheres of agglomerated RDX were produced. The minimal mean size obtained was 400 nm: that submicrometer RDX exhibited a clear insensitivity towards friction, but with the same impact sensitivity as conventional micron-sized RDX (Table 2.1, p. 67).

Reus et al. (2014) then processed bi-component systems: proteins and RDX/TNT. XRD patterns of the final products are mentioned to be different from the ones of the raw material, which seems to indicate either a strong

RDX	Impact [J]	Friction [N]
Conventional	7.5	120
submicrometer	10	>360

Table 2.1 – Comparison of the sensitivity levels of conventional and 400-nm large RDX.

degradation or a cocrystallisation. Infrared definitely demonstrates a critical partial decomposition of both RDX and TNT due to the electro spray and the same phenomenon has likely happened for Radacsi et al. too. Whatever was really obtained, Reus crystallised very small particles, estimated by me to be under or around 100 nm for any initial ratio of TNT/RDX. AFM could have been much more informative about the size and shape of such nanoparticles already well dispersed on a substrate. Sensitivity tests have been performed on those degraded materials, which were found to be as insensitive as TNT.

Electrospray can create a fine spray of micron-sized charged droplets re-peeling each others, ideal for crystallisation; the high voltage needed is a major handicap for processing sensitive powders such as energetic materials containing nitro groups.

2.2.3 Plasma

During his PhD project (Radacsi 2012), Radacsi used an innovative and advanced technique to crystallise submicrometer RDX: a Collison nebulizer aerosolizes a RDX-acetone solution to a Surface Dielectric Barrier Discharge (SDBD) plate where a cold plasma disrupts the droplet by the Coulomb fission. Like the electro spray, one droplet should crystallise into a unique single-crystal. The minimal mean size obtained was 500 nm, with a range from 200 nm to 900 nm and with prismatic or spherical shapes. Again like the submicrometer powder obtained from electro spray, the 500 nm-sized RDX has been desensitized to friction but not to impact (Table 2.2, p. 67).

.RDX	Impact [J]	Friction [N]
Conventional	5	144
submicrometer	5	>360

Table 2.2 – Comparison of the sensitivity levels of conventional and 500-nm large RDX (Radacsi 2012).

2.2.4 Supercritical/Gas Anti-Solvent precipitation

Supercritical Anti-Solvent precipitation (SAS) uses the same principle as liquid crystallisation, substituting the liquid anti-solvent by a supercritical fluid. The very high diffusivity of supercritical fluids leads to a rapid supersaturation and so to a sudden precipitation. Various apparatuses are used in SAS: a specific one is the Gas AntiSolvent (GAS) precipitation, where the liquid solution is first loaded into the vessel, before the addition of the supercritical anti-solvent. For RDX, CO₂ is a correct supercritical anti-solvent. Gallagher et al. (1992) first investigated GAS process of RDX in 1992. Supercritical CO₂ was injected into RDX-cyclohexanone solution at various injection times, injection quantities and temperatures: in this first use of GAS for RDX, a lot of different particle size distributions and morphologies were obtained, but none under the micrometer size. Since then, several process derived from the GAS process, and which could be referred as SAS sub-process, have been used to reach the submicrometer and nano scale for energetic materials. But from 1992, no GAS/SAS process has been reported to produce energetic materials to a size lower than the micron (Jung et al. 2001; Lee et al. 2009, 2011b; Teipel et al. 1997), excepted for 5-nitro-1,2,4-triazol-3-one (NTO) by Lim et al. (1998) (Reverchon et al. 2005).

2.2.5 Aerosol Solvent Extraction System (ASES) process

Aerosol Solvent Extraction System (ASES) process involves spraying the solution to precipitate through an atomization nozzle into supercritical CO₂. Lee et al. (2011b) used GAS and ASES apparatus to crystallise β -HMX: undesirables shapes (needle-like, irregular and aggregated) were produced by ASES at any operating conditions, whereas GAS led to regular shape and the most desired β phase. Dou et al. (2013) sprayed RDX dissolved in DMF obtaining micron-sized particles highly polydispersed. However, submicron-sized polymers and biopolymers produced by ASES have been reported since the nineties by Dixon et al. (1993) and Reverchon (1999). Nevertheless, that technique could be used on NC based composite due to its polymer-like behaviour.

2.2.6 Solution Enhanced Dispersion by Supercritical fluids (SEDS)

Solution Enhanced Dispersion by Supercritical fluids (SEDS) process was developed and patented by the Bradford University to achieve a smaller droplet size compared to the previously described SAS methods. For SEDS process, a solution with the compound solvated is sprayed into supercritical anti-solvent gas (CO₂ for RDX) through a nozzle with two coaxial passages: this technique

can be seen as a specific implementation of the ASES process, where CO₂ is introduced through the nozzle continuously with the solution. Shang et al. (2014) produced by SEDS spherical RDX particles with a mean particle size of 770 nm, therefore finally lowering the particle size under the micron.

2.2.7 Particles from Gas-Saturated Solutions (PGSS)

Both patents “Conditioning of finely divided crude organic pigments” (1984) and “Finely dispersed carotenoid pigments prodn. - by dissolving carotenoid in a supercritical gas, pref. carbon di:oxide, and dispersing the soln. in an aq. colloidal matrix” (1981) first described a procedure that today is called Particles from Gas-Saturated Solutions (PGSS). The PGSS technique consists in dissolving a compressed gas into a solution of the substrate in a solvent, then passing it through a nozzle: the sudden decompression leads to crystallisation thus to the formation of solid particles. Although this method is widely used at large scale with a wide range of products from inorganic powder to pharmaceutical compounds (Pourmortazavi et al. 2005), nothing has been reported (Jung et al. 2001) concerning energetic materials processed by PGSS.

2.2.8 Rapid Expansion of Supercritical Solutions (RESS)

The RESS concept has been first described by Hannay and Hogart more than a century ago (Hannay et al. 1879) but studied by Krukonis (1984) and the Battelle Institute research team (Matson et al. 1987a,b). The RESS process consists in spraying in a lower pressure chamber (60-0 bar) through a nozzle a supercritical (sc) fluid containing the substrate. The sudden drop of pressure leads to rapid nucleation and so small (from micron- to nano-sized) particles which are finally collected. The use of a supercritical fluid like CO₂ allows the direct production of a dry and pure powder. Teipel et al. (1997, 2001) first reported the use of RESS for energetic materials: 10 µm large TNT particle were crystallised in those preliminary experiments. They mentioned parameters which influence strongly the crystallisation from a RESS apparatus: pressures, temperatures, geometry of the nozzle and mass flow. Stepanov in the group of Krasnoperov succeeded in the fine tuning of the RESS process to prepare dried n-RDX (Stepanov 2003, 2008; Stepanov et al. 2006, 2005). The formed RDX particles had a mean particle diameter ranging from 110 nm to 220 nm and an irregular spherical morphology. He performed an up-scaling of the RESS process in order to increase the production capacity of RDX to 6 g/h but with a CO₂ consumption of 35 kg/h. By RESS, a slight sensitization to impact and shock stimuli of the 200 nm nano-RDX occurred compared to 500 nm n-RDX (Stepanov et al. 2011).

CL-20 has also been reported to be processed by RESS from trifluoromethane (CHF_3) (Reverchon et al. 2005): sc-CHF_3 has similar thermodynamic properties and is a better solvent of CL-20 than sc-CO_2 . Only micron-sized particles were produced and no article reporting the results could have been found. Changing the solvent is a line of research followed by Lee et al. (2011a) using compressed liquid DiMethyl Ether (DME) for RDX. The parametric study points out the role of inlet pressure and temperature and the nozzle diameter: increasing any of those three parameters increases the particle size. Therefore, the two minimal mean particle sizes of 370 and 360 nm were obtained for the lowest mass flow rate of 0.37 and 0.85 g/s of DME.

2.2.9 RESS-AS (or RESOLV)

After the success of the RESS process, Essel et al. developed a new method from that technique, called Rapid Expansion of Supercritical Solutions into an Aqueous Solution (RESS-AS) first reported in 2010 (Essel et al. 2010). Rapid Expansion of Supercritical Solutions into an Aqueous Solution (RESS-AS) uses the versatility of the RESS process, spraying into an aqueous solution containing a dispersant and/or growth inhibitor (Kuo et al. 2011). They reported (Essel et al. 2012) a production of 30 nm sized RDX using a pH 7-stabilized solution, although a polymer coating (PEI or PVP) was necessary to avoid any agglomeration and so stabilize the colloid from the Ostwald ripening observed when no polymer was added. No sensitivity tests have been reported about any nano-powder which could be obtained from those colloidal suspensions.

2.2.10 Light Amplification by Stimulated Emission of Radiation (LASER) Ablation

Gottfried et al. (2012) successfully produced for the first time nanoparticles of RDX using LASER ablation. Near-infrared, nanosecond pulsed LASER has been focused on military-grade RDX pellets: Scanning Mobility Particle Sizer (SMPS) and SEM analyses showed a particle size distribution around 64 nm for 200 mJ pulse and 75 mJ pulse.

2.2.11 Ultrasonic Spray Pyrolysis

Since the nineties, spray crystallisations and synthesis have been performed using several atomizers, and among them piezoelectric transducers (Messing et al. 1993; Okuyama et al. 2003). As a spray technique, the goal is to produce one particle per droplet, but here the crystallisation is controlled by the drying step, an oven just after the atomization. Kim et al. (2011a), Kim et al. (2011b),

and Spitzer et al. (2011, 2010) both developed an apparatus to produce dried submicrometer RDX from an ultrasonic transducer. After the droplet generation, the solvent is evaporated by thermal gradient applied on the flux pulled by a pump. Highly agglomerated particles 200 nm–500 nm were produced. Gao et al. (2014a,b) used the same experimental setup with the exception of the addition of a thermal gradient in the furnace, in order to produce 78 nm FOX-7 particles, and submicron-sized CL-20:HMX cocrystals.

2.2.12 Spray Drying

The development of spray drying (Broadhead et al. 1992; Stein 1973) has been expanding since many years and has recently become a suitable commercial solution at both R&D and industry scales to produce dried particles from microns to nanometres. The pyrotechnic community quickly discerned the advantages of this simple technique to process energetic compounds as pure and composite materials.

The process sprays a solution containing a dissolved compound or particles in suspension into a hot gaseous stream (air or nitrogen) thus crystallising into particles and/or drying the granules. van der Heijden et al. (2008) has proven that spray drying is able to crystallise finer RDX particles (“from 400 nm and larger”) than their technique of precipitation into anti-solvent (1 μm to 10 μm). Qiu et al. studied the crystallisation of energetic compounds using the spray drying with ultrasonic (Qiu et al. 2011) or pneumatic (Qiu et al. 2012) nozzle or with both type of nozzles (Qiu et al. 2015b). All their experiments were done with the addition of Polyvinyl acetate (PVAc) and resulted in micron or submicron-sized hollow spheres made of nano primary particles; the smallest ones were estimated at 20 nm for RDX/PVAc made from a pneumatic nozzle with a mean droplet size of around 7 μm . The versatility of the process allows the production of energetic composites (coating of TATB on micron-sized HMX, RDX or CL-20 by Ma et al. (2015)), energetic/elastomer composites (micron-sized CL-20/EPDM by Ji et al. (2015), micron-sized spheres of agglomerated HMX/Viton by Shi et al. (2015)), and even cocrystals (micron-sized spheres of agglomerated HMX/TNT by Li et al. (2015b)).

2.2.13 Spray Flash Evaporation (SFE)

Risse and Spitzer at the NS3E laboratory developed an innovative process after experimenting the limitations of the Ultrasonic Spray Pyrolysis method: beyond the inherent risk of using a high voltage electrostatic precipitators for energetic powders, the rate of evaporation of droplets is too low to avoid agglomeration and to crystallise submicrometer particles. Risse (Doctoral Thesis 2012) and Risse

et al. (2012) used the flash-evaporation behaviour of droplets to dramatically reduce the life time and the size of droplets. The compound is dissolved in a volatile solvent and that solution is heated just before being sprayed into vacuum, where the crystallisation is triggered by the sudden temperature depression and the solvent evaporation. The process is discussed in more details in Section 2.4.2.

An unconventional application of nanosized explosives used at the NS3E laboratory is the synthesis of nanostructured material by detonation. Pichot et al. (2015) and Pichot et al. (2013) demonstrated that smaller nano diamonds are generated from the detonation of n-TNT/RDX composites produced by SFE than from a physical mixing of micron-sized commercial TNT and RDX.

2.3 Discussion on production methods

The smallest size of RDX is either obtained from wet techniques, or from small-scale approaches which cannot be transferred to industry (PVD and LASER). Even if PVD has been successfully used in the semiconductor sector for our everyday electronic devices since decades, PVD for energetic material will never be able to reach a production of several hundred of grams per hour. However, PVD is perfectly suitable for the current trend to create “pyrotechnic integrated circuits”. Femto second LASER ablation is used for nanoparticles synthesis of metal in solution at the laboratory scale; the colloids produced are found to be extremely stable. Used in dried conditions, a deposit of nanoparticles on a substrate could be obtained from a gas flow, or a dried powder could be collected within a cyclonic separator: this LASER technique has been used to cut high energetic material quite safely (Roeske et al. 2003) but nanoparticles production would be severely limited to high-added-value industrial applications due to low production rate and high operation cost. Besides those two aspects, neither methods would process advanced composites – with a binder for instance – or would be able to do concomitant or cocrystallisation.

The production of nanoparticles through wet techniques has become a common industrial chemical process. The Sustainable Hydrothermal Manufacturing of Nanomaterials (SHYMAN) European project aims to increase the production rate of a continuous hydrothermal process from 1-10 tons/annum to 100 tons/annum of inorganic nanomaterials (Charitidis et al. 2014). Tsuzuki (2013) statistically studied which method for inorganic nano synthesis are mostly used in industry: vapour (39 % mainly Chemical Vapor Deposition (CVD)) and liquid (45 %) phase synthesis are the main type of techniques. Patents or historic skills of the brand can restrain the choice of a technology, so such data should not be taken as indicators of the robustness or versatility of the method. Considering such wide adoption of wet techniques (Sheth et al. 2012) and the knowledge from

Process	working pressure(s)	heating (°C)	continuous	scale-up	limiting step(s)	smallest size ¹
Sol-Gel	atmo	no	no	--+	matrix, drying	100-150 ²
Anti-solvent	atmo	70	could be	-	injection, drying	38
Milling	atmo	cooling	no	+	drying	160 ³
PVD	10 ⁻⁴ Pa*	100-200	no	-	vacuum	50
Electro-spray	atmo	no	could be	-	mass flow, electric field	400
ASES	12 MPa	yes and cooling	no	-	sCO ₂	microns
SEDS	35 MPa*	yes	no	-	sCO ₂	microns
RESS	35 MPa → 0.1-5 MPa	yes and cooling	could be	--+	sCO ₂	200
RESS-AS	35 MPa → atmo	25	could be	--+	sCO ₂ , drying	30 ⁴
LASER	atmo	no	no	-	mass flow	64
Ultra-sonic	atmo	50-150	could be	--+	transducer	200-500
Spray drying	atmo	50-100	could be	++	evaporation ratio	400
SFE	5 MPa → 5 mbar	150	yes	++	vacuum	300

Table 2.3 – Comparison . ¹ smallest pure RDX mean size reported in nm | ² XRD measurement | ³ freeze dried from a 64 nm RDX slurry | ⁴ from DLS, no report about dried state | *Not available in the references, so the value is based on usual operating conditions | sCO₂ : supercritical carbon dioxide

chemical engineering – homogenization in large reactor, processing of liquid flow, versatility, safety ... –, wet crystallisation methods are a logical choice to process organic materials. However, unlike inorganic and metal nanoparticles, organic matter is very sensitive to drying as we previously saw in Section 2.1.5; yet that delicate step is required since the reactivity of high energetic materials fully exhibits at the dried state. Freeze drying and supercritical drying seem to overcome kinetically and partially the crystal growth occurring. Only a complete growth inhibition will lead to the production of smaller nanoparticles under 100 nm from milling or anti-solvent/cooling crystallisation. From an industrial point of view, freeze or supercritical drying are batch-only processes; all current industrial drying processes are not designed to tackle down the fast growth of soft-matter. Innovative techniques such as spin freezing (L. De Meyer et al. 2015) or spray drying enhance the processability and potentially the performances, but their reliability need to be tested.

The ball-milling technique raises question about the purity of the product; it is well known that after such an extensive friction process, industrial milled ceramics are not used for high purity chemical process (Carter et al. 2013). Industry moved to other techniques such as vapour phase ones, to overcome that limitation and others like the lack of control, local heating etc. Even with soft matter, similar issues can be expected; even small quantities of metallic impurities could catalyse the degradation of the explosive and/or sensitize it.

After 25 years of research and 10 years of process engineering, the SuperCritical Fluid (SCF) technology has never convinced the industry and only marginal uses for specific commercial drug products have been reported (Sheth et al. 2012). First, the choice of the gas at industrial scale is falling back to CO₂ due to safety and affordability criteria. For instance, gases such as nitrous oxide or ethane have low critical values, but explosive mixtures can be generated. Trifluoromethane is inert, non-flammable and is usually a better solvent but is way more expensive than CO₂ and a potent greenhouse gas. Second, the main limitation –the solubility into sc-CO₂– can be overcome by the addition of organic cosolvent: such modification alters the environmentally safe nature of sc-CO₂ based SCF and complicates the process by the need to remove any residual organic solvents. The aggregation phenomenon is commonly observed in SCF processes; further investigations on the role of different particle collection environments are needed, but RESS-AS processes greatly avoid the particle aggregation. The use of a liquid anti-solvent with polymeric stabilizers has been found to be very effective. However, it compromises the recovery of a dry pure powder, going back to square one with the drying issues previously discussed.

Spray techniques are commonly used in the industry, such as micro-encapsulation massively used for food (Gibbs et al. 1999; Madene et al. 2006), spray drying in

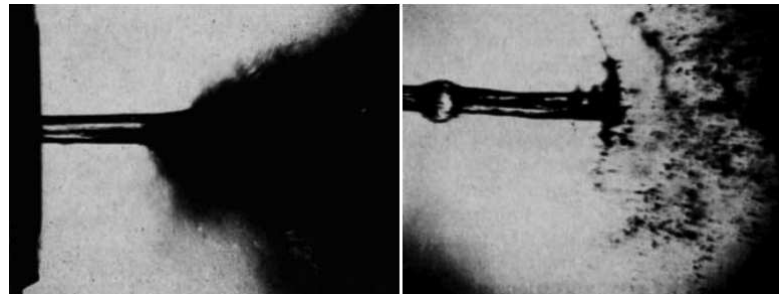
pulmonary drug delivery for production of uniform and breathable size particles (Bhavesh B. Patel et al. 2014) or even thermal spray deposition of metallic material (Lavernia et al. 2009). Spraying is a method which allows easy implementation of an installation and easy direct control over the injection. However, because of the low technological cost of atomizing nozzles and the low control over the spray itself, details and know-how are much more important than for other processes. Direct spray drying as crystallisation technique for RDX does not produce submicron-sized particles without the help of an additive and the SCF techniques are not suitable for industry: the need for an intermediate method in terms of pressure and temperature leads to the creation of the Spray Flash Evaporation technique, especially tailored for crystallisation. SFE operates from 40 to 100 bars with an RDX solubility in acetone around 5 wt%, whereas sc-CO₂ is formed from 74 bar to 500 bars for a solubility from null to 0.025 wt%.

2.4 The Spray Flash Evaporation Technique

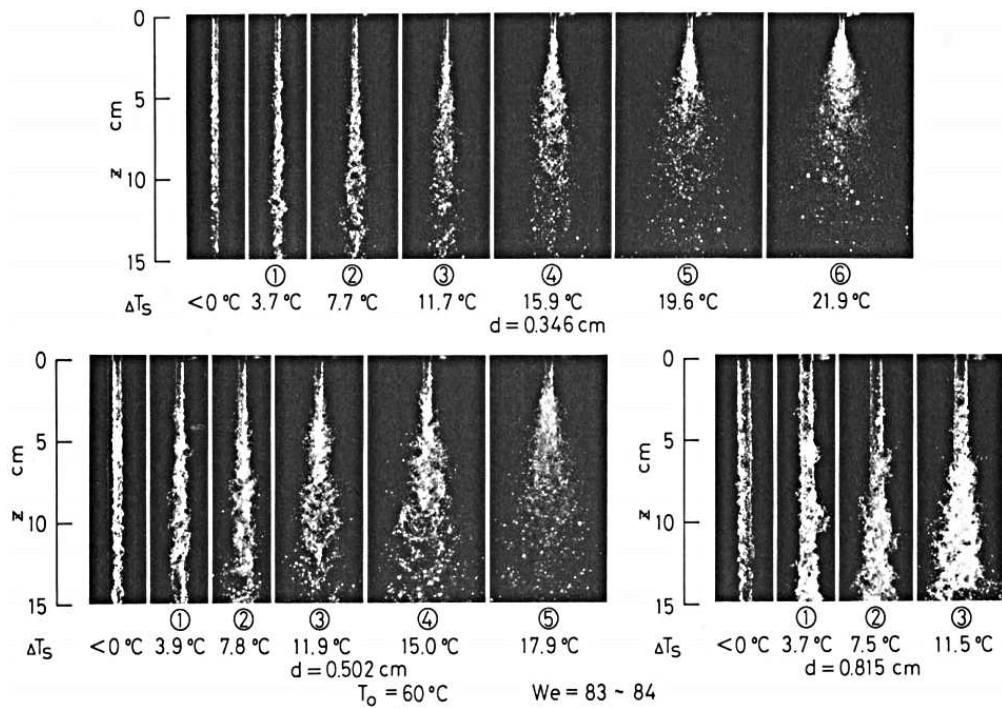
2.4.1 Theoretical Insights on the SFE technology

Flash Evaporation The flash evaporation is the physical phenomenon occurring when the boiling point of a liquid is lower than its actual temperature, due to a sudden drop of pressure and/or a quick increase of temperature. The excess of heat is instantly converted into latent heat of vaporization, cooling both liquid and vapour down to the saturation temperature. Multi Stage Flash (MSF) evaporators of static water have been used since the middle of the XXth century (“Combined flash and vapor compression evaporator” 1956; “Flash-type distillation system” 1959; “Method of and apparatus for flash evaporation treatment” 1957) with yield of around 100 m³ per day, receiving a growing interest mainly from the US West Coast (Resources 1969) and Japan (national research program “seawater desalting and by product recovery” launched in 1969, (Sawa et al. 1976)). Current applications are extended from solution concentration such as in wine industry (Sebastian et al. 2002) to heat dissipation of electronic chips and LASER devices (Cheng et al. 2016).

Flash Evaporation of Superheated Liquid Jet Brown and York (Brown et al. 1962) found a critical temperature above which the liquid jet was burst by rapid bubbling. They injected water up to 13 bar through simple single-hole nozzles with a minimal diameter of 500 μm into ambient pressure. The linear mean droplet sizes were found to follow a linear variation of temperature. Then in 1981, Miyatake et al. were pioneers in the field of flash evaporation and published the



(a) Two different disruptions in flashing water jets enlarged 10X from Brown et al. (1962)



(b) Flashing water jets under various superheating from Miyatake et al. (1981a)

Figure 2.2 – Flashing in water liquid jet

first known articles about spray flash evaporation with superheating (Miyatake et al. 1981a,b), after studying flash evaporation from water pool (Miyatake et al. 1972). Many technical limitations restricted their studies for current issues: only straight-lined liquid jets were studied with basic optical techniques where the smallest drops and bubbles could not be indexed. However, Miyatake et al. (1985) interestingly used electrolysis to generate more bubbles into a flashing water jet. Nowadays, not many laboratories still investigate flashing liquid jets; Günther et al. (2013) characterized with modern techniques flashing liquid jets and noticed the formation of bubbles inside a glass nozzle for high superheating. They also demonstrated that a simple acoustic measurement can be used to monitor the atomization of superheated liquids. The current application of flashing liquid jet is the improvement of MSF desalination processes of sea water (Ikegami et al. 2006; Miyatake et al. 2001); a much higher evaporation rate is obtained in contrast to static flash evaporator where the rate is surface dependent.

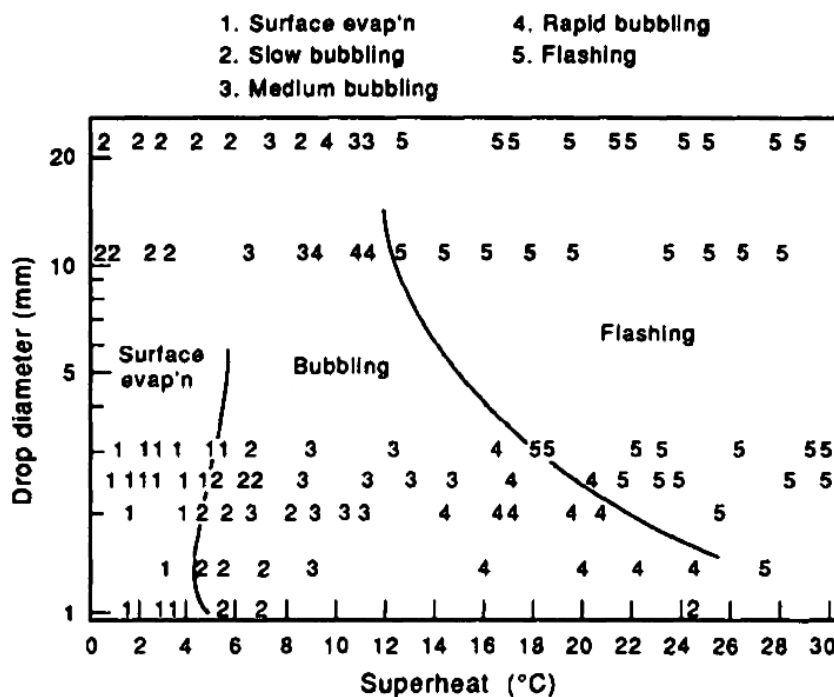


Figure 2.3 – Empirical diagram of the evaporation of a water drop (Owen et al. 1991)

Flash Evaporation of Droplets Specific studies on the flashing phenomenon are rare. Owen et al. (1991) investigated that specific form of evaporation on isolated drops. A superheat of 0°C to 5°C triggers only surface evaporation,

then boiling occurs at higher superheat. Flashing is triggered for superheat from 18 °C to 24 °C for drop of 1 mm–3 mm and larger drops flash more readily as illustrated in Figure 2.3. Since flash evaporation is closely related to cooling, many theoretical approaches start with a simplified model without superheating: Shin et al. (2000), Satoh et al. (2002) thoroughly described the evaporation behaviour of a water droplet in an abruptly evacuated atmosphere leading to its solidification. Sobac et al. (2015) developed a comprehensive model of the evaporation of a liquid spherical drop but not yet applicable to extremely small droplets as in flashing spray.

Interesting studies close to our SFE process came from Gebauer et al. (2012, 2015a,b, 2016). In their system, a pressurized superheated liquid is atomized through an hollow cone nozzle into a low pressure chamber and micron-size particles are recovered. However, only a partial evaporation occurs and leads to further crystal growth during the flying time and into the sump collected in the bottom of the crystalliser.

2.4.2 Comprehensive description of SFE

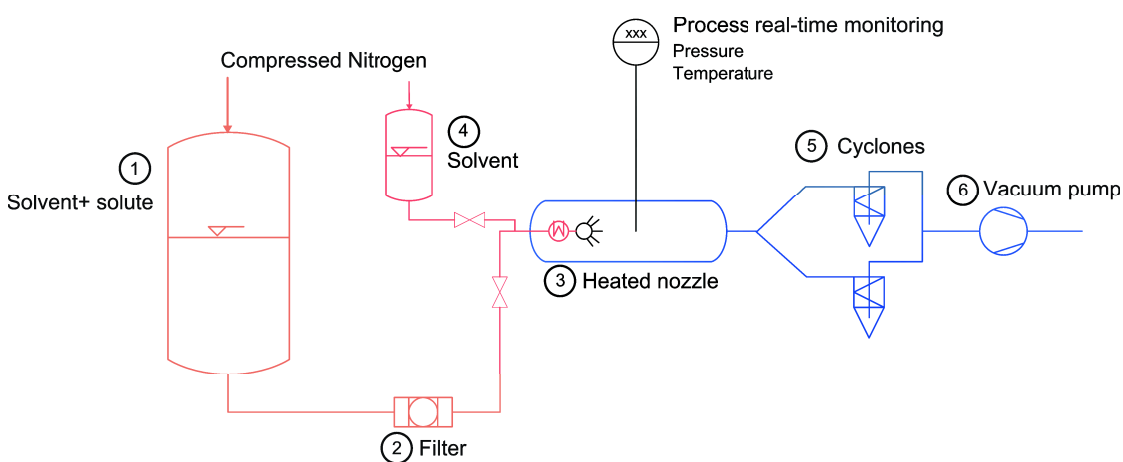


Figure 2.4 – SFE installation as patented and used in this present work

Figure 2.4 is a schematic diagram of the process, where the high pressure part is the red zone and the low pressure one in blue. One storage tank (4) is filled with technical grade solvent and is used for pre-heating, cooling and washing. The other tank (1) is filled with the solution containing the compound(s) to recrystallize. Both are closed and pressurized with compressed nitrogen at the pre-expansion pressure. Hydraulic tubes bring the fluid inside the atomization chamber; there, a heating jacket superheats the liquid, with a regulation made of thermocouple plugged to a Proportional-Integral-Derivative (PID) controller.

The superheated fluid is sprayed by a hollow cone nozzle (3) into the atomization chamber under a vacuum below 10 mbar. Details can be seen in Figure 2.5: the tip of the thermocouple (type K \varnothing 1.5 mm) measures the temperature after the heating jacket and just before the nozzle mounted on a full flow quick coupling.

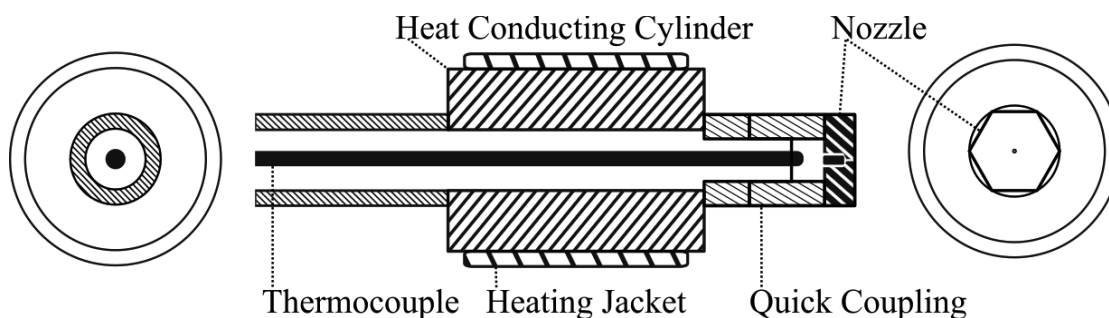


Figure 2.5 – Schematic insight of the nozzle and its heating system; from left to right, rear view, longitudinal cross-section and front view.

The gaseous flow from the evaporation and the recrystallized product is pumped to a cyclonic separator. The cyclones are made from the description of (Chen et al. 2006) who found a cut-off diameter of 21.7 nm–49.8 nm in their work. A glass flat flange reaction vessel allows to gather the powder easily as it can be seen in Figure 2.6. Each cyclone unit can be isolated from the vacuum to allow the recovery of the product from one unit and the continuous separation inside the other: the two cyclones in parallel ensure the continuous functioning of the process at any flow rate.

At the end, the flow of gaseous solvent passes through a 35 m³/h vacuum pump; a condenser after the pump can recover the solvent for industrial installations.

The standard operating conditions are 40 bar of inlet pressure and 160 °C at the hollow cone nozzle with an orifice diameter of 60 μ m.

The maintenance and constant improvements of several SFE installations took a significant part of this research project. The reliability, robustness, ergonomic and life-cycle of the process have been extended by replacing hydraulic and vacuum parts, by understanding phenomena, by developing on-line metrology and by stimulating the necessary feedback and cooperation between the various SFE users at NS3E.

2.4.3 Versatility of the SFE

Depending on the solute and the desired particle size range, the SFE can be adapted by changing the following parameters:

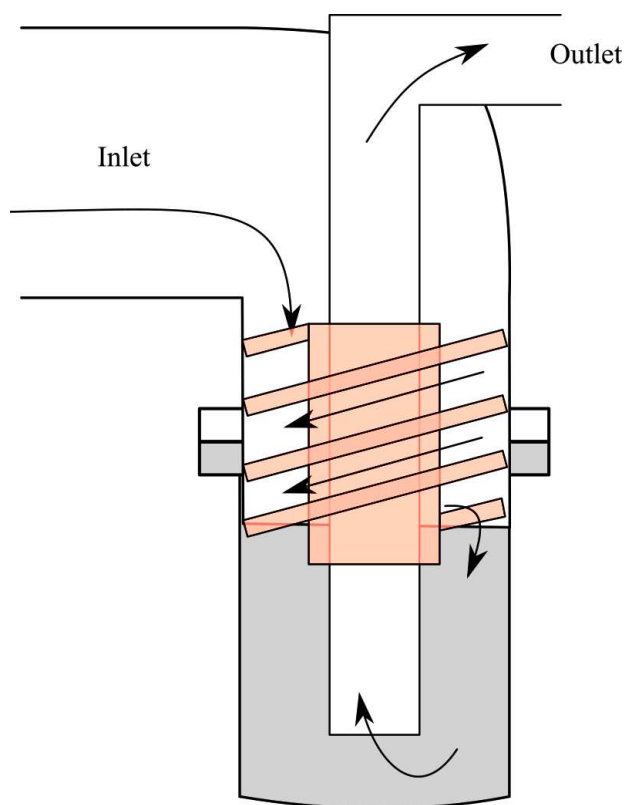


Figure 2.6 – System for the product recovery: in orange the cyclonic separator for vacuum and in gray the interchangeable vessel.

Type of solvent The most suitable solvents for SFE are low-boiling solvents with a high molar heat capacity. For easy handling and recovery, the solvents should have a boiling point in the range of 30 – 70 °C.

Superheating temperature The superheating temperature is proportional to the mass flow and the fluid properties. An increased superheating temperature enables higher evaporation rate.

Pre-expansion pressure The pre-expansion pressure has to be above the vapour pressure of the superheated solvent and compatible with nozzle diameter and type. The droplet size is also known to decrease at higher pressure.

Saturation pressure and temperature Saturation pressure and temperature of the spray cone in the atomization chamber depend mostly on the performance of the vacuum pump.

Nozzle diameter For most nozzles types like hollow cone nozzles, full cone nozzles, or flat jet nozzles, a decreasing orifice diameter decreases the

droplet size, but increases the pre-expansion pressure.

Besides the innovative applications of nano energetic materials such as the synthesis of ultra-fine nano diamonds (Pichot et al. 2015; Pichot et al. 2013) and reactivity enhancement (Comet et al. 2015), the SFE versatility allows the crystallisation at a submicron or nano scale of a wide range of organic compounds. In particular, cocrystals of medical materials are of interest for drug enhancement and were successfully processed through SFE at the nano scale (Spitzer et al. 2014). Inorganic nanoparticles were also produced at the nanoscale through SFE. ZnO was crystallised from the precursor zinc acetate dihydrate dissolved in ethanol with addition of water. From early experiments, nano primary particles of 20 nm were found to be agglomerated in sub-size structures, whereas the slightly larger nanoparticles were found much less agglomerated using the classical wet method. However, the SFE clearly demonstrated the feasibility of faster and quite efficient crystallisation of inorganic particles from precursors. Le Brize et al. (2016) processed energetic composite materials by SFE: a submicron structuration was evidenced from SEM pictures and an higher degree of chemical interaction was also found from Infrared (IR) and Raman spectra.

2.5 Scientific goals of the thesis

2.5.1 Particle Size Reduction

The first main goal of the project is to reduce further the particle size. During his PhD, Risse studied the effects of the superheating temperature, the inlet pressure, the ratio of MTBE/acetone as solvent, the nozzle diameter and the RDX-concentration. At higher superheating temperature and pressure, the droplets are likely smaller which leads to a noticeable decrease of the particle size. However, the role of solvent was not clarified; furthermore, both nozzle diameter and RDX-concentration need to be correlated with the inlet mass flow and the real superheating temperature – which is the difference between the spray and the inlet liquid – should have been monitored and kept constant. To reduce the particle size, the degree of supersaturation has to be controlled in both space and time resolution. Globally, we can distinguish two main approaches, a chemical one and a more physical one. On the chemical route, polymeric additives are studied to control the nucleation and growth steps. On the other side, different conditions of crystallisation are studied by a mixture of an anti-solvent and a solvent, and also by 'in-spray interactions' where two nozzles with overlapping spray patterns are used.

2.5.2 SFE understanding

The crystallisation by SFE results from deep and complex interactions between several physicochemical phenomena. That intricacy is illustrated by the mapping in Figure 2.7. While many parameters are involved, a few bottlenecks emerge: the volume of droplets, the degree of supersaturation and the time of the primary nucleation are keys to achieve a perfect control of the final particle size under flash-evaporation conditions. Therefore, the effort on *in situ* measurement for SFE technology is focused on those observable variables. In the meantime, other parameters has been changed such as the solvent type to influence the supersaturation and the nucleation time by additives.

2.6 Summary of the Chapter

Many crystallisation processes have been applied on RDX and similar energetic organic crystals. The smallest size of RDX is either obtained from wet techniques, or from small-scale approaches which cannot be transferred to industry (PVD and LASER). Finally, the Spray Flash Evaporation (SFE) process is a well balanced method between spray drying unable to process particles lower than the micrometer, and the expensive batch Rapid Expansion of Supercritical Solutions (RESS) process. The SFE relies on the superheating of a solvent sprayed into vacuum and thus flashing. The pressurization of the liquid before the injection provides the stability for the spray pattern and also for the overheated liquid. The flash evaporation is the physical phenomenon occurring when the boiling point of a liquid is lower than its actual temperature, due to a sudden drop of pressure and/or a quick increase of temperature. The excess of heat is instantly converted into latent heat of vaporization, thus provoking the fragmentation of the droplets called "flash". This allows formation of smaller crystallisation reactors (droplets) with a very high rate of evaporation therefore achieving smallest particle size.

From particle size and shape many properties are resulting such as the surface related ones for catalysis but also more physical one like the apparent density and the critical diameter for explosives. However, the definition of a particle is subject to variation; a real powder may be formed of macroscopic soft agglomerates of micron-sized hard agglomerates of nano primary particles. Therefore each characterization technique measures an unique mean distance depending of the physicochemical phenomena involved and the response of the sample. The following explains the characterizations previously in use at NS3E, their scientific criticism through analytical studies and the new methods applied.

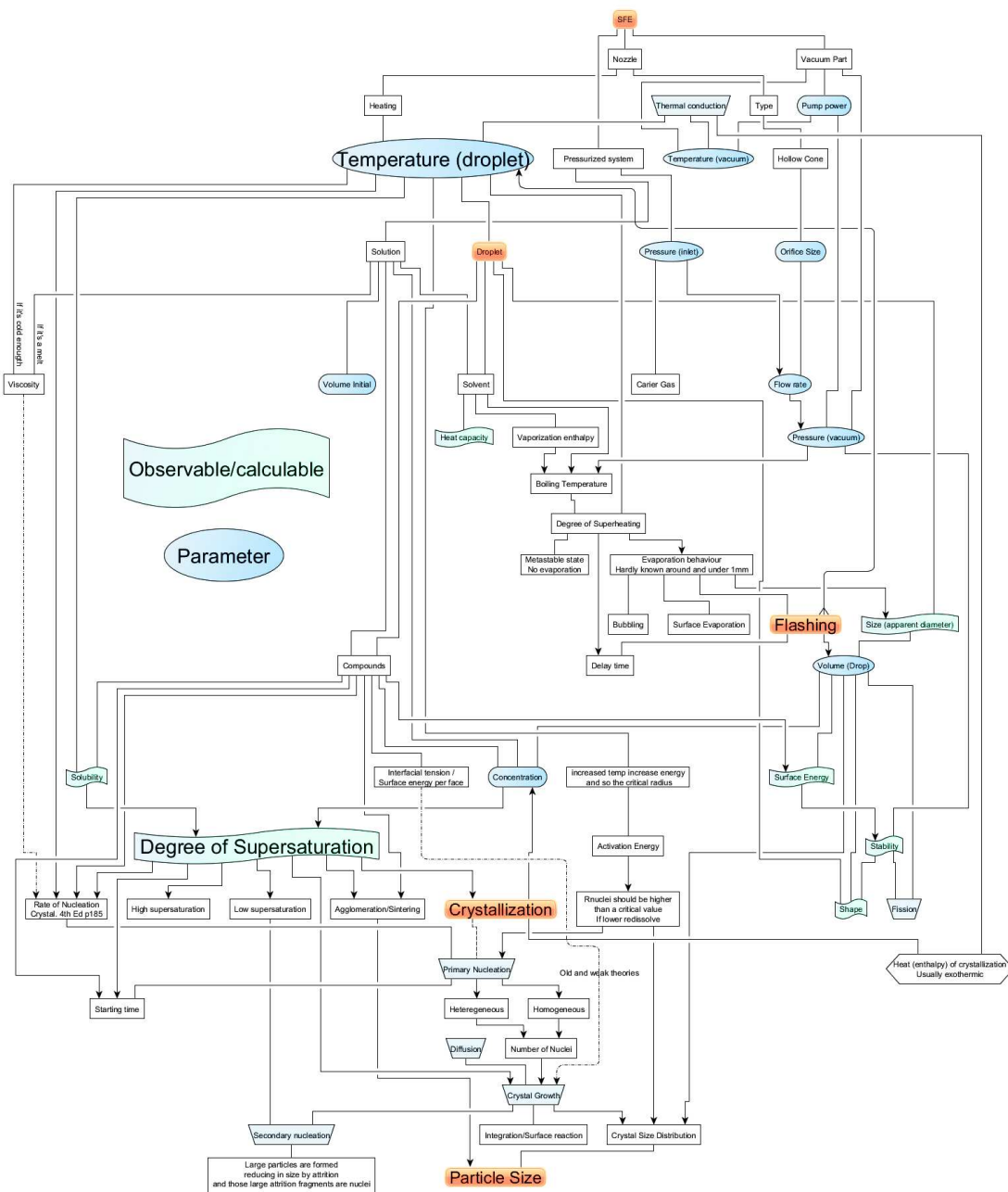


Figure 2.7 – Intricacy of the parameters and phenomena involved in the particle crystallisation by the SFE process.

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Chapter 3

Definition of Particle and Determination of the Particle Size Distribution of RDX processed by SFE

3.1 Size Measurement

3.1.1 Sensitivity of nano-organic energetic particles

A particle size distribution can be obtained through many methods: X-Ray Disc Centrifugation (XDC), Photon Correlation Spectroscopy (PCS), Differential Centrifugal Sedimentation (DCS), Laser Scattering (Dynamic or Static), Laser Doppler Electrophoresis, nitrogen adsorption (BET method), Differential Mobility Analysis (Scanning Mobility Particle Sizer), Phase Doppler Particle Analyzer, Electronic Microscopy, Atomic Force Microscopy etc. But only a few are suitable for organic nanoparticles. In molecular crystals, weak forces are holding the molecules together instead of covalent bonds for metals or oxide solids; therefore organic nanoparticles are much more sensitive to solvation issues. Water is commonly misused as an anti-solvent of RDX, whereas the few mg/L of solubility is enough to strengthen the growth of crystals through Ostwald ripening or to model a new crystal habit within a few hours or minutes. The liquid alkanes such as hexane are much more often used to precipitate active pharmaceutical ingredients in industry. Besides the solvation, all characterization methods from a colloid are measuring aggregates and agglomerates; some even measure a bigger diameter, a hydraulic one which includes one or several solvations or ionic layer depending of the technique.

In a dried state, measurements can be performed from an aerosol: LASER techniques such as Phase Doppler Analysis (PDA) suffer from a submicron limit of detection. The first stage of a Differential Mobility Analysis (DMA) technique is the neutralization of the aerosol from a radioactive source then particles are sorted by their mobility and so size, then counted by a Condensation Particle Counter (CPC); to overcome the size limitation, the CPS creates vapour from a working fluid (usually butanol, isopropyl alcohol, or water) which condenses onto the particles helping them grow in size and can be optically counted. It is important to notice that hard aggregates in aerosol can not be distinguished through DMA; surface area and volume can be corrected but the primary particle diameter has to be known already. However, DMA provides statistically significant and real time size distributions.

On static dried powder, particle size can also be extracted from BET theory by adsorption of a known gas. Diverse trials to investigate surface area and derive particle sizes from BET were found to be inefficient on n-RDX: no compromise between an appropriate degassing and a prevention of nanomaterial degradation and sintering could be established, due to high vacuum and heating that have to be applied on the sample (Section 1.4.2).

Direct particle observation should always be performed to verify the validity of the assumptions made from the other characterization techniques. Particle aggregation, particle morphology and degradation can be measured or at least reasonably estimated for particles under 50 nm. To reveal details at the nano scale, Atomic Force Microscopy is well suited for insulator nanoparticles. No energy is brought to the material but only a slight mechanical stress; imaging is performed at ambient temperature and pressure. Nevertheless, the tip is not a single point probe: the curvature radius and cone angle lower the height and also cause a "profile broadening" effect. Those side effects can be reduced by scanning in tapping mode and selecting a tip with a smaller radius to improve accuracy. However, a balance has to be found between the accuracy and the differential height that the tip can follow without being damaged. Therefore, when the particle size exceeds the hundreds nanometres, electron microscopy allows data acquisition on bigger areas in a minute.

3.1.2 AFM

3.1.2.1 Methodology

To overcome the difficulties encountered with SEM and to improve the accuracy, Atomic Force Microscopy is a good and obvious choice, especially when a laboratory has both apparatuses. For this reason, a standard procedure has been established prior to my arrival to measure particle size. To minimize the

roughness of the sample surface for an AFM tip, an original technique was introduced. The powder is pressed into pellets then its surface is flattened by the use of a rotary microtome.

A stainless steel tubular mould with an inner diameter of 4 mm is filled with the energetic material then closed with a stainless steel rod; the system is placed under a press where different weights can be hang on the extremity of a lever. The whole apparatus follows the pyrotechnic safety guidelines thanks to a mould with thick walls and a protective transparent screen. In this case, the mass of energetic materials is below 50 mg. The material is maintained under a pressure of 97 MPa for one minute, with transitions slowest as possible to avoid friction heat. Microtomy is done by a succession of cut thinner and thinner on one side of the pellet: five times 20 μm , then five times 5 μm and finally five times 1 μm to remove superficial layers and have the smoothest surface. The quality of the surface preparation can be easily seen with the naked eye, by checking its great reflectivity.

The mean apparent density is $1.406 \pm 0.035 \text{ g/cm}^3$ from results reported in Table 3.1 which is in good agreement with densities from Pichot et al. (2015) and shows good reproducibility. The easy shaping of the powder into a cylindrical pellet is only possible thanks to the reduced particle size: pellets of the finer commercial available RDX with a PSD around 6.8 μm break apart (Spitzer et al. 2011). Moreover, pellet of n-RDX exhibits a glassy structure with transparency.

Height (mm)	Mass (mg)	Density (g/cm^3)
1.09	19.69	1.395
1.61	28.42	1.377
0.92	17.33	1.462
1.56	28.04	1.395
2.08	38.89	1.451
1.50	26.23	1.357

Table 3.1 – Several apparent densities of pellets pressed at 97 MPa.

The analysis of height fields obtained by AFM is then made through a semi automatic process with the free and open source software Gwyddion (Nečas et al. 2012). Gwyddion is a modular program for SPM (Scanning Probe Microscopy) data visualization and analysis. It has been chosen thanks to its large number of data processing functions, including all the standard statistical characterization, the levelling and data correction, the filtering or grain marking functions. Among them, the watershed algorithm allows the detection of particles by local minima determination then image segmentation. The grain size analysis is made through several steps:

Grain localisation process the surface is inverted – hills become valleys – then virtual water drops are placed on each point. Then drops fall to the closest local minimum, following the steepest descent. The process is repeated and accumulated drops are forming lakes. Those small lakes filling the inverted surface depressions are the position of grains.

Segmentation While the drops are filling the surface, if a lake touches another one, they are merged in the previous step. In the segmentation step, drops are again falling but the growing lakes are not merged and their border is refined. The quality of grain boundary depends on the drop size set but computing time increases when the drop size is smaller.

Visual checking and corrections The software allows manual marking of grains and several contrast improvements to control and correct the results from the watershed method. The phase and amplitude channels can also help to determine the validity of a grain boundary.

PSD and fitting The software allows the direct display for the PSD but also can export the results. The diameter of a grain is computed from the diameter of a disc with the same surface area. A frequency count on the diameters renders the raw PSD; then the curve is fitted with a log-normal distribution function. Gaussian fitting is in poor accordance. Therefore, the PSD is generated by many small random effects that are multiplicative for the log-normal distributions (Limpert et al. 2001)

3.1.2.2 Effect of the concentration on the particle size

During his PhD in our laboratory, Risse studied the RDX concentration from 0.5 wt% to 2 wt% in acetone; as the concentration increases, the particle size decreases and so the specific surface increases. This can be linked to the increase of the degree of supersaturation with the concentration, therefore triggering a high nucleation rate. In this context, the first work of my PhD project was to start studying the crystallisation process and so the degree of supersaturation by extending that previous work.

SFE parameters were chosen from the optimized operating conditions: the nozzle temperature is set at 160 °C, the inlet pressure at 40 bar and the nozzle is an hollow cone one with a diameter of 60 µm. The walls of the vacuum chamber from the nozzle to the cyclone are heated to 80 °C to avoid any condensation and to reduce the losses of product by thermophoretic force. The solvent used for all the study is the same lot of acetone CHROMASOLV®, for HPLC, ≥99.9% , from Sigma Aldrich. The same lot of RDX provided by Eurengo, labelled as M5, is used all along this study and this PhD project.

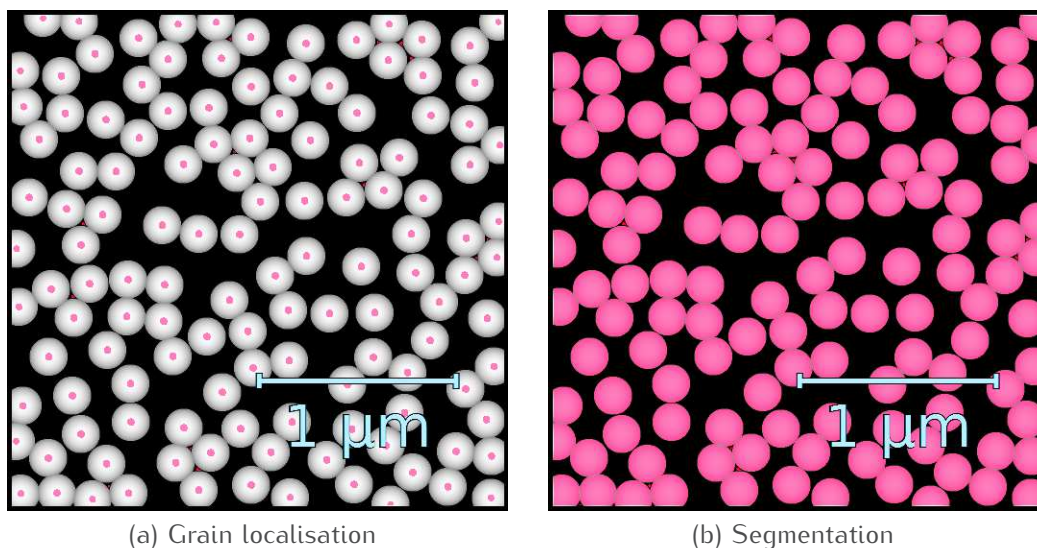


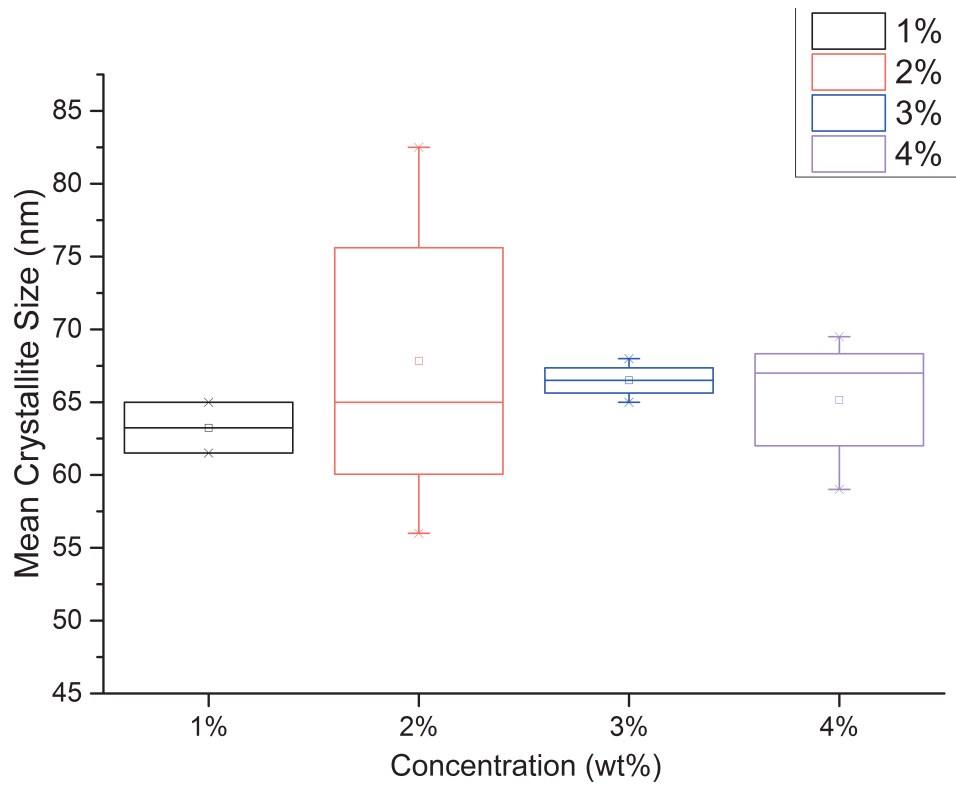
Figure 3.1 – Watershed analysis illustrated on simulated 200 nm spheres.

PSDs are determined by the previously mentioned method on pellets. XRD is also performed in order to calculate the apparent volume weighted domain size from the Scherrer equation as described in Section 1.4.2 p. 49. The sensitivity of the energetic powders is also quantified in order to investigate an eventual link with the mean particle size and crystallite size. Also the results are reported in Figure 3.2.

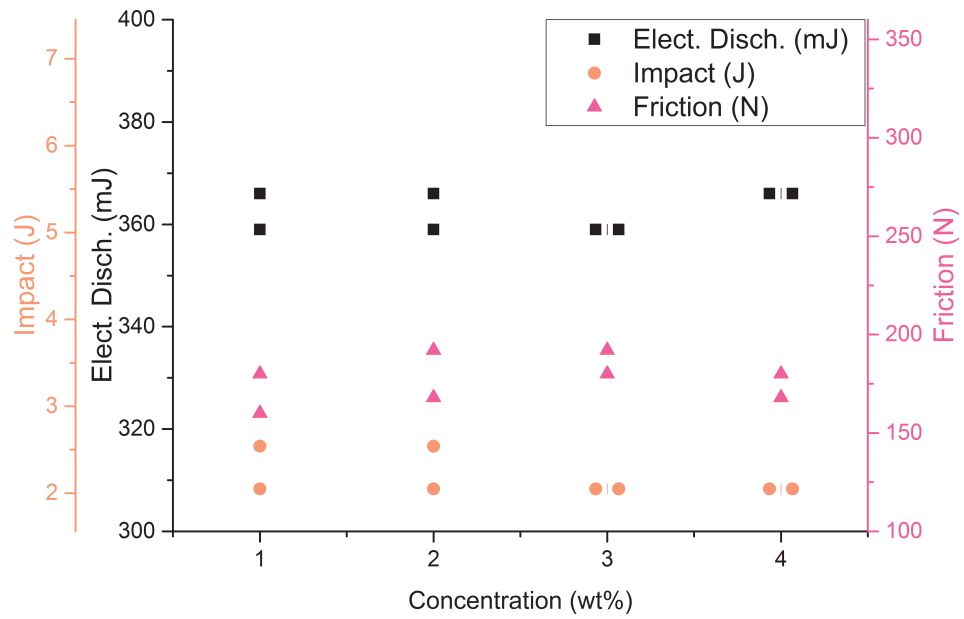
A parabolic trend could be interpreted from Figure 3.2e. However, the statistical significance of the result should be first performed. Thus, statistical analysis are made from the software GraphPad Prism 5 to compare mean particle size obtained from AFM pictures from one concentration to another. Table 3.2 shows that globally these means are not significantly different. Table 3.3 compares mean to each other and still no significance has been found.

The concentration of RDX in solution up to values close to the saturation does not influence the particle size according to the statistical analysis. Moreover, sensitivity remains constant among all samples: to up-scale the SFE process, such constant properties while increasing the RDX content is advantageous to increase the mass flow and so decrease the cost of the process.

The mean crystallite size is also always around 65 nm; RDX particles are polycrystalline and the nucleation seems to be unchanged while changing concentration.

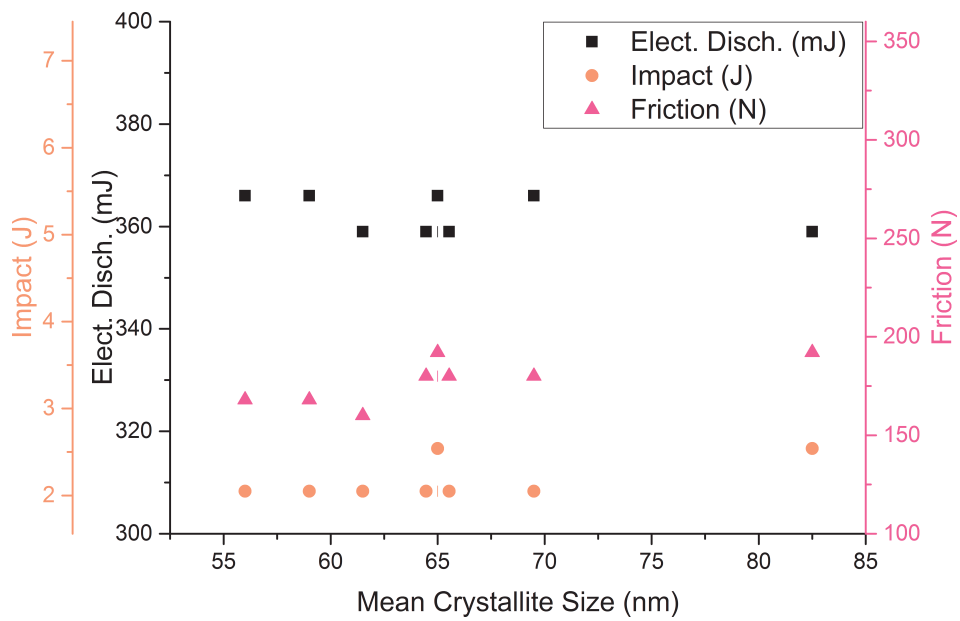


(a) Crystallite against concentration

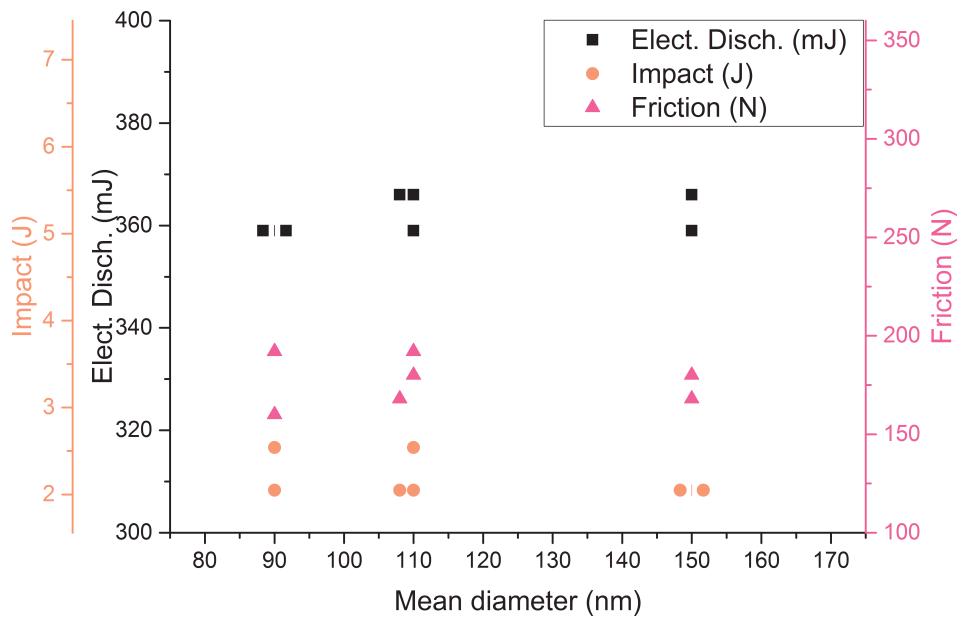


(b) Sensitivity against concentration

Figure 3.2 – Parametric study based on the variation of the concentration in solvent.

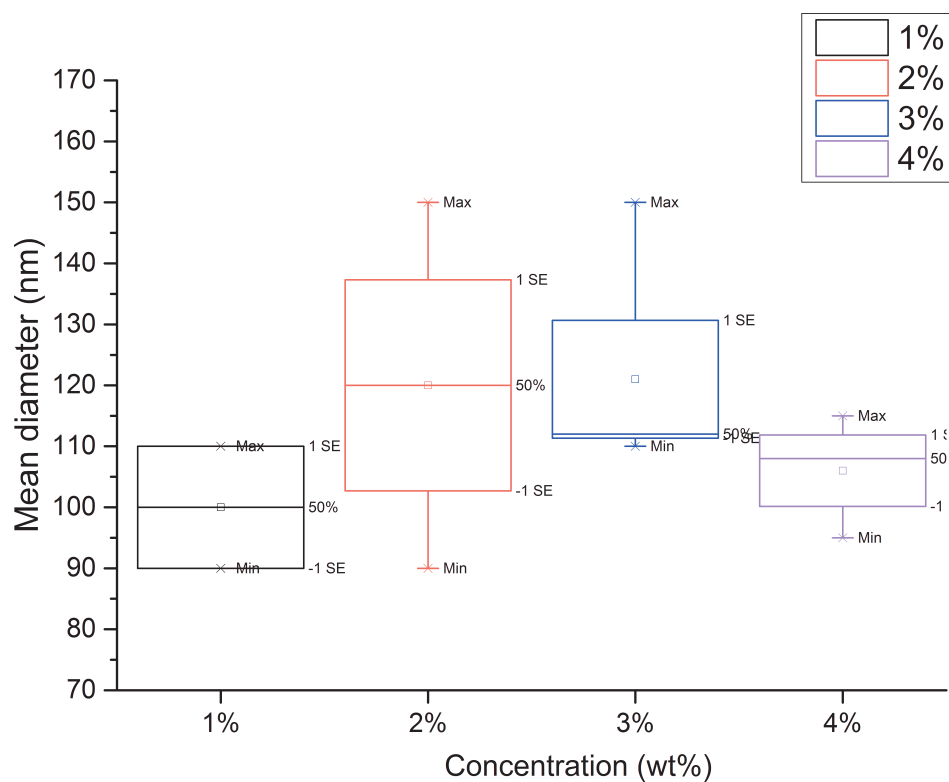


(c) Sensitivity against crystallite



(d) Sensitivity against particle size

Figure 3.2 – Parametric study based on the variation of the concentration in solvent.



(e) Particle size against concentration

Figure 3.2 – Parametric study based on the variation of the concentration in solvent.

P value	0.5734
Are means signif. different? ($P < 0.05$)	No
Number of groups	4
F	0.7087
R squared	0.2100

Table 3.2 – One-way analysis of variance on the particle size from AFM pictures.

Tukey's Comparison Test	Mean Diff.	q	Significant?	95% CI of diff
1% vs 2%	-20	1.519	No	-79.64 to 39.64
1% vs 3%	21	1.681	No	-77.58 to 35.58
1% vs 4%	-6	0.4556	No	-65.64 to 53.64
2% vs 3%	-1	0.09076	No	-50.90 to 48.90
2% vs 4%	14	1.189	No	-39.35 to 67.35
3% vs 4%	15	1.361	No	-34.90 to 64.90

Table 3.3 – Tukey's multiple comparison test on the particle size from AFM pictures.

3.1.2.3 Reliability and accuracy

Risse also found that a crystallite size remained constant around 65 nm. However, the concentration had a significant influence on PSD from BET and SEM characterizations: the particle size decreased while the concentration increased. The mean particle size from SEM was 715 ± 244 nm at 0.7 wt% and 408 ± 175 nm at 2 wt%: those values were much higher than the mean particle size obtained from the AFM method.

No statistical assessment was performed previously and the repeatability of the previously work is questionable. The difference between SEM and AFM was a scientific question previously discussed. The high vacuum decreases the thermal stability of the energetic compounds which also have a very low vapour pressure (3.30×10^{-9} Torr the vapour pressure of RDX at 25 °C (Östmark et al. 2012)); it can be assumed that sublimation of the smallest particle leads to that significant difference in mean size. Sintering can also be strongly worsen by the energy brought by the electron beam.

To finally settle those long term doubts and question the reliability and accuracy of the pellet method, a parametric study was performed halfway across this PhD project thanks to the help of the ex-internship, currently PhD student, J-E Berthe. The uncertainty of the Watershed method was estimated and the following two key parameters were studied

- pressure applied
- microtomy

Uncertainty of the Watershed Method As implemented in the current version of Gwyddion (2.45), the Watershed Method suffers from a lack of optimization and synergy between the other correction tools of the software. To study the sole effect of the Watershed method, ideal AFM topographies of a virtual deposit of spherical particles were made through the build-in particle generator. In that way, all instrumental influence (AFM tip geometry, noise etc.) is totally suppressed as it can be seen from the Figure 3.1 p. 99.

Several tests were performed with different particle sizes, picture dimensions and surface sizes: values were taken from the AFM picture usually analysed. An alternative method introduced with the most recent updates was also tried: the threshold algorithm which relies on the height, slope and curvature parameters; those three options can be combined by union or intersection. The result of the algorithm is updated in real time but requires much more attempts. The Table 3.4 shows that the Watershed method is always more accurate than the threshold one due to more rigorous grain boundaries. However, the size is always minimized: this can be easily explained due to the boundary layer of

one pixel to mark grains. So the accuracy decreases with the particle size and the resolution since the missing pixels represent an higher relative area. As rule of thumb the mean particle sizes measured from AFM have to be increased by 10% for 1024 px × 1024 px pictures and by 20 % for 512 px × 512 px pictures. The values reported in the previous study on the effect of the concentration are then corrected by 10%.

	particle radius	resolution	simul. area	method	nbr. of analysed part.	measured radius	deviation from the initial radius
unit	nm	lines	µm			nm	
trimmed	50	512x512	5x5	threshold	1445	36.75	27%
	50	512x512	5x5	threshold	1406	36.75	27%
	50	512x512	5x5	watershed	1474	40.25	20%
trimmed	50	1024x1024	5x5	threshold	1477	40.75	19%
	50	1024x1024	5x5	threshold	1416	40.75	19%
	50	1024x1024	5x5	watershed	1539	44.25	12%
trimmed	150	512x512	5x5	threshold	215	129.75	14%
	150	512x512	5x5	threshold	177	129.75	14%
	150	512x512	5x5	watershed	248	136.75	9%
trimmed	150	1024x1024	5x5	threshold	214	133.75	11%
	150	1024x1024	5x5	threshold	176	133.75	11%
	150	1024x1024	5x5	watershed	235	137.5	8%

Table 3.4 – Watershed and threshold method tested on simulated data; the ‘trimmed’ results mean that the grains at the edge of the picture are removed since they are probably trimmed. The Watershed algorithm add a one pixel boundary at the edges too, so trimmed grains cannot be removed easily.

Effect of the Pressure The press used for the compression of energetic materials consists of a lever supported by an hydraulic piston; at the extremity of the lever an hook allows to put several weights on it (from 5 kg to 97 kg), then the piston is actuated to slowly lower the lever thus forming the pellet. The pressure applied on the sample is calculated according to the weights applied; values are reported in Table 3.5.

In the results reported in Figure 3.3, the same face was always inspected by AFM (the upper one here) and microtomy was not applied. The scan surface is 5 µm × 5 µm in 1024 px × 1024 px. In Figure 3.3a clear drop of the mean size begins at 140 kg and then the value fluctuates around 90 nm: that change is

Weight (kg)	Pressure (MPa)
2	12
5	26
10	50
20	97
30	140
45	210
70	330
97	460

Table 3.5 – Weights used and their calculated corresponding pressures: the leverage follows the law $P = 6 \cdot \frac{M}{A} + 31$ where $A = \frac{\pi}{4} \cdot \varnothing^2$ with M the mass of the weight.

also observed in Figure 3.3b with a shift and a major broadening of the particle distribution. On the AFM pictures in Figures 3.3c and 3.3d, particles are hardly identifiable.

The results from samples processed by microtomy in Figure 3.4 also demonstrate that the pressure has a significant influence on particle size. In that case, the particle size is reduced further and further with increasing pressure. Above 97 MPa (20 kg), the pellets start to be too glassy for microtomy; due to the great hardness, the pellet breaks apart when the blade hits the sample.

Raw micron-sized RDX (M5 Eurenco) were also investigated; the pellets are much less cohesive and were not flattened by microtomy. However, at the highest pressure of 97 MPa, a similar breakage appears with a much lower particle size. Therefore the milling of n-RDX processed by SFE is much easier; for industry, it would be interesting to find a balance between optimization of the SFE conditions and an additional rough milling/mixing step. Also this effect would have an huge impact on energetic pressed charges.

Effect of the Microtome From the curves in Figures 3.3a and 3.4a, the microtomy reduces the size. The surfaces from samples pressed at 97 MPa and processed by microtomy (Figure 3.4e) are quite similar to the samples pressed above the critical pressure and not processed by microtomy (Figure 3.3e).

Pressure reduces the inter-granular void which increases compactivity and hardness. Therefore, the blade of the microtome needs more energy to penetrate the pellet and a surface milling occurs reducing further the particle size.

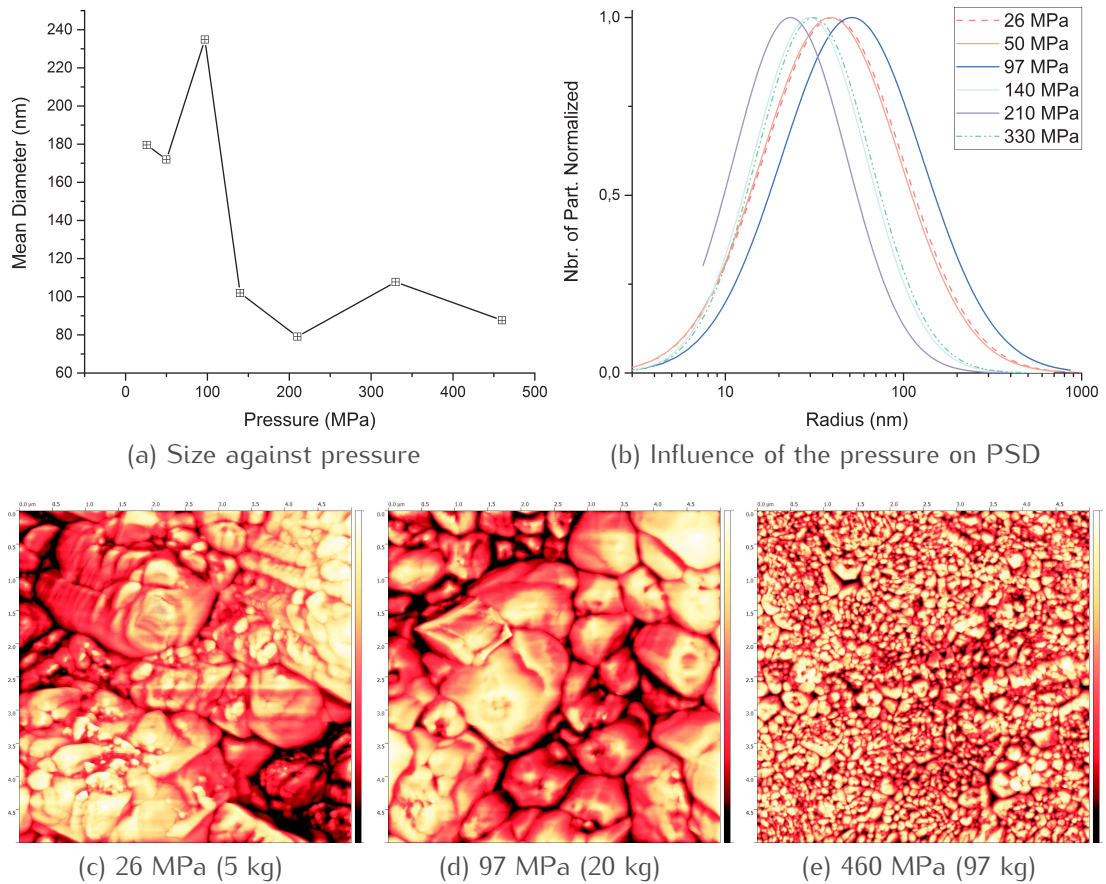


Figure 3.3 – Effect of the weight; same face, no microtomy, $5\mu\text{m} \times 5\mu\text{m}$ for $1024\text{px} \times 1024\text{px}$, enhanced contrast.

Pressure (MPa)	Raw	With Microtomy
12		280
26	180	
50	170	230
97	235	140
140	100	
210	80	
330	110	
460	90	

Table 3.6 – Mean Diameters (nm) according to the pressure applied and the pre-treatment by microtomy; by SEM, the mean size is 500 nm.

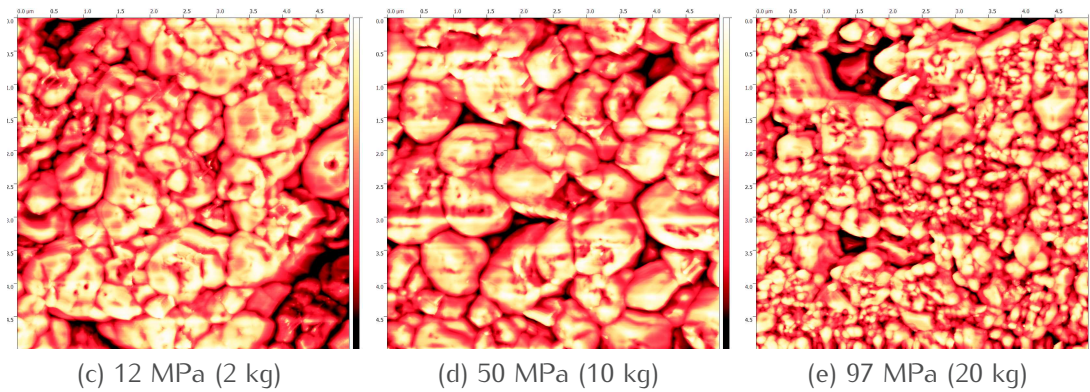
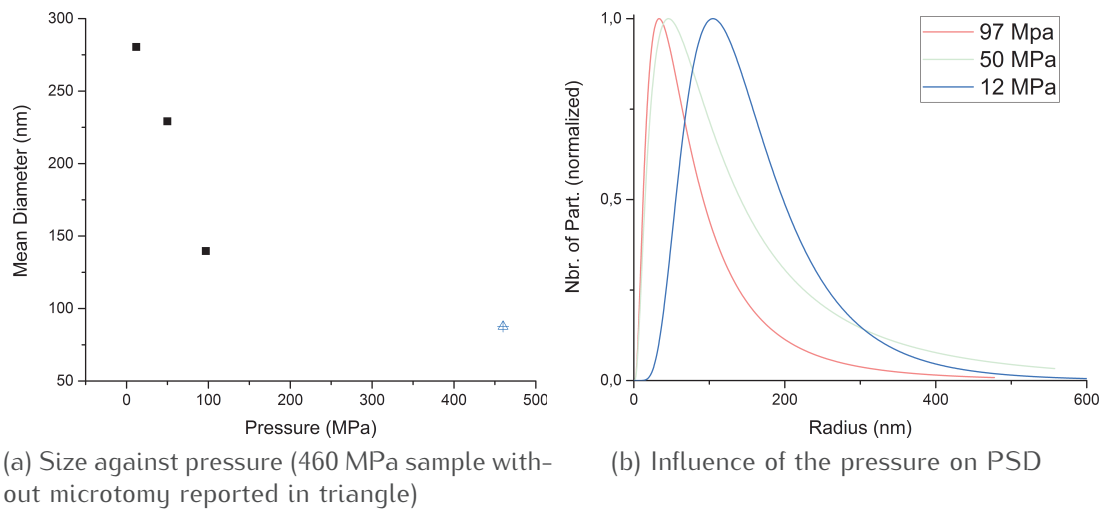


Figure 3.4 – Effect of the weight; same face, processed by microtomy, $5\mu\text{m} \times 5\mu\text{m}$ for $1024\text{px} \times 1024\text{px}$, enhanced contrast.

3.1.2.4 Conclusion on the AFM pellet method

The particle size variation when adding PVP or PolyEthylene Glycol (PEG) studied from SEM in Chapter 5 where initially discovered from the analysis of pellets by AFM. The exact same trend from SEM was also found from AFM picture analysis whose results can be found in Table 3.7. However, instead of a particle size around 160 nm as found by direct imaging in SEM, a mean value around 70 nm is measured. The content of polymer seems to have no influence on how brittle is the energetic material since PEG samples also have an increasing size with the PEG content: those results show that not only the hardness of the material is a major parameter but also the initial size of the particles. This seems to be valid only when the pressure applied is below the critical pressure. Another interpretation would be that this critical pressure changes; for instance it could

have decreased for RDX/PVP samples, thus leading to one of the smallest PSD ever observed on RDX.

Compound(s)	Polymer content (wt%)	Mean Diameter AFM (nm)
RDX/PVP40K	1	66
RDX/PVP40K	1	73
RDX/PVP40K	1	67
RDX/PVP40K	0,5	165
RDX/PEG400	1	965
RDX/PEG400	0,1	180

Table 3.7 – Particle size from pellet imaging by AFM of some samples at 97 MPa with microtomy.

SEM pictures were taken from pellets made from n-RDX by the pressing technique mentioned above, in order to observe at larger scales their surface. After being pressed and imaged by AFM, the sample is cut in half to be analysed by SEM on one piece; the other is used as a reference.

Thanks to the results in Figure 3.5, the surface of pellets appear to have two different areas: linear grooves and holes. The holes let the inside of the pellet to appear from outside; those are rough and bumpy which is a problem for AFM. However, the particles seen from inside are very similar in size and shape to the ones observed from the loose powder. In the Figure 3.7, the particles inside have the same rounded shape as in the loose powder. On the contrary, the grooves are smooth and made from the smaller particles; those areas are perfect for landing an AFM tip and scan. The AFM method suffers so from an additional bias which is the area segregation. To land the tip, to initialize the scan and to have a correct AFM picture, the tip is moved until the scanning area is flat enough: the biggest particles inside the holes of the pellet are never investigated. Surfaces of pellets of energetic materials are not representative of the loose powder of the same material.

The comparison between AFM and SEM of the same sample clearly illustrates the reason behind the particle size difference between those two techniques. The press hardens the pellet, the microtome mills the surface and scanning by AFM selects the flattest area where the smallest particles lies.

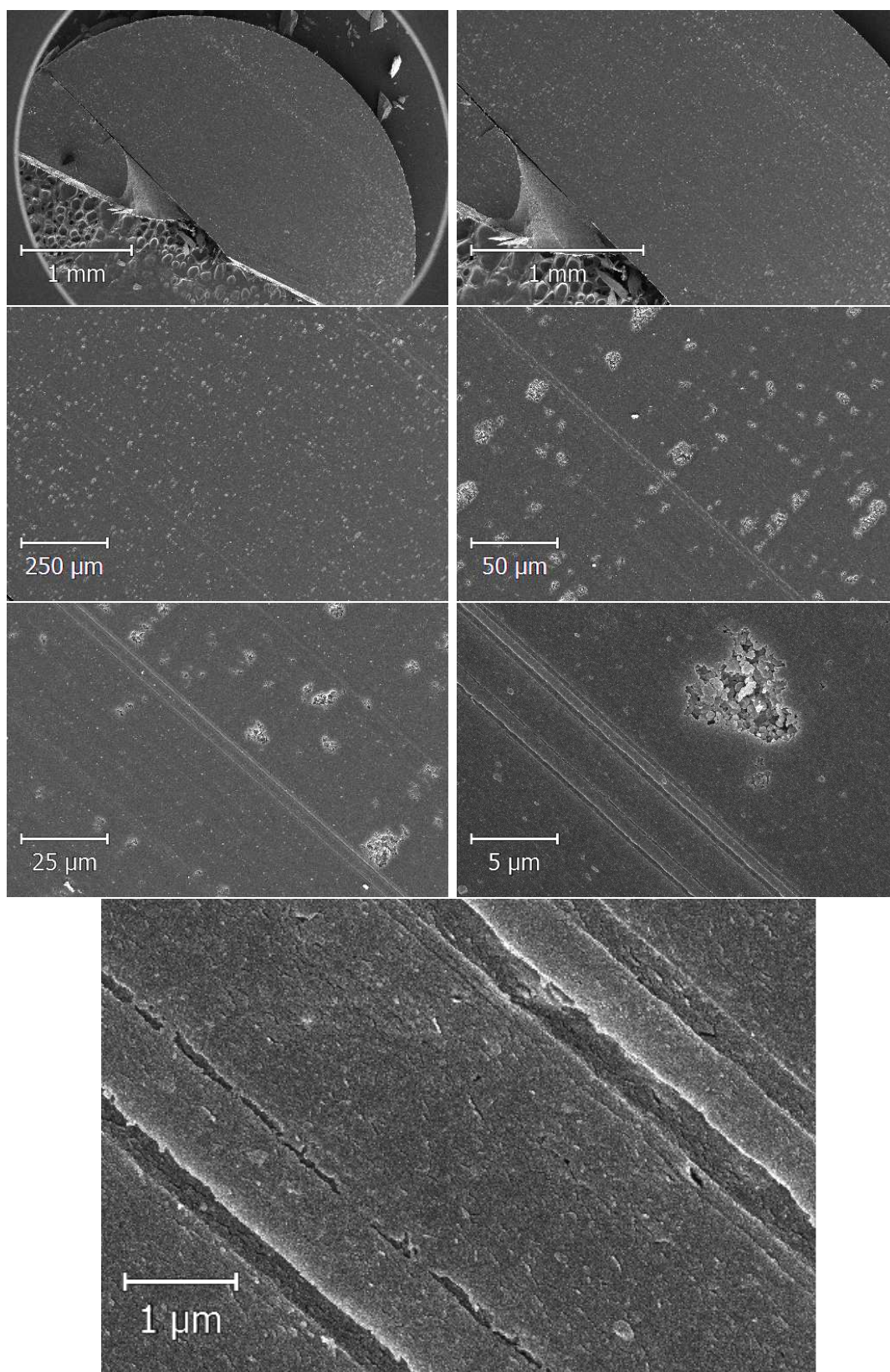


Figure 3.5 – SEM imaging of a 97MPa pellet of RDX processed with 5wt% of PVP 40000.

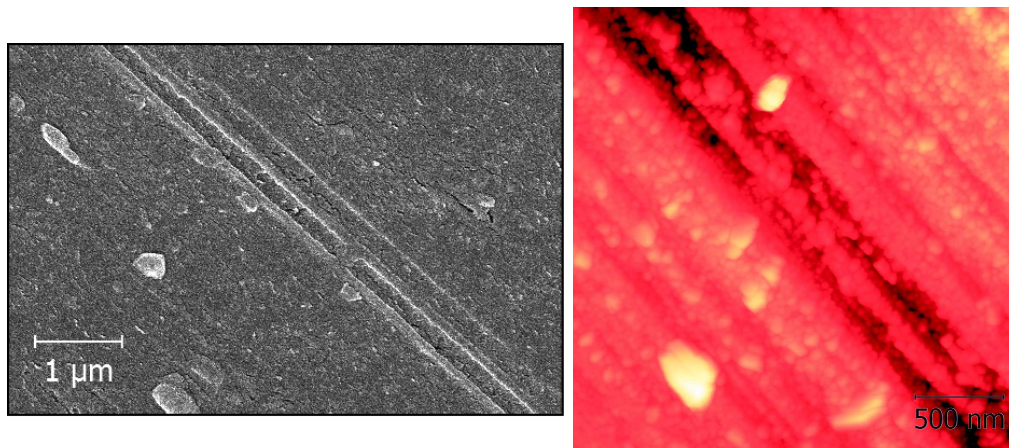


Figure 3.6 – SEM and AFM imaging of a 97 MPa pellet of RDX processed with 5 wt% of PVP 40000.

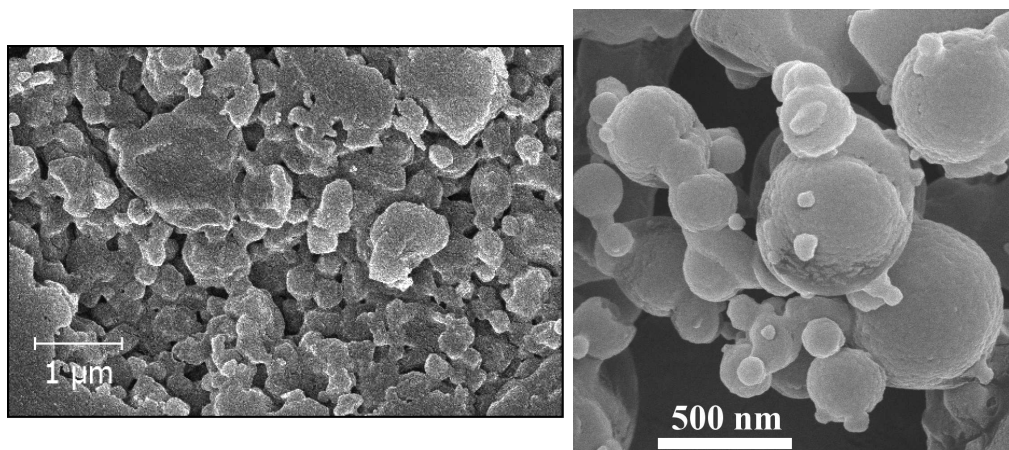


Figure 3.7 – SEM imaging of one hole of a 97 MPa pellet compared to the loose powder of the same sample of RDX processed with 5 wt% of PVP 40000.

3.2 One Technique, One Size

3.2.1 XDR

3.2.1.1 Determination of the apparent volume weighted domain size

From an XRD pattern, many information can be extracted. The mean crystallite size can easily be calculated from the Scherrer equation, the strain inside the crystal is available from more advanced analysis such as Williamson-Hall, and the morphology of the crystallite can even be 3D-modeled from a fine Rietveld refinement.

The Scherrer equation is a quick method to determine the average coherence length, so it is widely used. However, the value is calculated from the broadening which is influenced by many other physical parameters such as the lattice strain. Williamson et al. (1953) defined a alternative method taking into account the strain contribution into the broadening. Explained in the Section 1.4.2 p. 49, the analysis relies on plotting $\beta \cos(\theta)$ as a function of $\sin(\theta)$ and fitting it to an affine function where the slope is directly related to the strain.

Results in Figure 3.8 show the attempt to fit five n-RDX samples crystallised through SFE in the same operative conditions. The sub-figure A, on the left, illustrates different approaches in measuring the Full Width at Half Maximum (FWHM) according to the angle: due to the poor accuracy of the peak per peak measurement (peak fit from Origin or manual peak marking in EVA), data seems to be linear in the range 0.1-0.2. This also explains the large difference with the Full Pattern Matching (FPM) analysis: FPM relies on the whole pattern allowing a large number of peaks to be analysed by an algorithm. The usual mathematical functions to fit XRD peaks are implemented in the code, and the software compares the experimental data to the theoretical hkl planes calculated from the space group. The FPM is therefore more accurate, computes a large dataset and has a real meaning. Our XRD diffractometer does not filter the $K_{\alpha 2}$ ray of the Cu source: so each peak is actually a double-peak. The FPM as implemented in Fullprof can fit the pattern knowing the peak position for each radiation thus deconvoluting each peak in two. The peaks shape was fitted with a Thompson-Cox-Hastings pseudo-Voigt convoluted with axial divergence asymmetry function (Finger et al. 1994).

In Figure 3.8, only two samples could have been fitted into a linear regression. The other three evolve into parabolas. Such diverging results clearly indicates that the Williamson-Hall theory does not describe accurately the peak broadening.

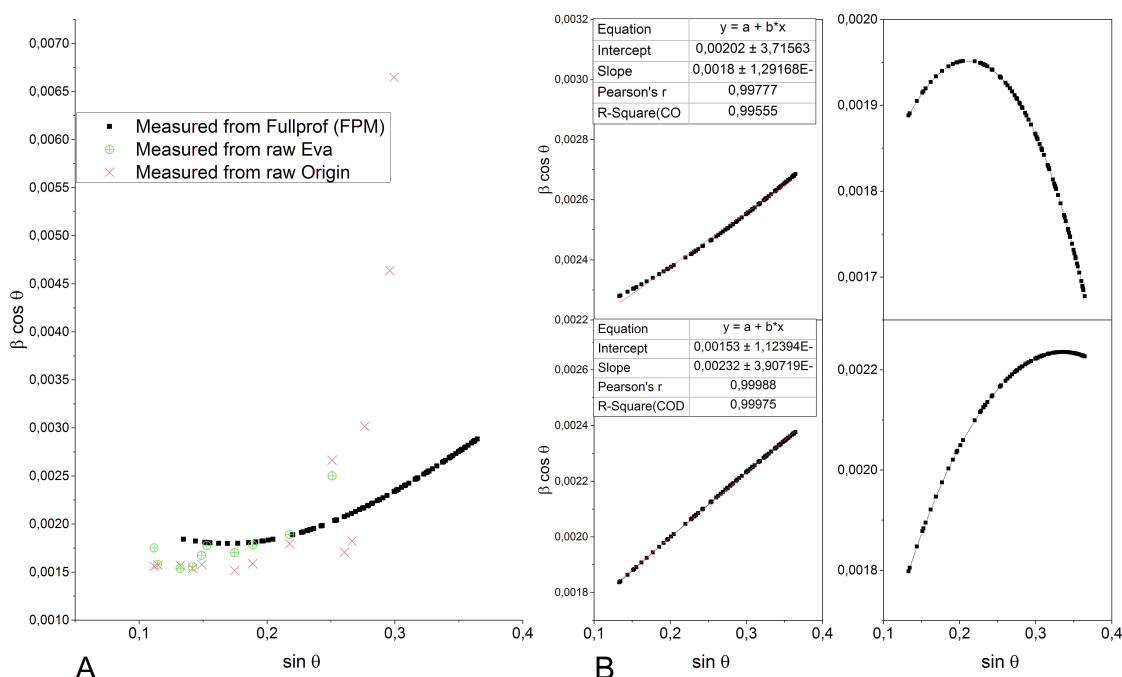


Figure 3.8 – Williamson-Hall of *n*-RDX processed by SFE at 2 wt% in acetone.

3.2.1.2 Rietveld refinement

The Rietveld refinement allows the fine analysis of the crystals properties (size and strain according to several models, hkl shifts, asymmetry, preferred orientation etc.) but also a complete segregation with instrumental effects on the pattern.

In most implementation of the Rietveld method, to refine crystallite structures, the microstructure (size and strain) of each lattice is modelled by considering only an average crystallite size. Although this technique gives good results, it is important to notice that the real sample has a distribution of the crystallite sizes. Usually such models for the crystallite size approximate the crystallite shape with a sphere. Some even more complicated models consider a specific morphology of the crystallites. But, the best results for the average crystallite size are obtained by modelling its shape in the reciprocal space with an expansion of symmetrized spherical harmonics; then the corresponding crystallite shape obtained in the real space would be the one obtained from direct imaging of the primary particles.

The micro-structural analysis from Rietveld refinement is implemented in several size broadening models into the free software Fullprof. We will be using the Anisotropic Lorentzian size broadening: it considers the size broadening as a linear combination of spherical harmonics (SPH). The anisotropic size is

supposed to contribute to the Lorentzian component of the total Voigt function. After refinement of the coefficients the program calculates the apparent size (in Ångströms) along each reciprocal lattice vectors if the instrumental resolution is provided.

A preliminary calibration of the peak broadening due to the apparatus is performed on LaB_6 : the resulting refinement can be seen in Figure 3.9. If the peak broadening is too close to the instrumental resolution, the software will not refine the peak. The Table 3.8 contains the values used for all the following Rietveld refinement. U, V and W are parameters used to model the change of the FWHM with the angle from the instrument, by the equation $H^2 = U \tan(\theta)^2 + V \tan(\theta) + W$. The peak shape for LaB_6 is a Pseudo-Voigt; the parameters were adapted from the instrument parameter and input files of the Beamline 11-BM of Argonne National Laboratory. Then, n-RDX patterns are refined using a Thompson-Cox-Hastings pseudo-Voigt convoluted with axial divergence asymmetry function as the peak shape (Finger et al. 1994). Therefore, the FWHM of the Gaussian (H_G) and Lorentzian (H_L) components are calculated as:

$$H_G^2 = (U + D_{ST}^2) \tan^2 \theta + V \tan \theta + W + \frac{I_G}{\cos^2 \theta} \quad (3.1a)$$

$$H_L = X \tan \theta + \frac{[Y + F(S_Z)]}{\cos \theta} \quad (3.1b)$$

Much more technical details can be found in the manual and help provided with FullProf.

Uins	Vins	Wins	Xins	Yins	Zins
0.001356	-0.005000	0.003910	0.063891	0.000083	0.0
0.001356	-0.005000	0.003910	0.063891	0.000083	0.0

Table 3.8 – Instrumental resolution determined from LaB_6 pattern refinement.

The Rietveld refinement requires some expertise and patience to analyse with accuracy and avoid any divergence of the parameters toward non physical meanings. The process is made step by step following this sequence:

1. Scale factor
2. Scale factor, zero point of detector, lattice constants. The background is refined if the background subtraction from EVA is not satisfactory.
3. Atomic positions

ALS 11-BM - NIST SRM 660a LaB₆

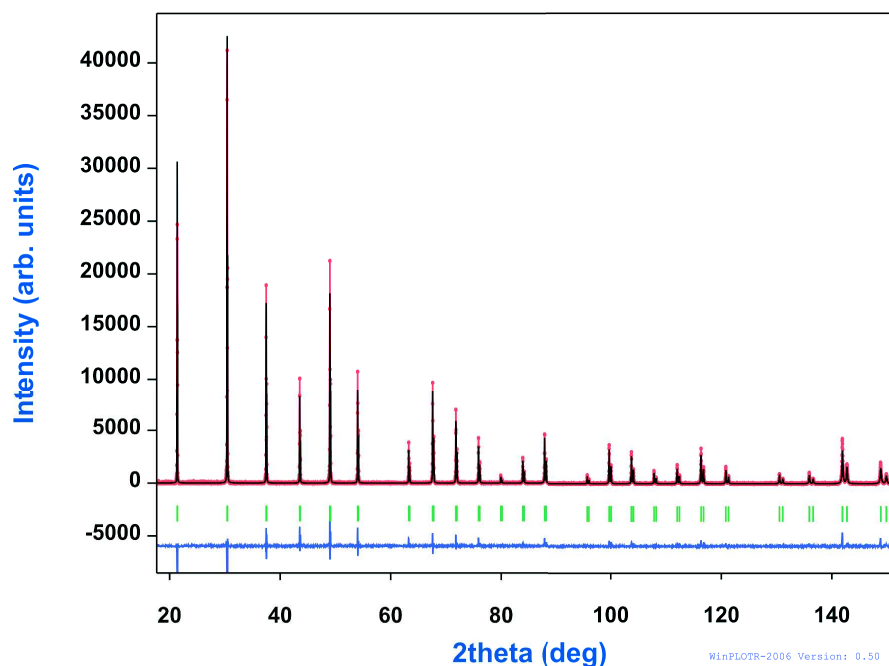


Figure 3.9 – Rietveld refinement performed on LaB₆.

4. Peak shape and asymmetry parameters
5. Atom occupancies
6. Microstructural parameters: size and strain effects. The model used is the Anisotropic Lorentzian size broadening (Spherical Harmonic) with the Laue class *mmm*, which allows the crystallite morphology determination.

The experimental pattern, refinement and residual are frequently checked during the refinement process. The final results are found in the Figures 3.10 to 3.14: the curves in black is the refined pattern, in red the experimental data and in blue below the first two is the residual. The small ticks between the residual and the curves are the hkl positions from $K_{\alpha 1}$ and $K_{\alpha 2}$ rays of the Cu source. The refinement takes a dozen minutes, with an increasing computation time when adding parameters to refine. Also the refinement diverges easily, corrupting the input file. Dozens of refinements were saved per samples with reducing χ ; attempts increasing χ were not saved but are sometimes used to start from original values leading afterwards to a more accurate solution.

The refinements of the sample of n-RDX processed pure at 3 wt% acetone in Figure 3.11 and the one with a 80 μm nozzle in Figure 3.14 are acceptable but

less accurate than others, with a negative residue on the angles at small angles and a positive residue on angles above 20° . Finding a realistic refinement was the most difficult issue to solve: having a refinement accurate enough with no bias –such as that angular dependency– and an acceptable 3D model at the same time. The results shown here are the best refinement possible with a realistic 3D model. The three other refinements are in very good agreement with the experimental data.

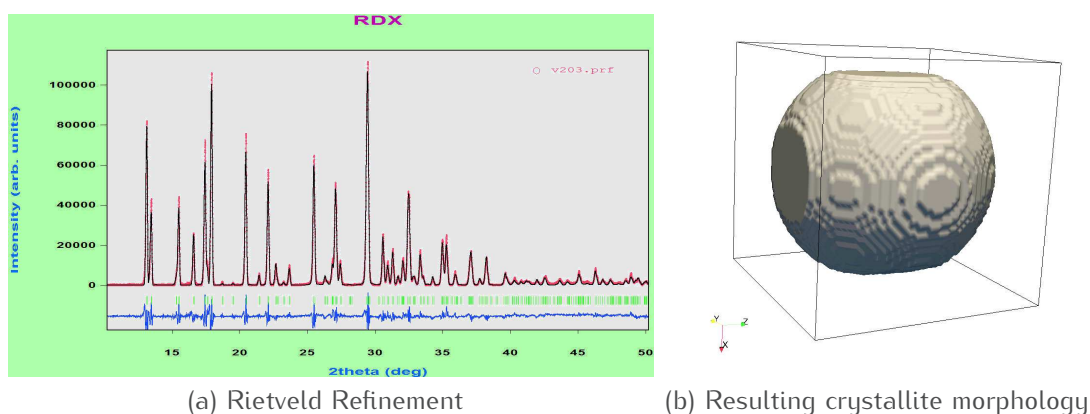


Figure 3.10 – Sample of *n*-RDX processed pure at 2 wt% in acetone.

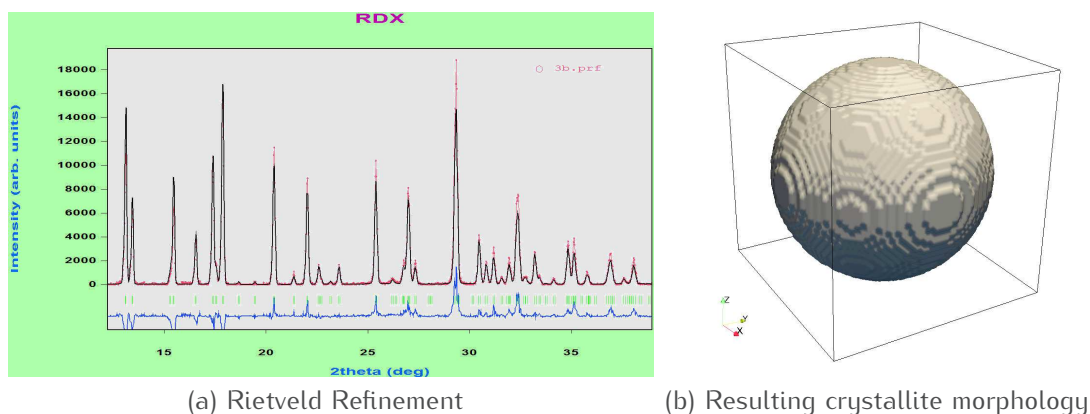


Figure 3.11 – Sample of *n*-RDX processed pure at 3 wt% in acetone.

A global appreciation on the refinement would be a more accurate fitted solution with the smallest particles. Beyond the inherent difficulty of the micro-

structural analysis by the Rietveld theory, the organic crystals exhibit a large number of peak with many overlaps, and a natural broadening due to a lattice crystalline less ordered, which is far from the ideal condition.

Nevertheless, all the models seem to converge on spherical particles slightly flattened on two planes (4 faces/extremity). This oblate geometry is correlated to an almost homogeneous growth with no preferential direction growth. Size and morphology found with those analysis are then compared to the particle size and morphology obtained by AFM on pellets and on the smallest particles imaged on SEM.

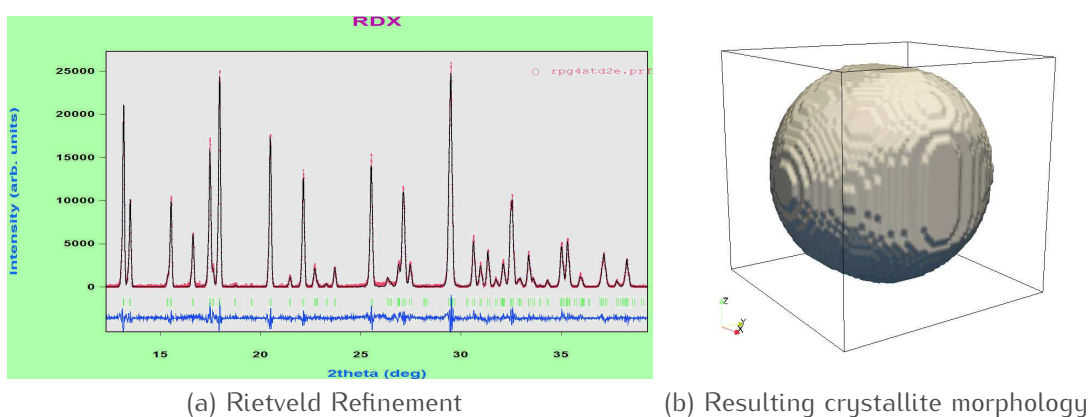


Figure 3.12 – Sample of *n*-RDX processed with 0.1 wt% of PEG.

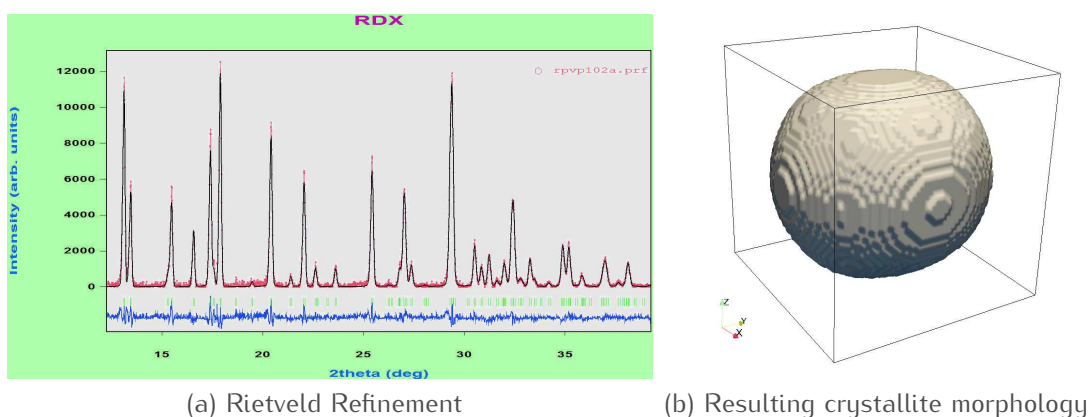


Figure 3.13 – Sample of *n*-RDX processed with 10 wt% PVP.

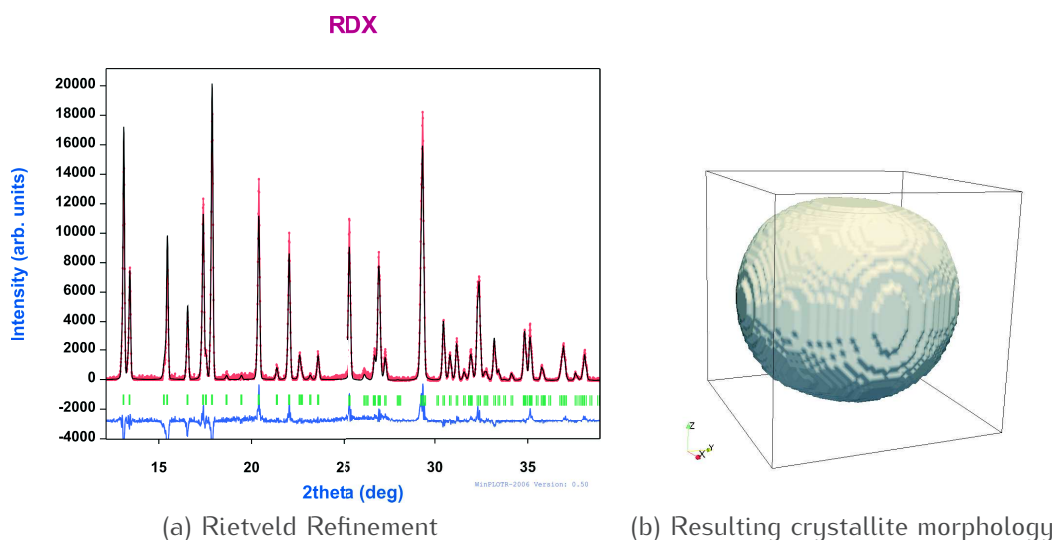


Figure 3.14 – Sample of *n*-RDX processed with 1 wt% PVP with a 80 μm nozzle

3.2.2 Smallest observable object

In order to assess the problem of the particle size and definition of a particle, a new deposit technique for SEM was developed recently in our laboratory: it is based on the rubbing of the powder between two glass sheets. Individual and very small particles have been found to be more easily observed on a glass support. The method is still under investigation, especially to explain the influence of the support. However the spreading due to the rubbing allows the distinct imaging of the smallest particles. The particle size and morphology is studied through SEM and compared to the results from Rietveld refinement. The aim of this study is to answer to the questions of the crystallinity and aggregation of *n*-RDX processed by SFE.

Spray techniques may produce particles made from much smaller primary particle: Qiu et al. (2015) successfully probed the interior of their micrometer spheres (RDX) to found out a gradient of the primary particle size at the submicrometer scale. Focused ion beam (FIB) is the technique used to make the cross-sections: even if a low probe current helps to preserve the sample (Gierak 2009) no attempt has already been reported on energetic materials. An easiest solution is to use the rubbing deposition technique to image the smallest particles. Results reported in Table 3.9 show that the RDX processed with polymers actually exists as single crystals. On the contrary, the smallest pure *n*-RDX are still polycrystalline. The oblate shape found by Rietveld seems consistent with morphology imaged by SEM, as it can be seen in Table 3.9.

AFM on pellets of those samples were also analysed. As seen in Figure 3.16,

n-RDX	Average apparent size and standard deviation (anisotropy) (Å)	Average maximum strain and standard deviation (anisotropy) (% (x 10000))	Smallest Particle Sizes from SEM (nm)
pure at 2 wt% in acetone	716 (28)	5.53 (0.0039)	180-200
pure at 3 wt% in acetone	814 (21)	3.23 (0.0017)	125-140
with 0.1 wt% of PEG	826 (27)	5.61 (0.0046)	70-70
with 10 wt% PVP	769 (21)	8.58 (0.0068)	60-60
with 1 wt% PVP with a 80 µm nozzle	793 (29)	6.87 (0.0048)	80-95

Table 3.9 – Smallest particle imaged on SEM compared to the computed average apparent size from Rietveld refinement.

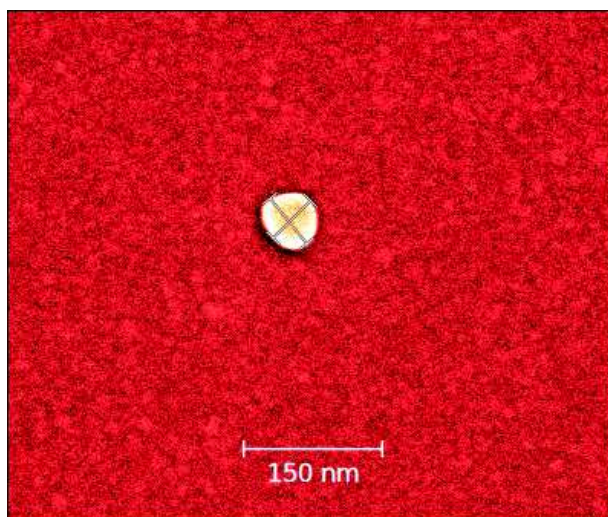
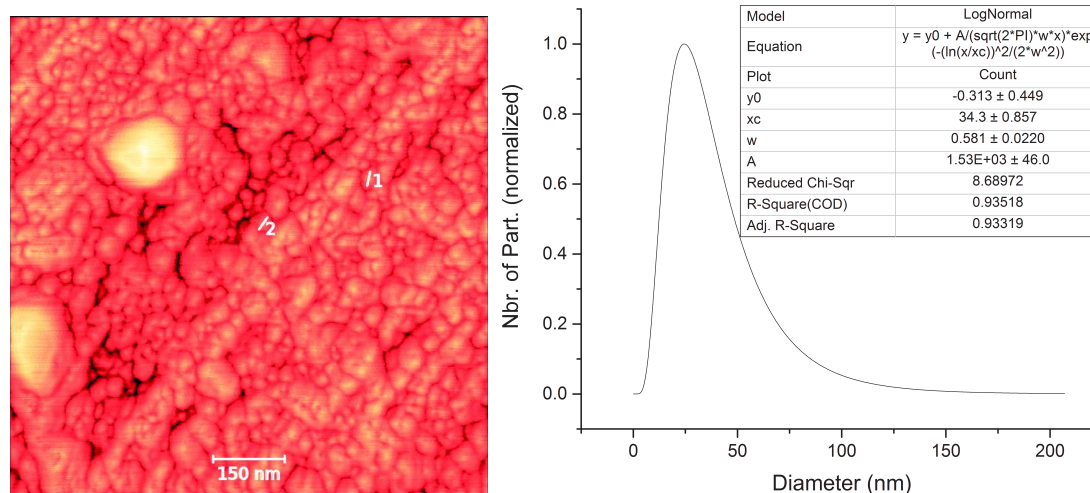


Figure 3.15 – One of the smallest particle (63x58 nm) observed by SEM on RDX processed with 10 wt% PVP.



(a) AFM topography. The length of the marked particle is 30 nm

(b) Particle Size Distribution: mean at 35 nm

Figure 3.16 – *n*-RDX processed with 10 wt% PVP.

even much smaller particles were measured –after the surface milling– when adding more polymer and reducing the original particle size (the ones imaged by SEM). For pure *n*-RDX the sizes of the smallest particles stay in the same range as the particle size from AFM below the critical pressure without microtomy: this confirms that due to the segregation by AFM the smallest particles are scanned, thus implying that below the critical pressure the particles may stay unbroken. Those results raise again the question of the hardness of the nanoparticles. Since the smallest particles imaged in SEM are bigger than the one observed by AFM, the rubbing method does not bring an energy (friction work and pressure) as high as in the case of the AFM pellets: that technique seems suitable to spread the particles without breaking the brittle particles.

3.3 Summary of the Chapter

Several sizes have been measured depending on the technique and the conditions. By AFM, pellets are imaged, without or with microtomy to flatten the surface; many samples were analysed by this technique at 97 MPa plus microtomy such as the result reported by Spitzer et al. (2014) or the preliminary study with a range of RDX content. Classical SEM were made on loose powder and pellets, and a rubbing technique has been developed to spread particles on a glass substrate in order to image the smallest particles. The lattice structure and the apparent volume weighted domain size were computed from Rietveld

refinement. All that high amount of data were interpreted and correlations between techniques have been found.

n-RDX can be broken in smaller particles by compression. For pure compounds and below a critical pressure, the particles observed by AFM are about 200 nm with a irregular round shapes; that size and morphology is the same as imaged on the smallest particles, by the rubbing technique by SEM. When using a microtome on n-RDX pellets, the surface is milled and the blade imperfections imprint grooves on the surface or strip off parts which reveal the original particles inside the pellet, as seen by SEM. By AFM a segregation is made by the roughness of the surface: those holes with bigger particles are never scanned on the pellets processed by microtomy, thus only the smallest particles are counted. That bias also explains why size and shapes on AFM can be identical to the smallest particles imaged on SEM.

XRD patterns analysed by Rietveld refinement reveal an average apparent size around 80 nm with an oblate morphology for all samples, meaning that an homogeneous growth occurs in all SFE conditions. The smallest particles imaged by SEM seem to be single crystals in the case of n-RDX processed by polymers.

As the particles sizes after mechanical stress depend on purity and quantity of polymer, the hardness is probably a key property for a deeper comprehension of the phenomenon reported in this chapter. Nano indentation is used to study the mechanical properties of material: Hudson et al. (2012) found that micron-sized crystals with many internal defects have reduced modulus of elasticity, stiffness and prone to greater deformation under applied load, therefore correlate shock sensitivity and stiffness/elasticity. Nano mechanical tests can be done under the direct visualization of an SEM or Transmission Electron Microscopy (TEM). However, due to the already mentioned difficulties to image energetic organic nanoparticles, such experiments would require a dedicated scientific study.

After being able to define an absolute particle size representative of the sample, the reduction of the particle size can be studied without bias; the crystallisation has to be controlled in both space and time resolution. Two main approaches have been established, a chemical one and a more physical one. The next chapter focuses on the physical attempt by the exploration of various supersaturation conditions, just after introducing all the needed concepts for the formation of organic crystal, with a specific focus on the nucleation.

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Chapter 4

Crystallisation study and comprehension of the SFE process

4.1 Crystallisation, Nucleation and supersaturation

Crystallisation from solution occurs when the concentration of the compound is higher than its solubility, namely in the supersaturation zone. Various strategies can be used since the solubility depends on the temperature, the solvent(s) and other compound(s): temperature change (cooling in the case of a positive gradient $\frac{dC}{dT}$ of the solubility curve or heating in the case of a negative one), solvent removing (evaporation), addition of a drowning-out agent (an anti-solvent) or reaction partners. But achieving the supersaturation may not be enough; to trigger the crystallisation in that metastable system, an external energy (stirring, mechanical shock, friction or extreme pressures) or a seed (impurity or a crystal of the compound) can be brought to the solution. Others stimuli such as electric and magnetic fields, spark discharges, UV light, X-rays and ultrasonic irradiation have also been studied since decades (Atwood et al. 1969) but no application in large-scale crystallisation has been ever reported.

Three types of nucleation can be distinguished. The secondary nucleation occurs when a crystal already exists: a seed triggers the nucleation of the metastable solution or the compound nucleates on the surface of the growing particles. Primary nucleation can be spontaneous –homogeneous nucleation– or triggered by impurities –secondary nucleation–. Since impurity free solutions are virtually impossible, cases are often reported when a system nucleates at a few degrees lower than predicted or than the previous smaller batches (Mullin 2001). The exact formation of nuclei is still not known (Sosso et al. 2016). The molecules have to coagulate, then to resist to re-dissolution but since the lattice faces are not equivalent, the molecules should have the right orientation. Even

the mechanisms are not resolved yet, a nucleus has to achieve a critical size to actually grow into a crystalline particle. From the Classical Nucleation Theory, the critical radius corresponds to the one minimizing the overall excess Gibbs energy ΔG :

$$\begin{aligned}\Delta G &= \Delta G_S + \Delta G_V \\ &= 4\pi r^2 \gamma + 4/3\pi r^3 \Delta G_V\end{aligned}\quad (4.1)$$

$$\Rightarrow \frac{d\Delta G}{dr} = 8\pi r \gamma + 4\pi r^2 \Delta G_V = 0 \quad (4.2a)$$

$$\Rightarrow r_c = \frac{-2\gamma}{\delta G_c} \quad (4.2b)$$

ΔG_S is the excess Gibbs energy between the surface of the particle and the bulk, and ΔG_V is the volume excess Gibbs energy between a large (infinite) particle and the compound dissolved. $\Delta G_S > 0$ while $\Delta G_V < 0$. ΔG_S relies on the interfacial tension –also called surface energy– γ and ΔG_V is the volumetric volume excess Gibbs energy. Therefore, critical overall excess Gibbs energy can be expressed as:

$$\Delta G_c = \frac{16\pi\gamma^3}{3(\Delta G_V^2)} \quad (4.3)$$

The supersaturation S is expressed as a ratio between the concentration c and the solubility s at the given temperature: $S = c/s$. With the Gibbs-Thomson relationship, the supersaturation becomes with v the molecular volume:

$$\ln S = \frac{2\gamma V}{RT r} = \frac{2\gamma v}{k_B T r} \quad (4.4)$$

So from the Equations (4.3) and (4.4), we can finally express the critical overall excess Gibbs energy with the supersaturation:

$$\Delta G_c = \frac{16\pi\gamma^3 v^2}{3(k_B T \ln S)^2} \quad (4.5)$$

To go further, the rate of nucleation can be written as an Arrhenius velocity equation $J = A \exp(-\Delta G/kT)$, which is given from Equation (4.5)

$$J = A \exp\left(-\frac{16\pi\gamma^3 v^2}{3(k_B T)^3 (\ln S)^2}\right) \quad (4.6)$$

The rate of nucleation finally relies on the temperature, surface energy and the supersaturation, and has been plotted in Figure 4.1a; after a critical value

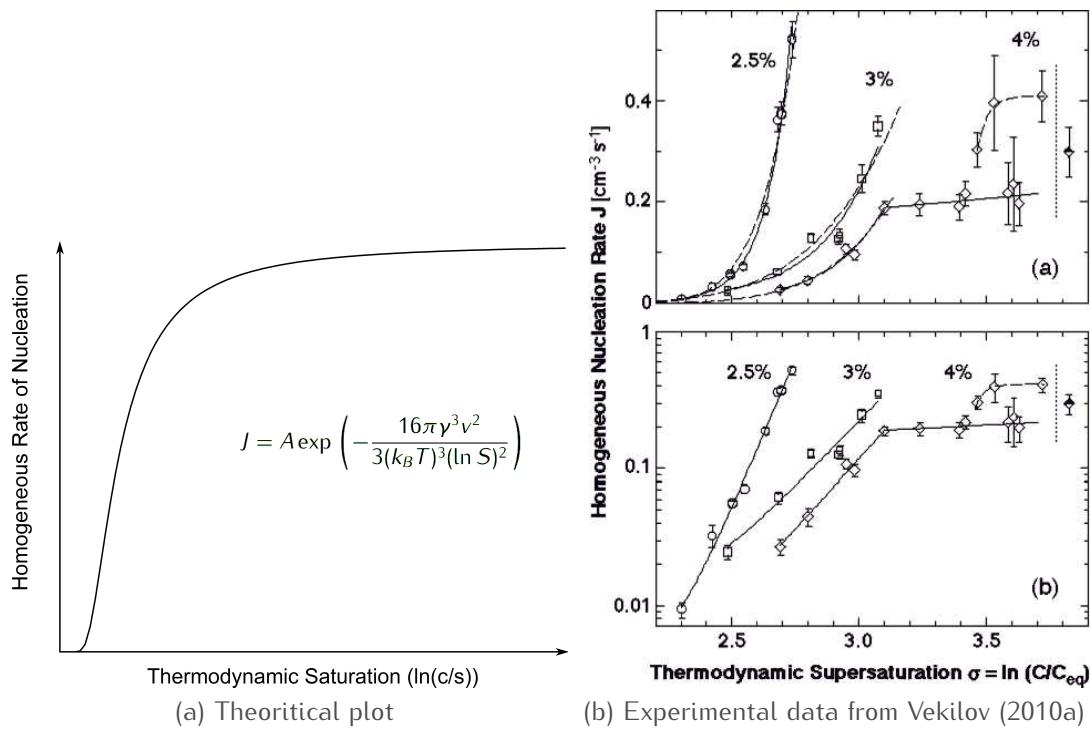


Figure 4.1 – Rate of nucleation against the supersaturation.

the rate increases rapidly up to an asymptotic rate. The experimental values in Figure 4.1b are in good agreement with a sudden increase followed by a plateau.

However, many efforts have been devoted since 2010 to extend and improve the Classical Nucleation Theory (CNT) (De Yoreo 2013; Gebauer et al. 2014; Vekilov 2010b; Zahn 2015). On the contrary of melts where the liquid is dense enough to neglect concentration gradients and related phenomena, the case of crystal nucleation of molecules in solution is quite different. A significant concentration fluctuation is required to bring the needed number of molecules to construct the nuclei. That's why a two-step mechanism was developed recently where two free energy barriers have to be overcome instead of a unique one expressed in Equation (4.1) from the CNT: as displayed in Figure 4.2, the first one illustrates the density variation to create a primary cluster of molecules, then the second one describes the ordering of those clusters into the crystalline nuclei. Early stages of the nucleation of organic crystals have been investigated using Molecular Dynamics (MD) backed up with experimental data from single-molecule real-time transmission electron microscopy (SMRT-TEM); Salvalaglio et al. (2015, 2012) demonstrated that different solvents can lead to different

nucleation mechanisms such as a single-step nucleation process favoured for urea molecule in methanol and ethanol and a two-step mechanism in acetonitrile and water.

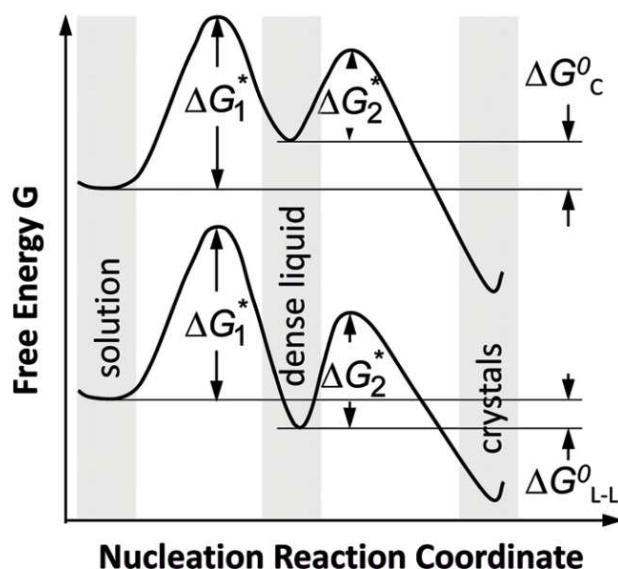


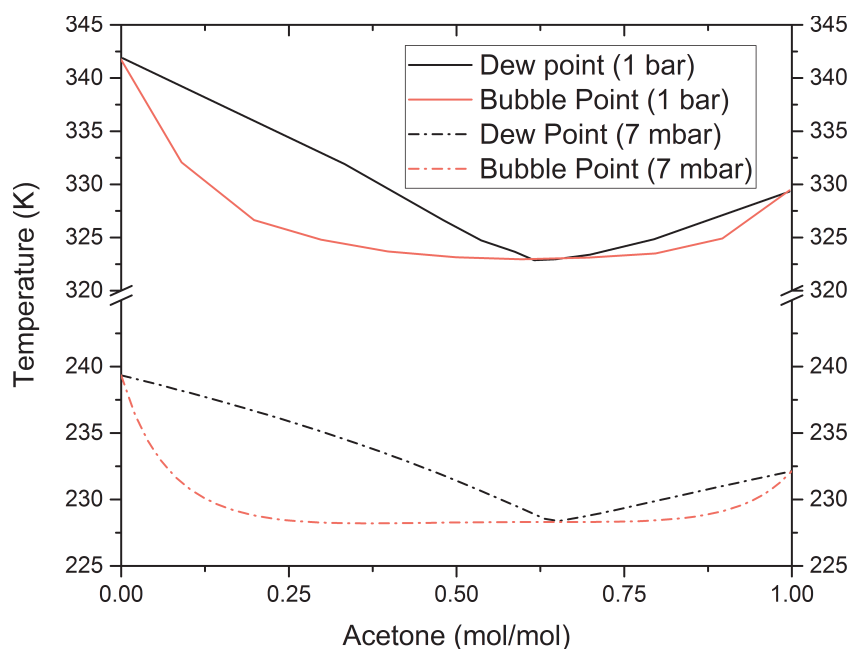
Figure 4.2 – Two possible scenarios from the two-step nucleation mechanism: the first one involves an intermediate state at a higher energy due to an unstable dense liquid existing as mesoscopic clusters, and the second lower curve applies if the dense liquid is stable ($\Delta G_{L-L}^0 < 0$)

The link between the rate of nucleation and the crystal size is far of being established since several phenomena follow the nucleation: the firstborn nuclei are subject to growth but also aggregation. Thus an optimal value of the supersaturation exists for each system; a supersaturation too high would lead to aggregation and also to secondary nucleation on growing particles.

4.1.1 Increasing Supersaturation in SFE with an Anti-solvent

The key to control crystallisation and so particle size is to determine the supersaturation which is time dependent but also is unique in each droplet. Supersaturation, as a function of time and coordinates, was not available: since we were not able to determine *in situ* droplet size distribution, extreme variations of the supersaturation are investigated. Therefore, a suitable anti-solvent for RDX and for SFE has been searched in order to increase the supersaturation by reduced solubility. Water is commonly used as drowning out agent for RDX recrystallisation (Essel et al. 2012; Gallagher et al. 1992; Lee et al. 2014), but due

to a high temperature of evaporation and a modest heat capacity (75.28 J/mol K at 25°C), such solvent can not be processed by SFE: a flash evaporation can be triggered but a quick condensation will occur thus wetting the particles.



(a) Vapor-Liquid Equilibrium (VLE) diagram

pressure	temperature (K)	x (acetone)
1 bar	323	0.648
7 mbar	228.5	0.621

(b) Azeotropes

Figure 4.3 – VLE of the binary system acetone-hexane at 1 bar (solid lines) and 7 mbar (dashed lines): the data at 1 bar are obtained from the Dortmund Data Bank, and curves at 7 mbar are computed from ProSim.

n-Hexane is a perfect non-polar solvent of RDX (PANT et al. 2013). n-Hexane is miscible with acetone and has a low boiling point of 342 K at atmospheric pressure, a high vaporization enthalpy around 31 kJ/mol and a remarkably high heat capacity of 195.8 J/mol K at 298 K. All of those thermodynamic properties are better than any solvent studied by PANT et al. (2013). Moreover, n-hexane forms an azeotrope with acetone: Vapour-Liquid equilibrium data at ambient pressure are plotted in Figure 4.3a. Values at reduced pressure close to the

ones in the SFE are computed by ProSim using the Non-Random Two-Liquid (NRTL) model for the activity coefficients. The UNIFAC model was also tested, but lowered the bubble point temperatures by 0.2 K with no change on the azeotrope position. The VLE of an n-hexane/acetone system exhibits significant lower bubble points than both of the boiling temperatures: the azeotrope at atmospheric pressure is 7 ° lower than the standard boiling point of acetone and 19 ° lower than the one of n-hexane.

Beside increasing the supersaturation with a binary system solvent/anti-solvent, an original approach was developed: to understand the flash-evaporation mechanisms, especially the life-time of droplets and the time dependant crystallisation, the SFE system has been upgraded with a second nozzle. An entire second channelling for the new nozzle has been added and build on an existing system. Also the nozzles have to be oriented to effectively overlap the hollow spray cone: to achieve that the piping system has been reconsidered. The Figure 4.4 describes the new system. Due to technical limitations, a lateral distance between the inlet pipe has to be kept and the channelling has to remain parallel up to the heating elements. Therefore the distance between the end of an heater and the nozzle has been minimized and the stainless steel pipes insulated to prevent heat loss. From the experiments made in Section 4.2.2, an optimal angle around 70 ° has been found and used here. For the present study, one system is used to spray RDX dissolved at 2 wt% in acetone through a 60 µm nozzle; the other one sprays n-hexane trough a 80 µm nozzle in order to permanently have a higher flow of hexane over acetone and so to maximize the overlapping. The system was patented in the international version of the patent ("Method for producing cocrystals by means of flash evaporation" 2016).

Several molar ratio were tried: very near the azeotrope at $x_{\text{acetone}} = 0.642$ and two others flanking the azeotrope from far. But due to the specific boiling point curve of the acetone/n-hexane, the three ratio x_{acetone} 0.573, 0.642 and 0.817 correspond to the same boiling temperature at atmospheric pressure and below. Therefore the driving force of the SFE, the superheating, is kept constant and only the variation of the saturation over time varies. Then after the flash of droplets, it assumed that the nucleation already occurred and classical evaporation applies. Finally, depending on the ratio the rare remaining drops will either enrich in acetone ($x_{\text{acetone}} = 0.817$) or in hexane ($x_{\text{acetone}} = 0.573$): that phenomenon could provoke the generation of a secondary PSD. Only a single peak following a log-normal distribution is found from the frequency count of particle size determined by SEM. The classical evaporation is negligible.

The overall mean diameter of RDX particles is quite high; for instance the reference –pure RDX at 2 wt% in acetone– result in a mean diameter of 790 nm instead of the usual 500 nm (Doctoral Thesis Risse 2012). Such an increase

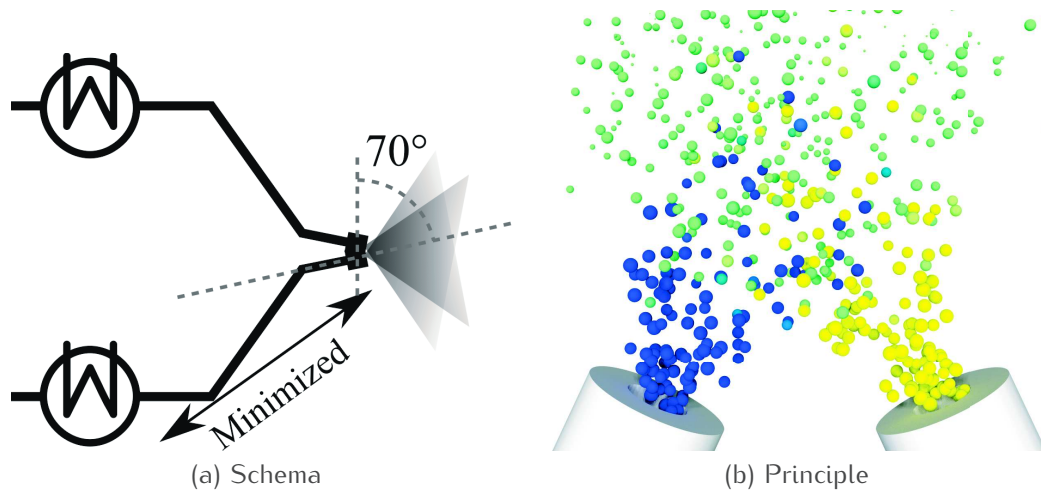


Figure 4.4 – The dual nozzle system.

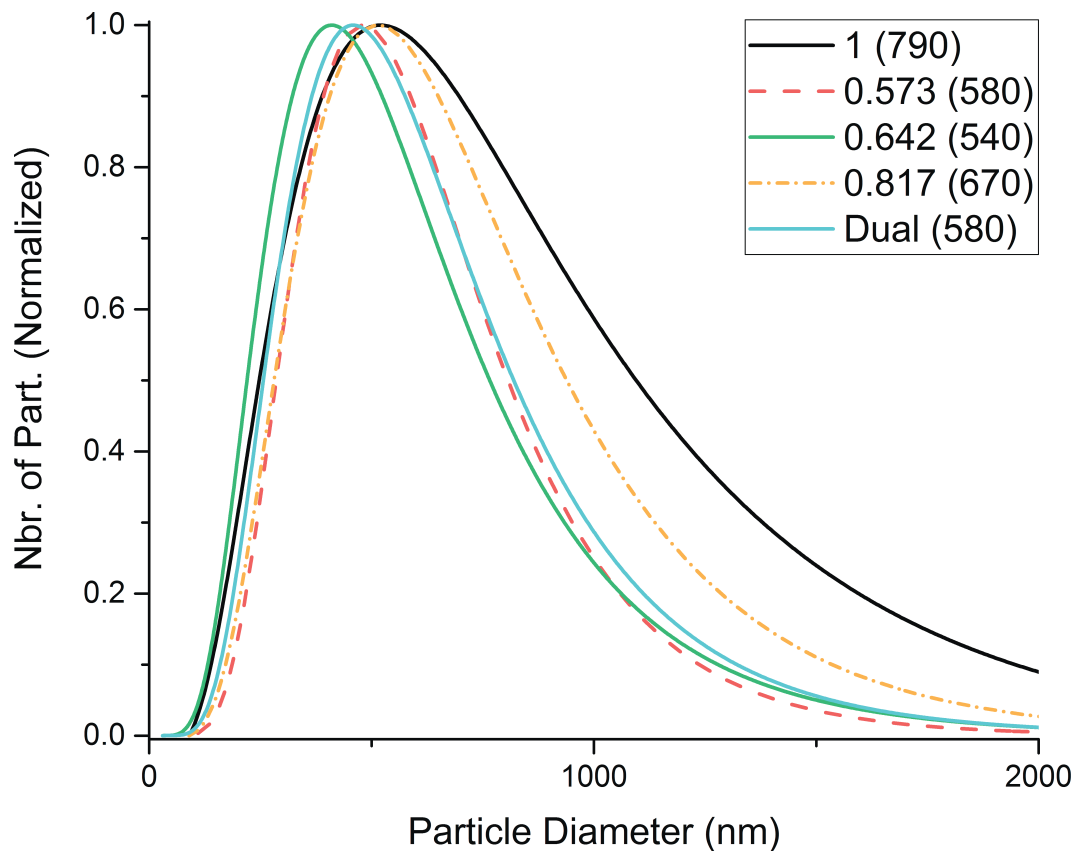


Figure 4.5 – PSD for RDX processed in the binary system acetone/n-hexane by SFE through one or two nozzles; the legend shows the molar ratio of acetone and in parenthesis the mean diameter in nm.

suggest a deterioration of the flash-evaporation due to a lower superheating: the dual nozzle is less efficient to keep the solvent superheated from the heaters to the nozzles because the distance induces higher heat losses. However, the flash-evaporation characteristics such as broadened spray and a lower vacuum pressure are still observed.

From Figure 4.5, the ratio of hexane clearly decreases the particles size from around 800 nm down to around 550 nm. That lower bound already appears for $x_{\text{acetone}} = 0.642$. Increasing the supersaturation up to a certain degree seems to improve the nucleation rate and therefore the particle size with no drawback due to aggregation. The experiment using two nozzles is very informative: droplets have enough life time for an effective overlapping. A possible interpretation would be that acetone droplets are first in a metastable state with no nucleation and no flashing thus allowing them to collide and merge with hexane droplets. The sudden saturation due to a lower solubility in the system acetone-hexane triggers the nucleation in the same conditions as for the one-nozzle at ratio 0.573 and 0.642. So the overlapping induces a ratio of acetone lower than 0.817.

The dual nozzle system has many advantages; in order to increase the mass flow rate, the percentage of the compounds in solution can be raised, then crystallisation is triggered by a second solution containing a drowning out solvent or a crystallisation partner. Advanced chemistry could also be explored when the reactive species should not be mixed until a thermal activation. Two points have to be confirmed first: the droplets interpenetrate each others from both sprays and hexane is not already gaseous thus drying acetone droplets. Therefore a reactive specie is added to the second solution: the cocrystallisation of CL-20:HMX 2:1 is chosen and explained in Section 4.2.

4.1.2 Supersaturation Determination

The supersaturation is a key element which will be unveiled by using the latest advances in LASER and phase Doppler analysers. Particle Image Velocimetry (PIV) were first tried at ambient pressure but is not suitable due to the high density of the spray and limited spatial resolution of the technique. The LASER Doppler technique was first proposed in 1964 by Cummins et al. (1964) but was widely used only in the 70's. The phase Doppler technique exhibited a similar development about 20 years later from Bachdo et al. (1984), Bauckhage et al. (1984), and Saffman et al. (1984). The recent advances in signal filtering and analysis allows now the light-scattering interferometry to simultaneously record in real time object velocities and size distribution. The principle of Phase Doppler Analysis (PDA) is illustrated in Figure 4.6. A measurement volume is defined by the intersection of two focused LASER beams: the light is scattered by the particles passing through this volume. The second refraction order is

specifically used by the three detectors of the PDA probe. Each detector is pre-aligned and converts the optical signal into a Doppler burst with a frequency linearly proportional to the particle velocity. Then the phase shift Φ between the Doppler signals from different detectors allows the calculation of the particle diameter D :

$$\Phi = \frac{-2\pi D}{\lambda} \frac{n \sin \theta \sin \Psi}{\sqrt{2(1 + \cos \theta \cos \Psi \cos \varphi)(1 + n^{2-n} \sqrt{2(1 + \cos \theta \cos \Psi \cos \varphi)})}} \quad (4.7)$$

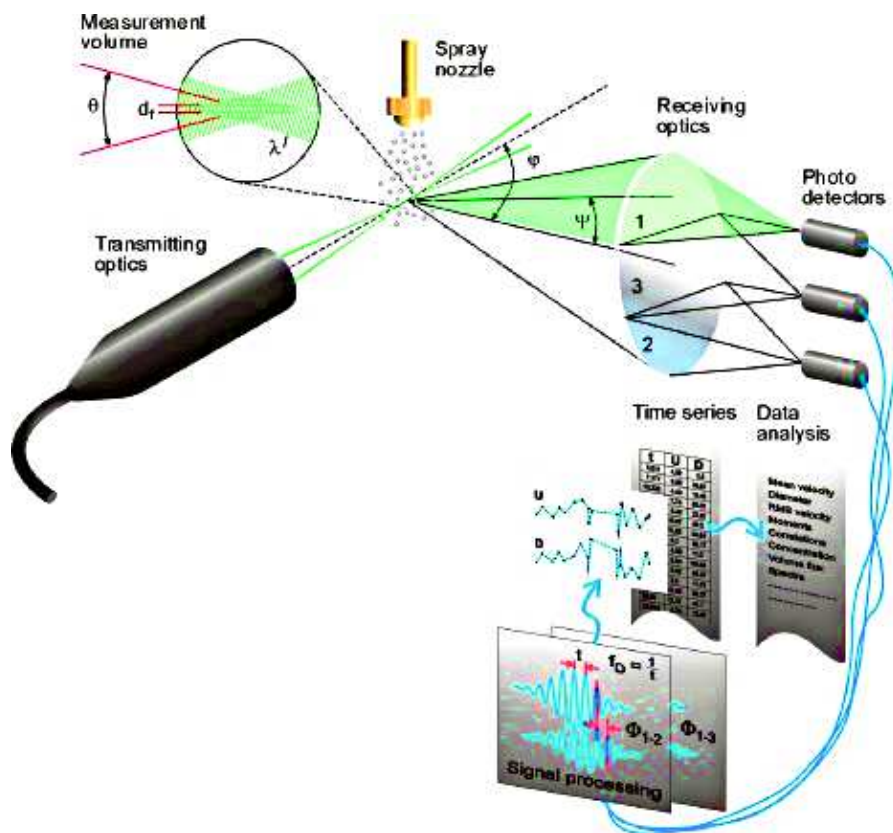


Figure 4.6 – Principle of the Phase Dopler analysis (PDA) in a glance (Dantec Documentation).

Preliminary results from a demonstration apparatus are reported in Figure 4.8. No calibration were performed to assess the accuracy of the apparatus. No optimizations nor quantification of the error were done. However, the droplets are clearly extremely small around the microns or even lower; the closer we are to flash evaporation, the smallest are the drops. The velocity is also very

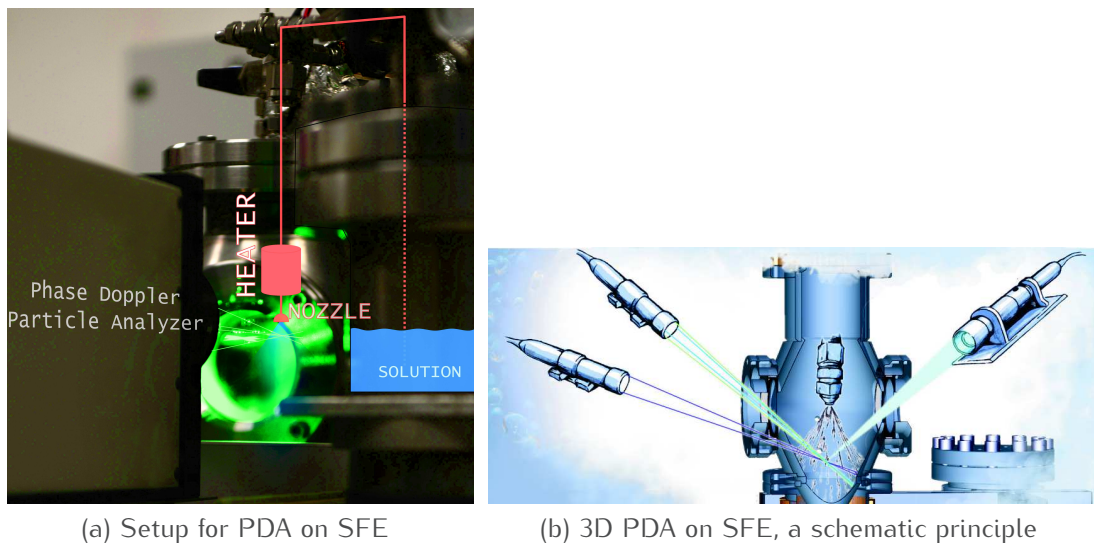


Figure 4.7 – PDA in situ measurements for SFE.

high with an order of magnitude of 2 (100 m/s): it is one order above the rare velocities reported in flash-evaporation of spray by Gebauer et al. (2015) and Miyatake et al. (1981). Those preliminary data confirm that the SFE process involves high energy and fast crystallisation. It can be estimated that after 1 cm from the nozzle the spray is no more visible, which could imply that after only $0.1 \mu\text{s}$ the evaporation is complete and the crystallisation performed.

More reliable results were acquired thanks to the work of Mr Lasserre to deliver us an operational PDA apparatus quickly after the purchase. The beams were focused a few millimetre after the nozzle orifice and as close as possible to the nozzle axis. The PDA were stabilized and operated in coincidence mode (the velocity measured by Laser velocimetry is coupled to the measurement of the diameter by Phase Doppler interferometry, resulting in the exact measure of both for each object in the measurement volume) with a sequence of 10 measurements each with 20k objects measured ; the receiving optics adjusted for the highest rate of coincidence and optimized with the Laser power. About the SFE, the temperature is stabilized for 15 min before each sequence. Each batch from the set of ten is compared to each other: no changes in the PSD has been noticed in a set of measurement for a given temperature so all the 200k objects measured per temperature are concatenated to render the Figure 4.9.

While the temperature is raised the droplet size clearly decreases close to the detection limit around one micron. Moreover the polydispersity exhibited for each PSD is reduced while increasing the temperature; multi peak fitting reveals three modes centred at 2.1, 2.8 and $3.8 \mu\text{m}$ at all temperatures. The

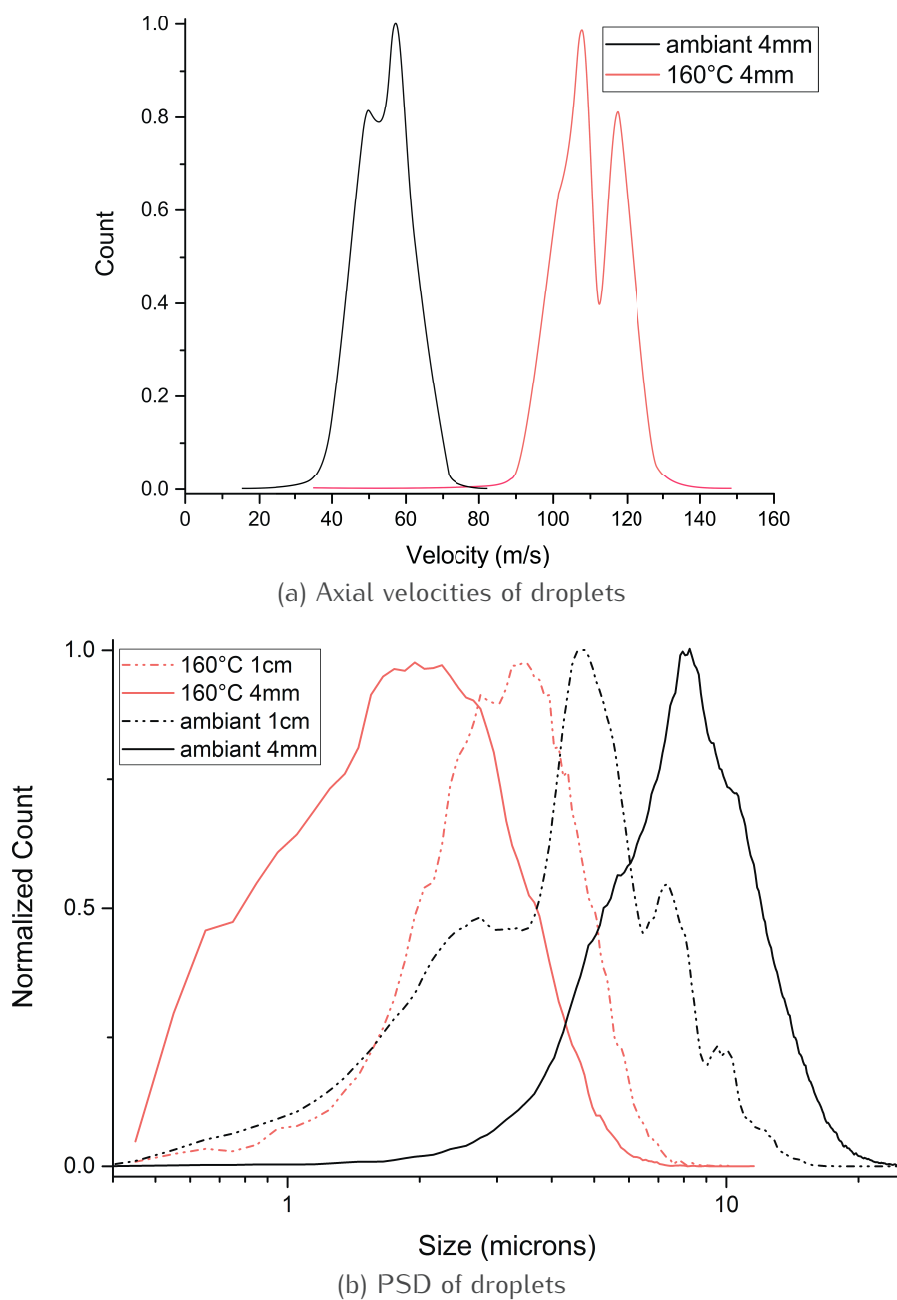


Figure 4.8 – Preliminary measurements from a demonstration apparatus inside the SFE under vacuum while spraying acetone. Acquisitions were performed at two different axial distances from the nozzle orifice: at around 4 mm or quite far at around 1 cm

center of gravity doesn't change with temperature but only the area. Therefore at such temperatures the SFE is under a transition state toward flash evaporation which seems to be the dominant phenomenon at temperatures around 160 °C. To complete this study, the influence of the nozzle type should be study to evidence a potential change in the centre of gravity of the modes.

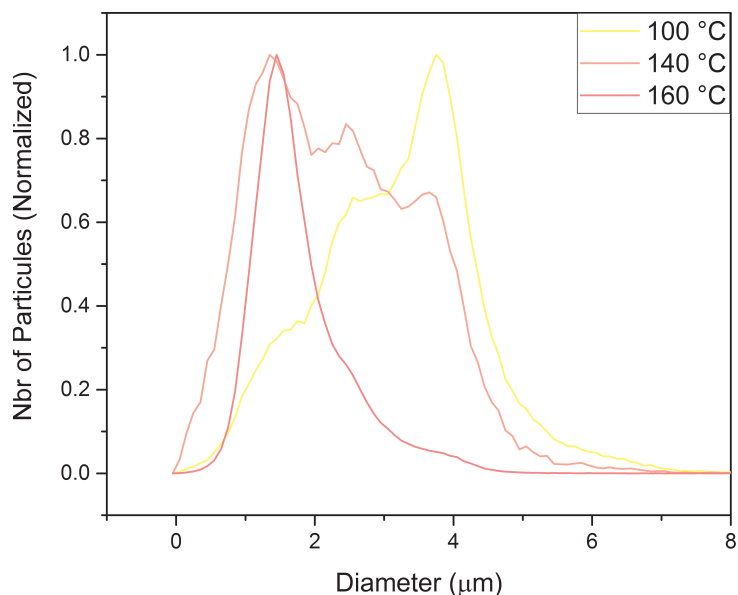


Figure 4.9 – Particle Size Distribution of droplets of acetone sprayed at 100, 140 and 160 °C.

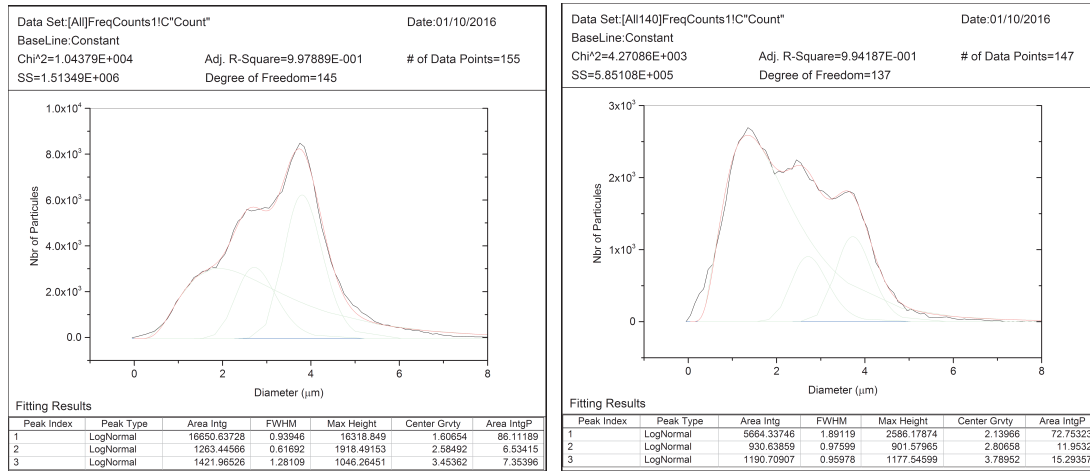
4.2 CL-20:HMX 2:1 Cocrystal as a Tool for Understanding Crystallisation by SFE

4.2.1 Cocrystallisation

A cocrystal consists in the combination of two or more electrically neutral molecules within a single crystal lattice in a stoichiometric ratio. The exact definition is still under debate (Sun 2013) but hydrates and solvates are usually excluded. The constitutive compounds are often called co-formers. While cocrystals are known to potentially combine the drug effect of two Active Pharmaceutical Ingredient (API)s (Vishweshwar et al. 2006), it is interesting to notice that historically the pharmaceutical industry first avoided cocrystal, the racemic ones (Toda et al. 1997).

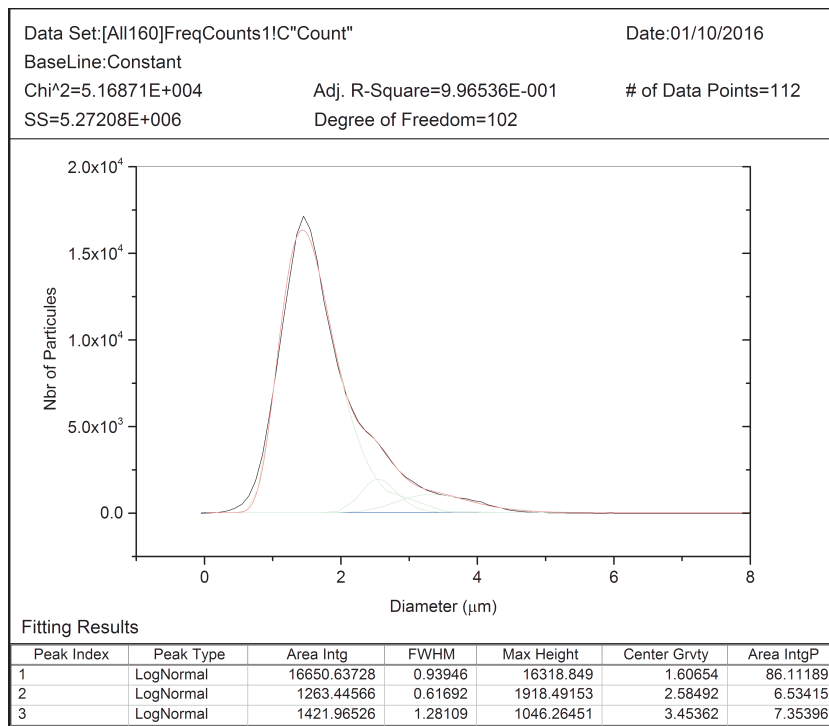
The formation of an existing cocrystal and the crystals of the co-formers relies on their solubility. A Phase Solubility Diagram (PhSD) shown in Figure 4.11

4.2. CL-20:HMX 2:1 COCRYSTAL AS A TOOL FOR UNDERSTANDING CRYSTALLISATION BY SFE



(a) 100 °C

(b) 140 °C



(c) 160 °C

Figure 4.10 – Peak fitting of the PSD of droplets of acetone sprayed at 100, 140 and 160°C.

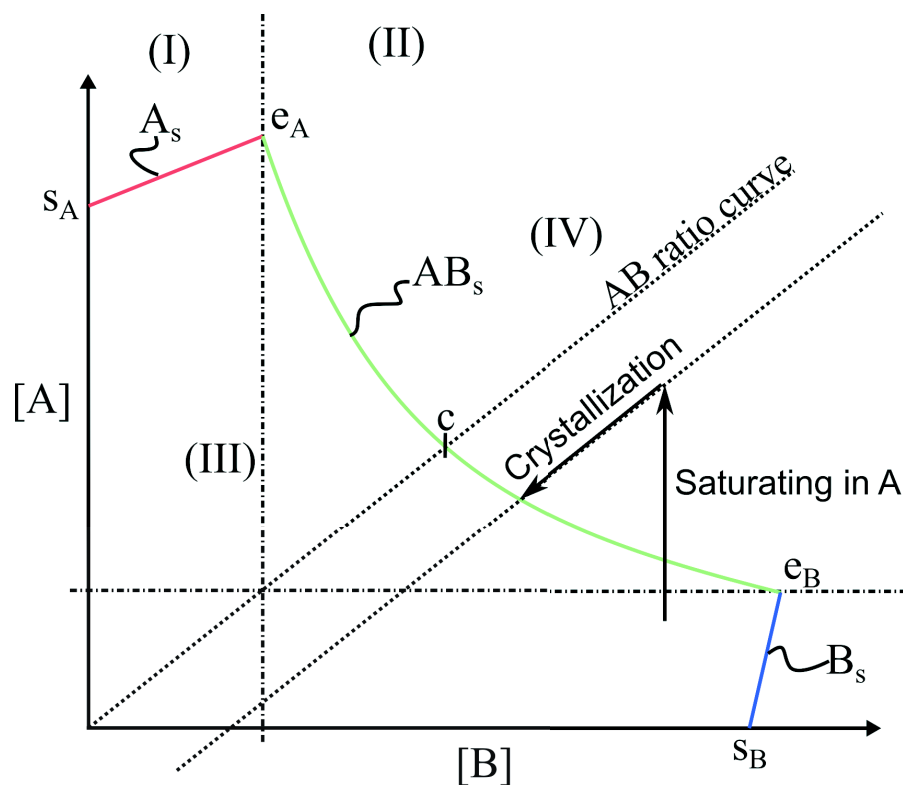


Figure 4.11 – Phase Solubility Diagram (PSD) of a 1:1 AB cocrystal from co-formers A and B; in red the solubility curve of the A crystal, in blue the one of B, and in green the cocrystal. Arrows illustrate a possible crystallisation by addition of B to the solution followed by the cocrystallisation.

depicts the co-former concentrations in a solvent at equilibrium at a given temperature with the different domain for each crystals (Nehm et al. 2006). The domain I is saturated in A and under saturated with respect of the cocrystal AB: only polymorphs from A can be crystallised. In the domain II both A_s and AB_s crystallises; the domain IV is situated above the solubility curve of the cocrystal and thus allows the crystallisation of the AB_s alone. In the domain III, the solution is under saturated for all species and no crystallisation can occur.

Unlike the PhSD, the triangular phase diagram (TPD) in Figure 4.12 shows the total composition of the system. Chiarella et al. (2007) explained why the formation of cocrystals could not occur while having the appropriate stoichiometry and underlined the need of covering a wide range of ratio when screening for cocrystals (Chadwick et al. 2009).

Beside those thermodynamic properties at equilibrium, kinetics prevail especially when crystallising from multicomponent systems. Ostwald (1897) speculated that the critical cluster to nucleate from a supercooled liquid may not be

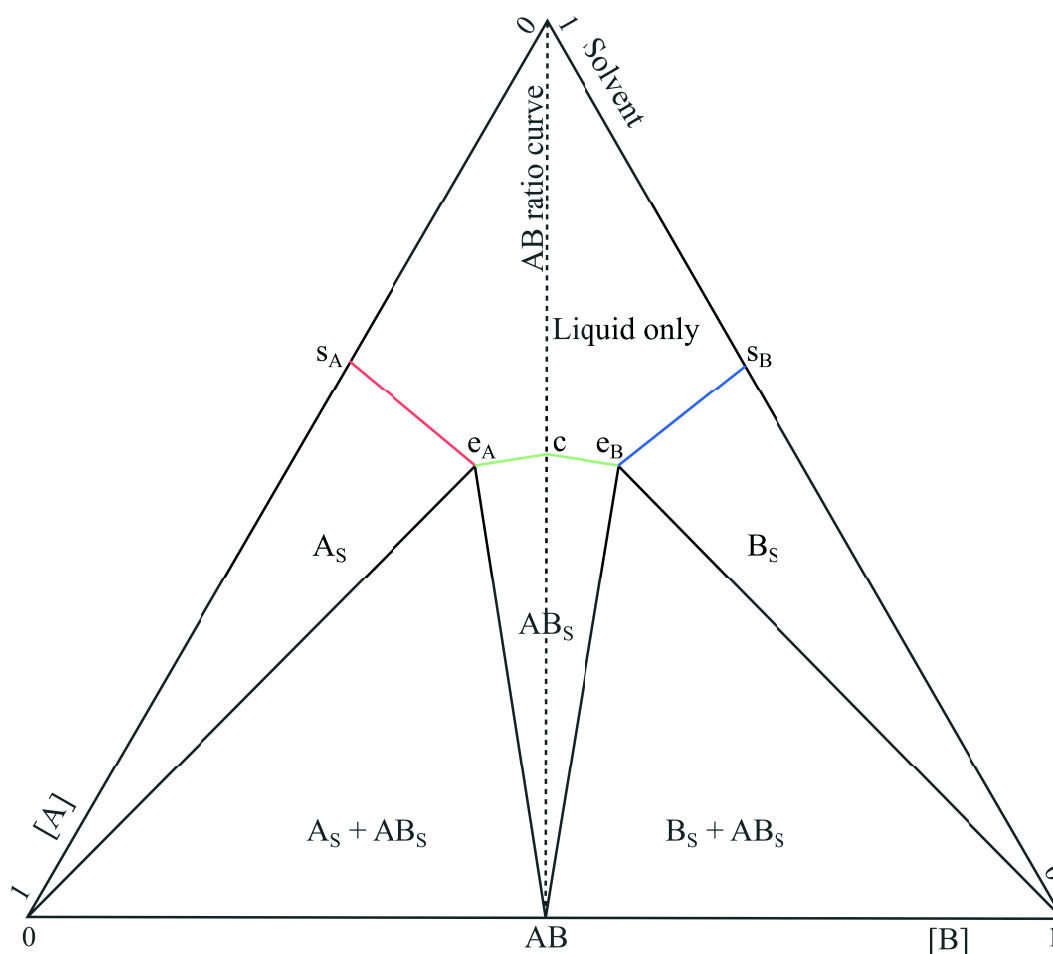


Figure 4.12 – Ternary Diagram of a 1:1 AB cocrystal from co formers A and B; coloured curves are the solubility curves from Figure 4.11.

the most stable polymorph but the polymorph closest in energy to the liquid phase. Since 1897, this behaviour has been observed a number of times (ten Wolde et al. 1999).

4.2.2 CL-20:HMX 2:1 Cocrystallisation from SFE

The SFE has already proved to be a suitable method to cocrystallise from a solution at the dried state (Spitzer et al. 2014). However to ensure a complete comprehension of the cocrystallisation by SFE, PhSD at several temperatures should be established for each compound such as the caffeine and acid glutaric from Yu et al. (2010). Unfortunately no PhSD nor ternary diagram exists for the CL-20:HMX 2:1 cocrystal.

In order to confirm the existence of metastable droplets in a state where no nucleation nor flash-evaporation occurred, an experiment with the co-formers sprayed separately was designed: the first dual-nozzle system was build for those experiments. Instead of an angle of 70°, the nozzles were oriented at 45° as illustrated in Figure 4.13.

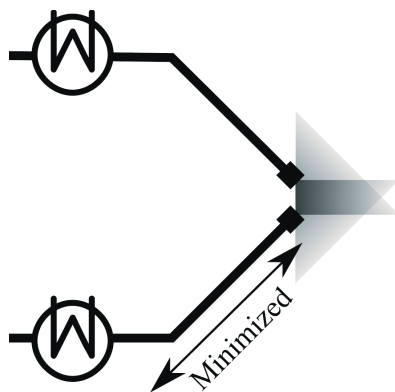


Figure 4.13 – First dual nozzle system with an orientation at 45°.

The solutions of CL-20 and HMX were prepared in the stoichiometric ratio 2:1 of the cocrystal, using acetone (CHROMASOLV ®, for HPLC, ≥ 99.9% Sigma Aldrich). The Figure 4.14 shows mean PSD of the samples obtained through that technique; the method used is the AFM on pellets explained in the Section 3.1.2. Therefore, even if the mean size obtained here of 73 nm can not be interpreted as an absolute size, it can be compared to other samples processed by this technique: 73 nm is among the smallest mean sizes counted for n-RDX –more specifically the RDX processed with PVP– meaning that an absolute size under 300 nm can be expected.

X-ray Diffraction was performed on samples processed from that dual nozzle setup. The XRD pattern in Figure 4.15 exhibits two crystalline structures: the main crystals present is β -CL-20 but the cocrystal is confirmed to have crystallised from the overlapped sprays. β -CL-20 is the least stable polymorph of CL-20; the crystallisation of β -CL-20 from SFE implies a kinetically controlled crystallisation and an high energy (Ostwald rule previously mentioned). The cocrystal being the minor product could be explained from a thermodynamic point of view from solubilities, but the solubility of CL-20 in acetone is much higher (100 wt%) than HMX (2.8 wt%). The explanation lies from a more practical issue.

The flow rate is not monitored in real time, but an estimation of the mean flow rate for each nozzle is calculated from the volumes left and the experiment time. It has been found that for all experiments with the dual nozzle at 45°,

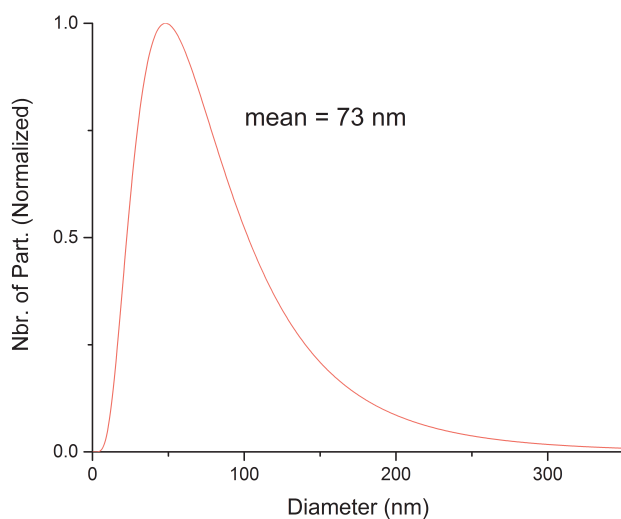


Figure 4.14 – Mean Particle Size Distribution of the cocrystal CL-20:HMX 2:1 samples processed by SFE (first batch) and counted from pellets analysed by AFM.

the nozzles have a very strong attendance to clog. Due to the angle and the spray broadening under vacuum, nozzles spray on each other; each nozzle forms a solid deposit on the opposite one and, after a while, one nozzle is clogging and blocking entirely the other one. Another system is build afterwards with an angle around 70° as previously introduced in Section 4.1.1; also to correlate the percentage of each crystal to kinetic or thermodynamic phenomena, the flow rate has to remain constant. Coriolis mass flow meters for high pressure were purchased and installed on the SFE process. To control in real time the flow rate of one inlet based on the variation of the other inlet, a master/slave system was developed: one flow meter read and transmit the flow rate of one nozzle to the second flow meter equipped with a valve and an internal PID controller. A variable resistor allows to set a ratio of flow rate between the inlets, thus allowing to have the compounds in a non stoichiometric ratio –with respect to the cocrystal– in solution but sprayed at the stoichiometric ratio. Those flow meters are currently at the testing stage before performing scientific studies.

An experiment was performed lately by spraying a solution of CL-20 in ethyl acetate and a solution of HMX in acetone at the constant stoichiometric ratio 2:1 by monitoring and controlling both mass flow rate. As it can be seen in Figure 4.16, even introduced with the right proportion with a controlled flow rate, the main product is again β -CL-20 with the cocrystal as the minor one. The amorphous content has to be calculated from the pattern; several methods

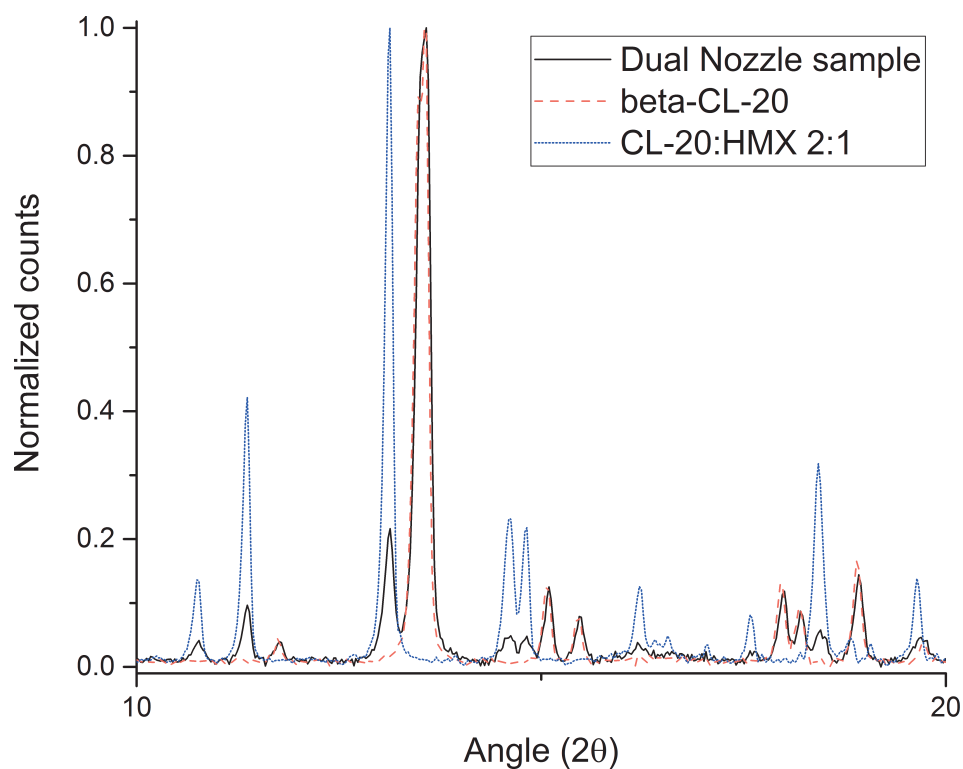


Figure 4.15 – XRD of a sample processed from dual nozzle system compared to CL-20:HMX and to β -CL-20 both from SFE via a single nozzle.

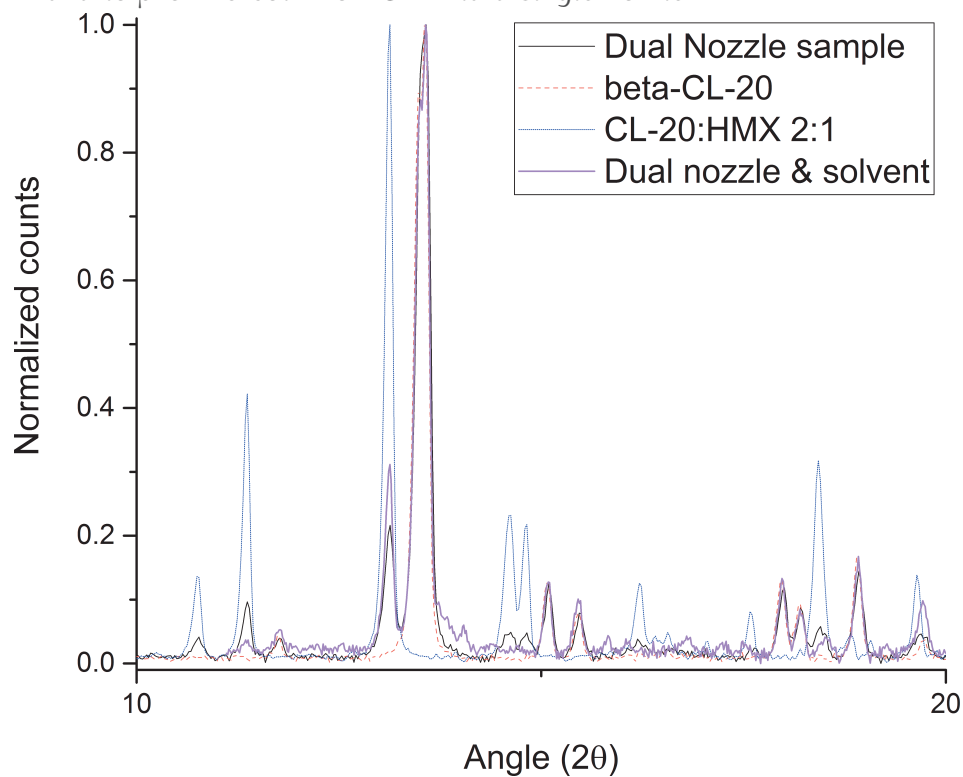


Figure 4.16 – XRD of a sample processed from a solution of CL-20 in ethyl acetate and a solution of HMX in acetone sprayed at the constant stoichiometric ratio 2:1 by monitoring and controlling mass flow rate; the pattern is compared to the sample from the Figure 4.15, CL-20:HMX and to β -CL-20 both from SFE via a single nozzle.

exists requiring calibration suite or internal/external standards. All of them would require to analyse the sample(s) with silicon or quartz zero-background sample holder: less than 20 mg are used and so the current sample holder has a strong amorphous contribution. If the HMX is found to be amorphous by chemical analysis such as IR or Raman, the system in the overlapping area is a solubility zone where the cocrystal can not be obtained pure. If no HMX is found, the crystallisation of CL-20 and HMX occurs already before the overlap and almost all crystallised HMX is lost due to a flaw in the process itself (cyclone cut-off, crust on the nozzle, affinity with walls etc.). The overlap should also be monitored to quantify the percentage of droplet interpenetration.

4.3 Summary of the Chapter

The crystallisation is a multi-step process not yet fully understood; the critical initial stage –the nucleation– is still under investigation by the crystallisation community with recent advances completing further the Classical Nucleation Theory (CNT). Nevertheless, the supersaturation still plays a major role on the rate and trigger of nucleation. Without a determination of the droplets size and evaporation rate, this present study focused on solvent exchange.

The n-hexane is used as anti-solvent to raise the supersaturation. The system acetone/n-hexane forms an azeotrope with a lower boiling point which increases the superheating. However, while using different ratios at the same boiling point, increasing amounts of n-hexane reduced the final mean particle size: from around 800 nm with pure acetone to a plateau around 550 nm. When spraying the n-hexane from a second nozzle, particle size has been improved with a mean particle size of 580 nm.

To confirm that the droplets interpenetrate each other and hexane is not already gaseous thus drying acetone droplets, the cocrystal CL-20:HMX 2:1 is studied. Two solutions of acetone are prepared and sprayed separately; one with CL-20 and another with HMX. The cocrystallisation occurs confirming the overlap. Another similar experiment where CL-20 is dissolved into ethyl acetate supports that interpretation with again a cocrystallisation.

Phase Doppler Analysis (PDA) has been used for the first time for *in situ* measurement of a superheated fluid sprayed under vacuum. The SFE technology will be studied and on-line monitored; the data acquired from both PDA and Small-Angle X-ray Scattering (SAXS) will be computed to provide evaporation rate and crystallisation kinetics, introducing a breakthrough for the SFE technology.

Size reduction can also be achieved by controlling the nucleation and growth steps by adding agents which will change the supersaturation conditions locally

or will interact with the solute favourably or not. PolyVinylPyrrolidone (PVP) and PolyEthylene Glycol (PEG) are two very common polymers identified as food additives – E1201 and E1521 respectively – but also as crystallisation agents for many organic compounds. The new chapter explores the chemical approach for controlling crystallisation by SFE, with a focus on those two polymers, resulting in a new wide range of RDX size available.

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Chapter 5

Tunable continuous production of RDX from microns to nanoscale using polymeric additives

The specificity of the SFE process arises from the intricacy of many physicochemical phenomena that occur with the spray of superheated and supersaturated solutions. The whole system needs to be resolved in space and time as illustrated in Figure 5.1. Crystallisation itself happens in successive steps, namely primary nucleation, crystal growth and secondary nucleation. The complexity of the flashing behaviour is increased by the lack of both theoretical and empirical bases on flashing droplets. In order to dissociate those dynamic events, one crystallisation step over the others can be promoted by the use of additives; nucleation and growth can be inhibited or favoured selectively by polymers. PolyVinylPyrrolidone (PVP) and PolyEthylene Glycol (PEG) are two very common polymers identified as food additives – E1201 and E1521 respectively – but also as crystallisation tools. Kim et al. (2013, 2011) and Lee et al. (2014) clearly identified the PVP as a both growth and nucleation inhibitor of RDX in acetone, although only an alteration of the particles morphology was measured without any reduction of the size under electrospray. McPherson and Cudney (McPherson et al. 2006) proved the great effectiveness of PEG for triggering proteins precipitation, notably by steric exclusion as shown by Bhat and Timasheff (Bhat et al. 1992). By the addition of PVP, a delay of the crystallisation at higher supersaturation degree is expected, thus triggering an homogeneous nucleation with a higher density of nuclei. However in those conditions, aggregation or coalescence of nuclei may occur leading respectively to bigger polycrystalline particles or to bigger single crystals. The PEG would increase the supersaturation too, but with a different mechanism than PVP; PVP trends to adsorb on crystal surfaces thus inhibiting the nucleation and growth,

whereas PEG acts as nucleation promoter due to its steric effect.

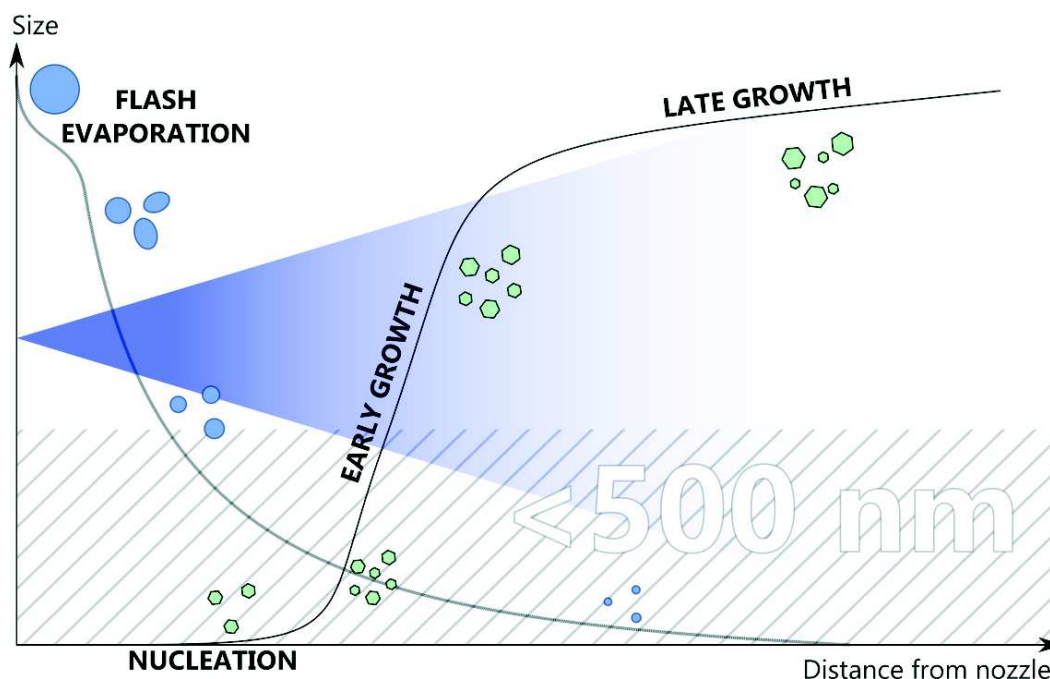


Figure 5.1 – Evaporation and crystallisation phenomena throughout the SFE process. The 500 nm limit displayed is roughly the detection limit for Phase Doppler Particle Analyzers, which allows in situ size and velocity measurements on both liquid and solid particles.

5.1 Material & Methods

As mentioned in Chapter 1, the RDX is provided by Eurenco, labelled as M5 and used as is, without further purification; the mean size is $6.8\ \mu\text{m}$. Standard PVP with an average molar weight around $40.000\ \text{mol/g}$ and PEG $400\ \text{mol/g}$ (liquid) are purchased from Sigma Aldrich.

RDX and the polymers when needed are dissolved in acetone by stirring one minute and then an ultrasonic bath of ten seconds achieved the dissolution. The concentration of RDX is kept constant at 2 wt% in acetone and weighted percentages of polymer are per gram of RDX.

The operating conditions of the SFE are 40 bar of inlet pressure and $160\ ^\circ\text{C}$ at a hollow cone nozzle with an orifice diameter of $60\ \mu\text{m}$.

5.2 Results & Discussion

5.2.1 Quantification by NMR Spectroscopy

The quantification of the amount of polymer in the final RDX products is the preliminary step before further characterizations and interpretation. NRM-H were conducted in cooperation with our colleagues from the ISL specialized in analytical chemistry. The robustness and accuracy of the build-in quantification integrated in the software is first tested. A well-known lot of RDX is chosen as a standard sample, then a mass gradation is performed in two different solvents, acetonitrile and DMSO at 35 °C to ensure complete dissolution. The linear regressions shown in Figure 5.2 are acceptable. DMSO is also the most suitable solvent.

Subsequently, RDX samples processed with polymer are analysed by NRM-H and the RDX peak integrated. The value for 100 wt% of RDX is taken from a pure SFE-processed RDX sample. The final results are shown in Table 5.1. All values are close to the initial amount of RDX. However, two trends can be clearly highlighted when calculating the difference between theoretical and experimental amounts. For the samples processed with PVP, when the amount of RDX increases, the final product contains more PVP than initially; on the contrary less PEG is found when increasing the RDX content. Due to the NMR accuracy and the percentages involved, those trends should be confirmed, at least some values, by using another analytical method such as HPLC before any interpretation. Nevertheless, final and initial ratio of RDX/polymer are similar.

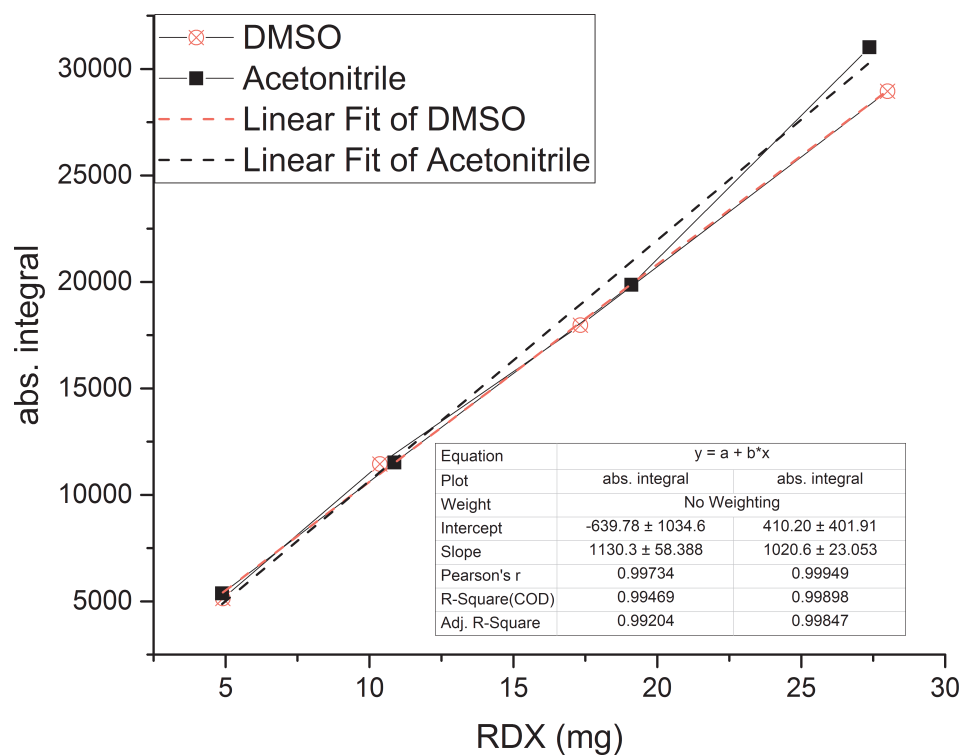
theoretical wt% of RDX	90.91	95.24	99.01	99.50
mean calculated value from NMR	90.9	94.5	98.0	96.8
difference	0.0	-0.7	-1.0	-2.7

(a) RDX processed with PVP.

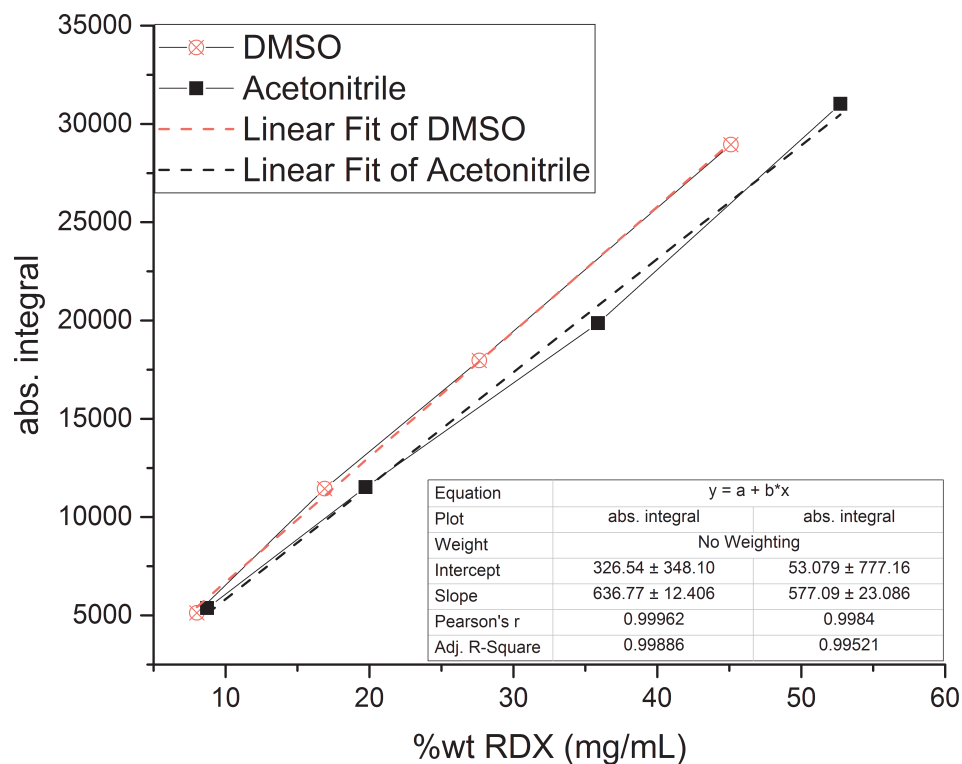
theoretical wt% of RDX	90.91	99.01	99.90
mean calculated value from NMR	88.6	98.5	99.9
difference	-2.3	-0.5	0.0

(b) RDX processed with PEG.

Table 5.1 – Mass percentage of RDX in the final products compared to the initial loading.



(a) Absolute integral in arbitray units plotted against the RDX mass.



(b) Absolute integral in arbitray units plotted against the RDX concentration.

Figure 5.2 – Test of the reliability of quantification by NMR.

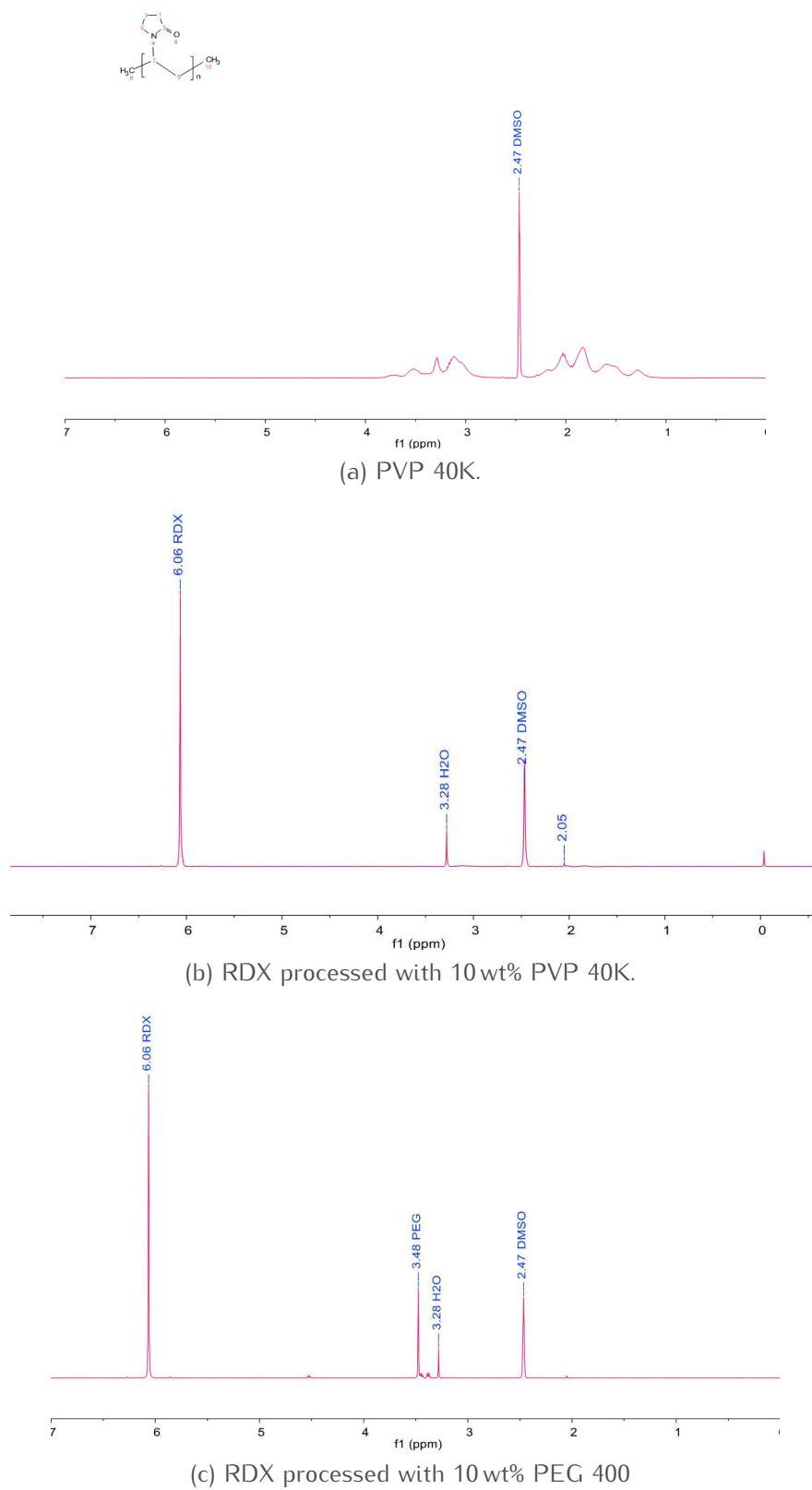


Figure 5.3 – NMR-H spectra of various representative samples

5.2.2 RDX processed with PEG 400

5.2.2.1 Particle Size and Morphology

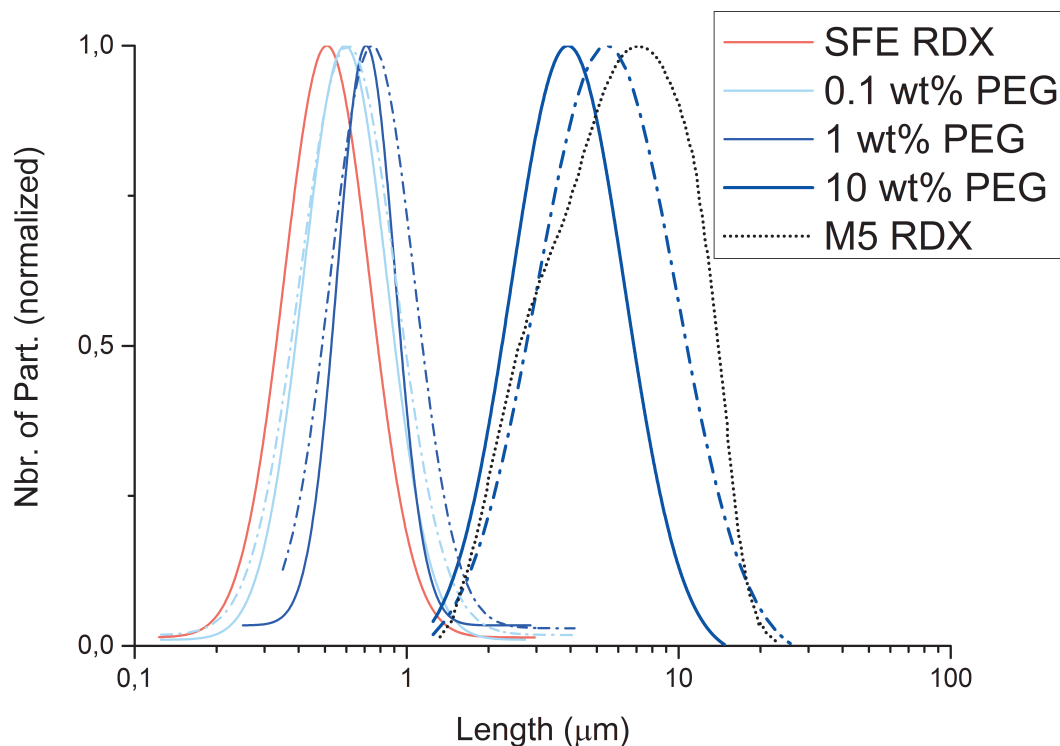


Figure 5.4 – Sizes – using a logarithmic scale – of samples processed with PEG measured from SEM micrographs; solid lines represent the smallest lengths and the dotted lines the largest. Pure RDX processed by SFE and raw M5 RDX added here for comparison.

Originally pure RDX processed by SFE can be obtained with a mean size in the range of 400 nm–900 nm depending on the conditions; with the parameters chosen for that study, the mean size would be around 500 nm (Doctoral Thesis Risse 2012). Starting with only 0.1 wt% of PEG per gram of RDX, the mean particle size increases to 670(0.356) nm. Then the mean size still increases to 750(0.244) nm with 1 wt% and reaches 4.9(0.482) μm with 10 wt%. The elongation of the particles while increasing PEG content can be clearly seen from Figure 5.4 but also when defining a roundness factor or aspect ratio by dividing the smallest length by the largest one. That width-to-length ratio is 0.94 at 0.11 wt%, 0.89 at 1 wt% and only 0.64 at 10 wt%, indicating a preferential growth in one direction.

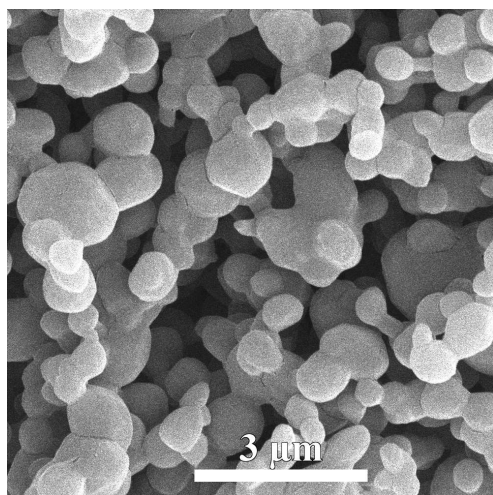
Due to a high solubility in acetone, PEG rapidly increases supersaturation in droplets at the very beginning of the atomization and, considering its influence on particle size, the supersaturation is far from the optimal value where the

nucleation rate is maximal. Vekilov (2010) proposed an explanation of why, while the nucleation rate should be increasing exponentially with the degree of supersaturation, experiments at high supersaturations clearly show unpredictable rate of nucleation; according to the two-step mechanism, the crystalline nucleus appears inside metastable clusters of several hundred nanometres. Those clusters of dense liquid which are suspended in the solution can be favoured by the steric effect of PEG and the rapidly increasing saturation due to the flashing behaviour of droplets. Therefore, the induction time of nuclei is reduced and the nucleation rate low thus allowing the formation of bigger particles. Further characterizations involving Phase Doppler Anemometry has to be conducted to kinetically discriminate the role of PEG in the SFE process. As shown in Figure 5.1, the crystallisation of RDX with PEG would allow the particle size to exceed 500 nm; kinetic growth from the apparatus detection limit to the final particle size could be established.

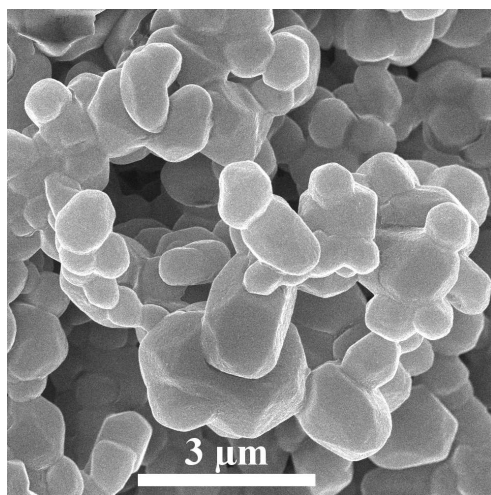
Although PEG is liquid at ambient temperature, no significant change of aspect between all the final nano powders of RDX processed either pure or with an additive can be noticed. The samples processed with 10 wt% of PEG are less electrostatic and slightly yellowish.

5.2.2.2 X-Ray Diffraction (XRD)

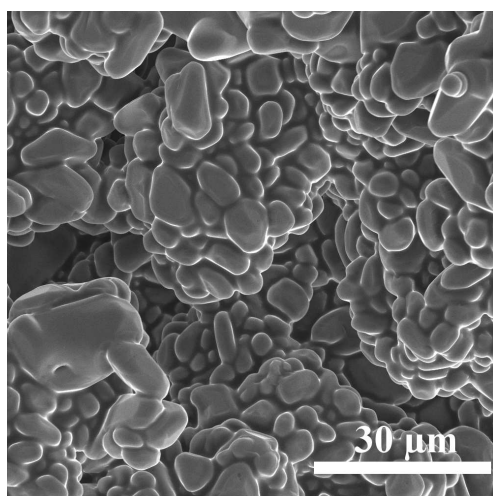
The XRD patterns in Figure 5.6 exhibit a slight different texture when micron-size RDX samples at 10 wt% of PEG are compared with others. From SEM pictures, morphology and PSD indicates a preferentially oriented growth ; the relative differences of intensity in XRD clearly shows that the face {311} is much more prominent whereas others like {111}, {002}, {102}, {020} and {021} are hindered. Those results are in contradiction with predicted and effective morphologies resulting for RDX growth in acetone; Shim and Koo (Shim et al. 2014) successfully predicted the crystal growth habit of RDX in acetone by the spiral growth model and Chen et al. (2015) went further using molecular dynamic simulations. They explained the increased growth rate of the polar faces {111}, {200}, {020} and {021} compared to the non-polar face {002} in polar solvents like acetone. From our experiment, the use of the chemical affinity of faces toward the solvent does not apply when processed by SFE with PEG ; the 311 face illustrated in Figure 5.7 exhibits both methylene and nitro group at the surface, and the non-polar {002} peak is also decreased as well as the polar faces while adding PEG, a relatively non polar molecule. A small templating effect involving a preferential organization of PEG at higher concentration could explain those differences.



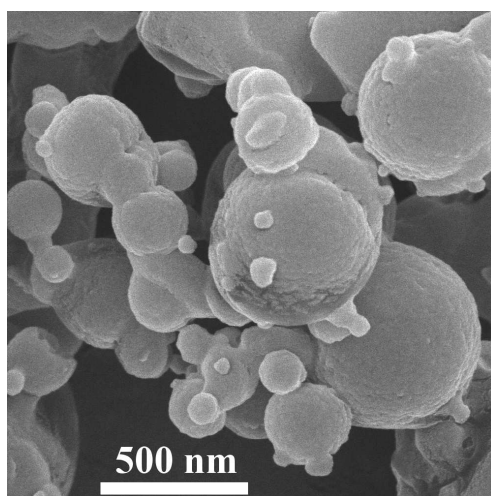
(a) SFE RDX



(b) RDX processed with 1 wt% PEG



(c) RDX processed with 10 wt% PEG



(d) RDX processed with 5 wt% PVP

Figure 5.5 – SEM micrographes of RDX samples processed by SFE in the same operating conditions.

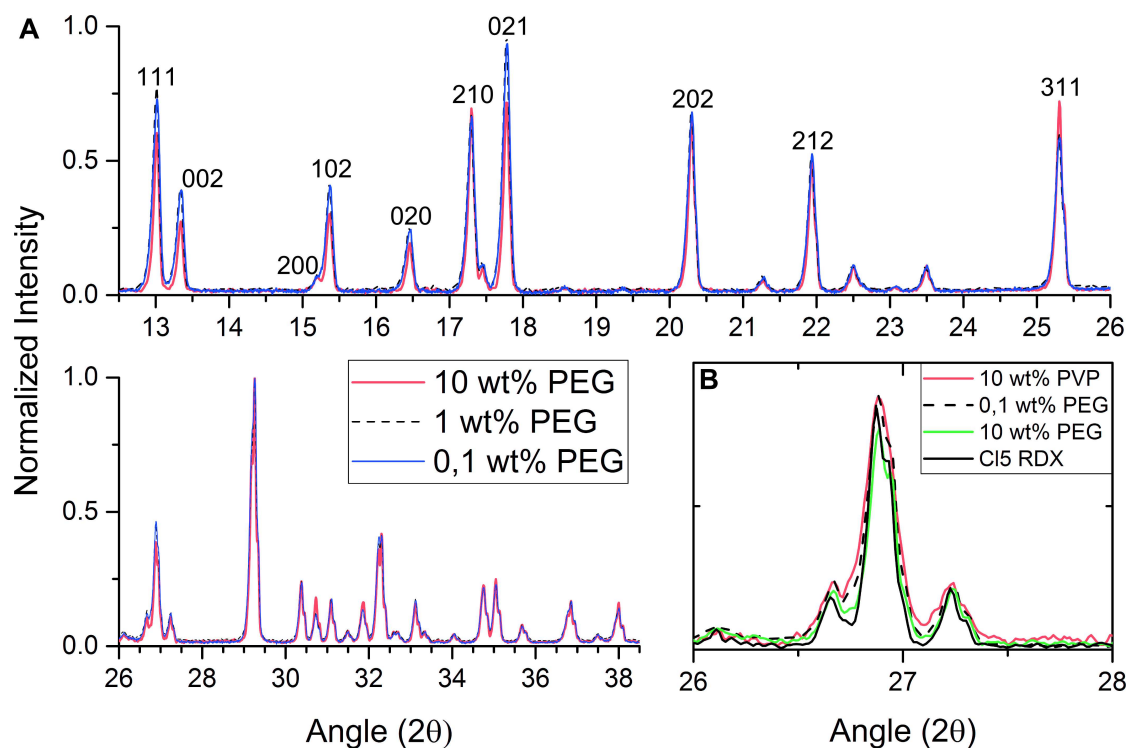


Figure 5.6 – (A) XRD patterns of RDX PEG-processed samples; only isolated peaks of major interest have been indexed for clarity. (B) inset of XRD patterns illustrating the broadening of peaks.

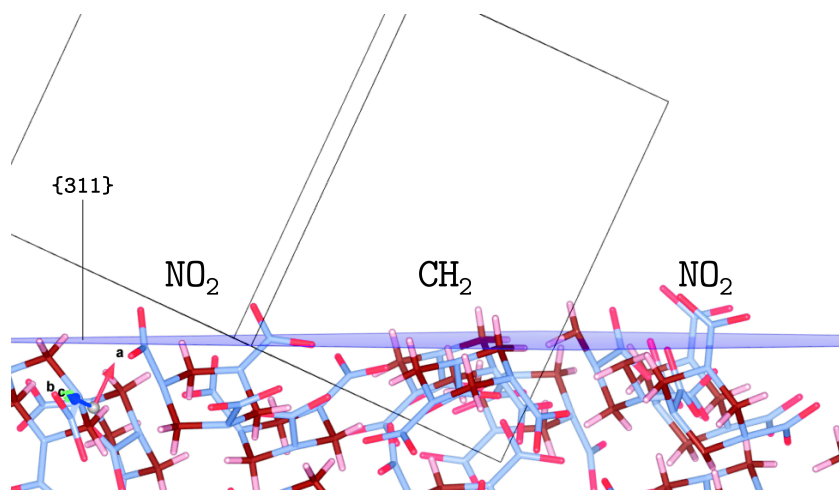


Figure 5.7 – View of the 311 plane (in violet, almost perpendicular to the plane of the drawing) and RDX molecules on the surface: both nitro and methylene group are located at the surface (on the background, the unit cell).

5.2.2.3 Thermal Analysis

The DSC results in Figure 5.8 show that the RDX processed by SFE is thermally less stable than the raw micron-size RDX, due to a higher ratio surface/volume for submicron size particles. Those results are in accordance with the work of Rosa et al. (2014) where micron size organic particles show also a similar slight melting depression. From 200 to 20 μm , they noticed a drop of 0.8 $^{\circ}$; from 7 μm to 500 nm, the melting point of pure RDX decreases of 1.2 $^{\circ}$. Although that ratio is decreasing while adding PEG, DSC curves in Figure 5.8 show that the content of PEG itself decreases the activation energies for melting and decomposition: the temperatures – merged in Table 5.2 – are all decreasing. The PEG 400 melts at 3 $^{\circ}\text{C}$ (peak minimum) and starts to decompose after 300 $^{\circ}\text{C}$ (data not shown). The broadening of peaks and decrease of melting temperature is a well-known trend for impure organic particles: the gain of entropy by the creation of a bi component melt drives the melting. This phenomenon appears also in PBX like formex-bonded explosives where BCHMX/Formex melts 5 $^{\circ}\text{C}$ lower (Yan et al. 2012).

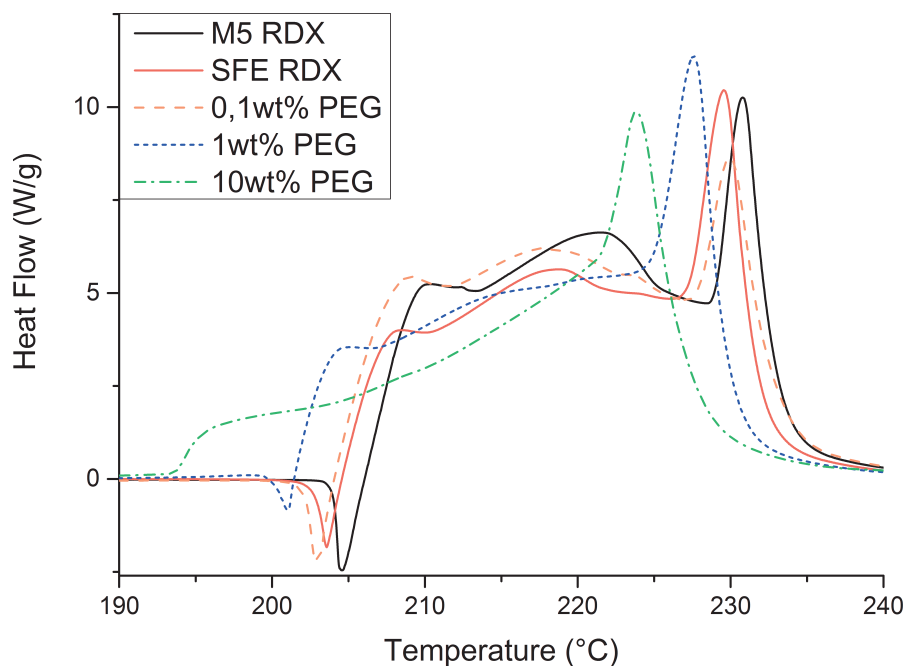


Figure 5.8 – DSC analysis of RDX samples processed with different wt% of PEG.

	$T_{e\ endo}$	$T_{e\ exo}$	$T_{p\ exo}$	$T_{c\ exo}$	$E\ (J/g)$
M5 RDX	204,0	206,1	230,8	233,6	4550
SFE RDX	202,8	204,6	229,6	232,1	4210
0.1%PEG	202,1	204,1	230,0	233,2	4710
1% PEG	200,0	201,4	227,6	230,0	4530
10% PEG	n/a	193,4	223,8	227,7	4010
0.5% PVP	202,2	204,3	229,3	231,7	4120
1% PVP	201,7	203,6	228,9	232,4	4190
5%PVP	197,1	199,1	226,0	229,4	2990
10% PVP	n/a	n/a	223,5	227,4	3090

Table 5.2 – Melting (endo) and decomposition (exo) temperatures in °C and decomposition energy in J/g for all samples (T_e extrapolated peak onset, T_p peak maximum temperature, T_c extrapolated peak offset). See Material & Methods section for more details.

5.2.2.4 Infrared (IR) Spectroscopy

In Figure 5.9, the mid-infrared spectra both 0.1 wt% and 10 wt% samples are compared to the raw PEG 400 used, and to pure RDX. The three main specific vibrations of PEG at 1000 cm^{-1} – 1200 cm^{-1} , at 2800 cm^{-1} – 3000 cm^{-1} and at 3200 cm^{-1} – 3600 cm^{-1} are broad absorption bands which can be clearly distinguished from RDX spectra; the 10 wt% sample exhibit those bands, but samples with lower amount such as the 0.1 wt% one are almost identical to the RDX one. The RDX characteristic bands at 3065 and 3075 cm^{-1} correspond to C–H stretching aromatic vibrations while 1590 cm^{-1} , 1570 cm^{-1} and 1270 cm^{-1} are assigned to stretching of NO_2 . A slight shift of 2 cm^{-1} to lower wavenumber of all bands from 500 cm^{-1} to 1650 cm^{-1} can be noticed only for the sample with the higher amount of PEG; since that region regroups both nitroamines and ring vibrations it seems more appropriate to consider that shift as negligible or at least not due to a specific interaction between the polymer and RDX.

5.2.3 RDX processed with PVP 40K

5.2.3.1 Particle Size and Morphology

The processing of RDX with PVP 40K dramatically changes the particles size and morphology as it can be clearly seen when comparing side by side the Figures 5.5a and 5.5d. The PSD of samples processed with PVP in Figure 5.10

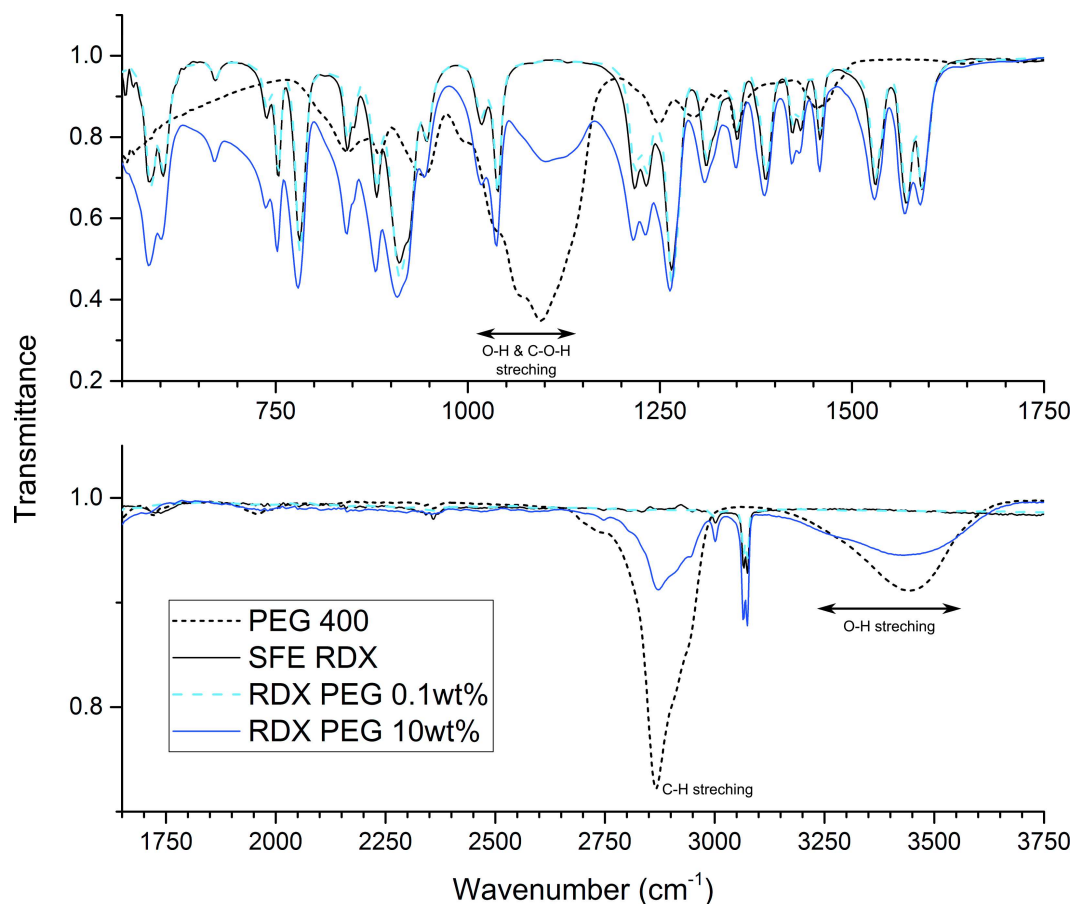


Figure 5.9 – FTIR spectra of two relevant RDX samples processed with PEG, compared to raw PEG 400 and pure RDX processed by SFE. (Socrates et al. 2001)

show a stabilized mean size around 160 nm with at least 5 wt% of PVP. At 1 wt%, the mean particle size is slightly higher at 180 nm and with a little more scattering: the multiplicative standard deviation increases from 0.843 for 5 wt% to 0.926 can be visualized from the dotted cumulative count curve in Figure 5.10.

It is very interesting to notice that only 0.05 wt% of PVP decreases the size by 34 % , from around 500 nm for pure RDX to 320 nm, and improves the spheric shape in a significant way. No preferential growth has been noticed and XRD (not shown here) confirms by identical intensity ratios within the micron-size raw RDX.

As previously mentioned Kim et al. studied the effect of additives on RDX crystallisation by electrospray and drowning-out and pointed out the role of PVP as nucleation inhibitor and growth inhibitor in acetone. The growth inhibition by PVP was only recently evidenced in their experiments of drowning-out where

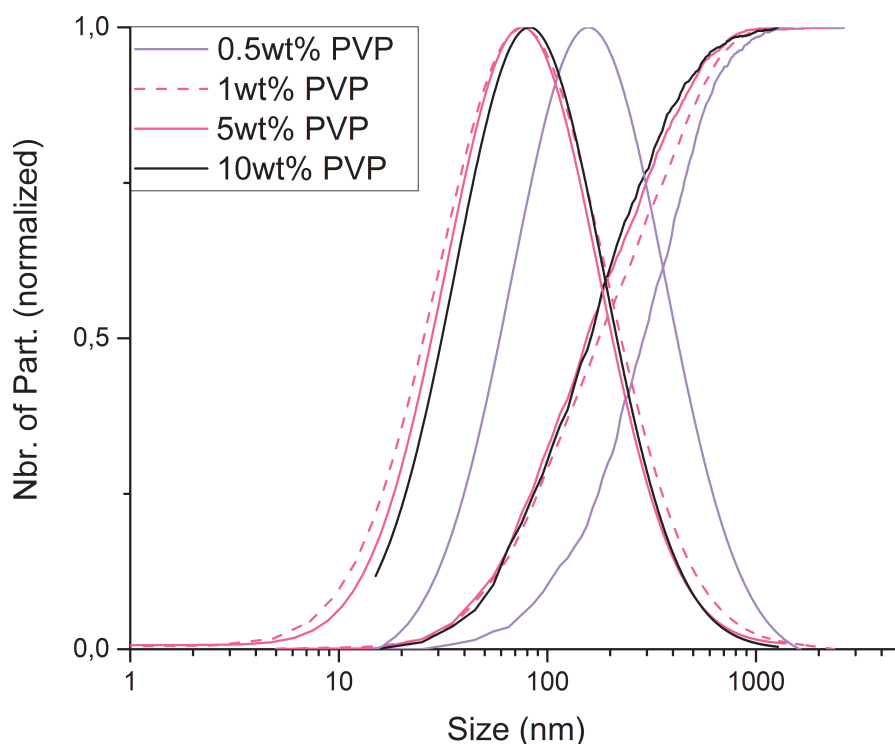


Figure 5.10 – Particle size distribution and cumulative counts – using a logarithmic scale – of samples processed with PVP measured from SEM micrographs.

RDX/acetone is sprayed into water, but not in the case of the electrospray; the difference can lie in longer times of flight in air and life in water of droplets in drowning-out and thus implies a more significant impact of the PVP on crystal growth. In contrast, the SFE process has a much higher mean evaporation rate and a two-step evaporation mechanism. Prior to the flash, the PVP inhibits the crystallisation of RDX until the flash of the droplet or delay the nucleation just before the flash. Then the sudden rise of saturation triggers the nucleation if not already, and implies a high crystal growth rate hindered again by the adsorption of PVP.

The size reaching a minimum at 1 wt% is certainly due to the mechanism of adsorption of the PVP. PVP possesses hydrophilic polar groups, that will interact preferentially on the crystal by chemical adsorption, thus slowing down crystal growth. The minima is then attained for a maximal surface coverage. Moreover, Patel et al. (2015) found out that the growth inhibition of PVP increased with the supersaturation of indomethacin in water. With the droplet fission, that trend is an additive phenomenon explaining the smaller size of RDX processed by SFE with PVP when compared to Kim's results.

In order to confirm the important role of the PVP, one small set of experiments

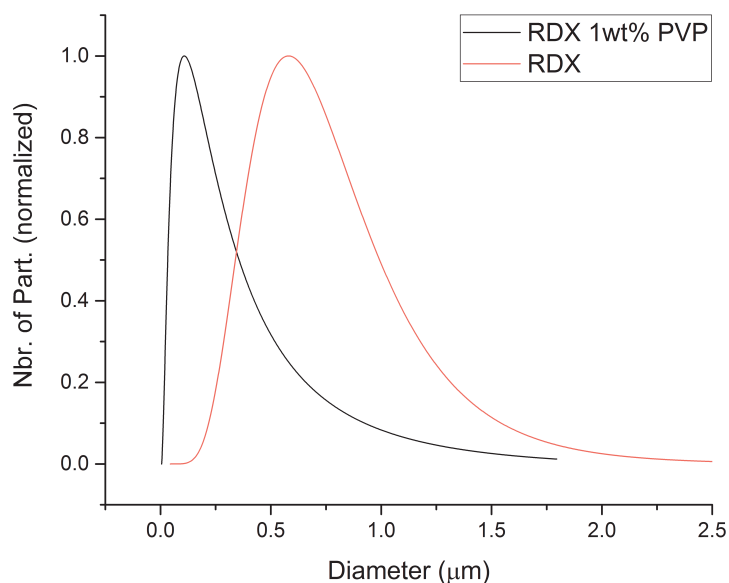


Figure 5.11 – Particle size distribution of RDX processed with a 80 μm nozzle at only 20 bar.

was conducted with a 80 μm nozzle at only 20 bar. From an industrial point of view, a higher mass flow at lowest pressure is a significant advantage; instead of a yield between 2 and 3 g/h for a 60 μm nozzle at 40 bar, RDX were recovered at a rate of 5–8g/h. However, as evidenced by Risse (Doctoral Thesis 2012), bigger particles are produced in those conditions; with only 1 wt% of PVP, the particle size decreases from 714(0.020) nm to 307(0.027) nm and again improves the sphericity. The increase of the particle size at higher flow rates can be counteracted by the addition of PVP, thus allowing both high production rate and small PSD.

5.2.3.2 Thermal Analysis

Figure 5.12 reveals that onset temperatures and temperatures at maximum decrease when adding PVP, following the same trend as the RDX samples processed with PEG. As we already discussed, a melting point depression for organic crystal can occur thanks to a decreasing particle size even above 500 nm and can be thermodynamically favoured: PVP-processed samples have a volumetric mean size well below 500 nm and the transition from a soluble solid formed by RDX and PVP to a liquid miscible solution is favourable. Moreover

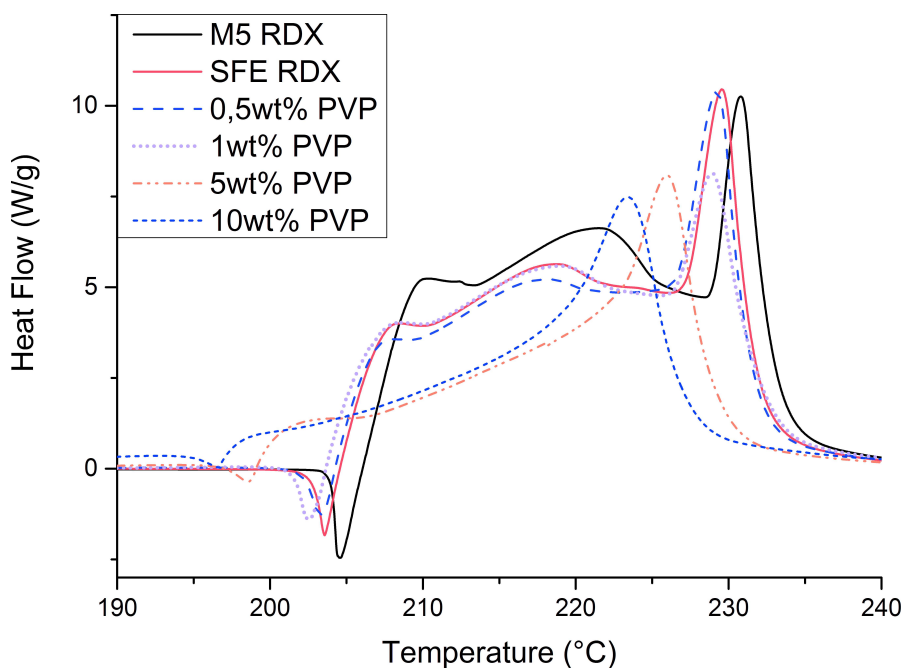


Figure 5.12 – DSC analysis of RDX samples processed with different wt% of PVP.

since PVP 40K has a glass transition temperature around 150–175 °C, solid PVP inclusion in the crystal lattice of RDX may also increase the internal energy. In case of crystal defects, micro-strain can be identified by XRD from peak broadening. Williamson Hall plotting has been found not to be a suitable model therefore a more reliable and calibrated method was required. details were given in Section 3.2.1.1; the Rietveld refinements then performed revealed an apparent volume weighted domain size always around 85 ± 10 nm and an average maximum strain around $10 \pm 5 \cdot 10^{-4}$ % for both pure and PVP processed samples. So it is very likely that only the effect of size and the presence of PVP are driving the melting point depression here.

5.2.3.3 IR Spectroscopy

In Figure 5.13, the mid-infrared spectrum of a 10 wt% sample is compared to the raw PVP 40K used, and to pure RDX. The two main specific vibrations of PVP around 1660 cm^{-1} and at 2850 cm^{-1} – 2950 cm^{-1} (CH stretching) are broad absorption bands which can be clearly distinguished from RDX spectra. The absorption at 3200 cm^{-1} – 3600 cm^{-1} is the vibration of water, the PVP being very hygroscopic. Only the 10 wt% samples exhibit a small broad peak around 1660 cm^{-1} from PVP.

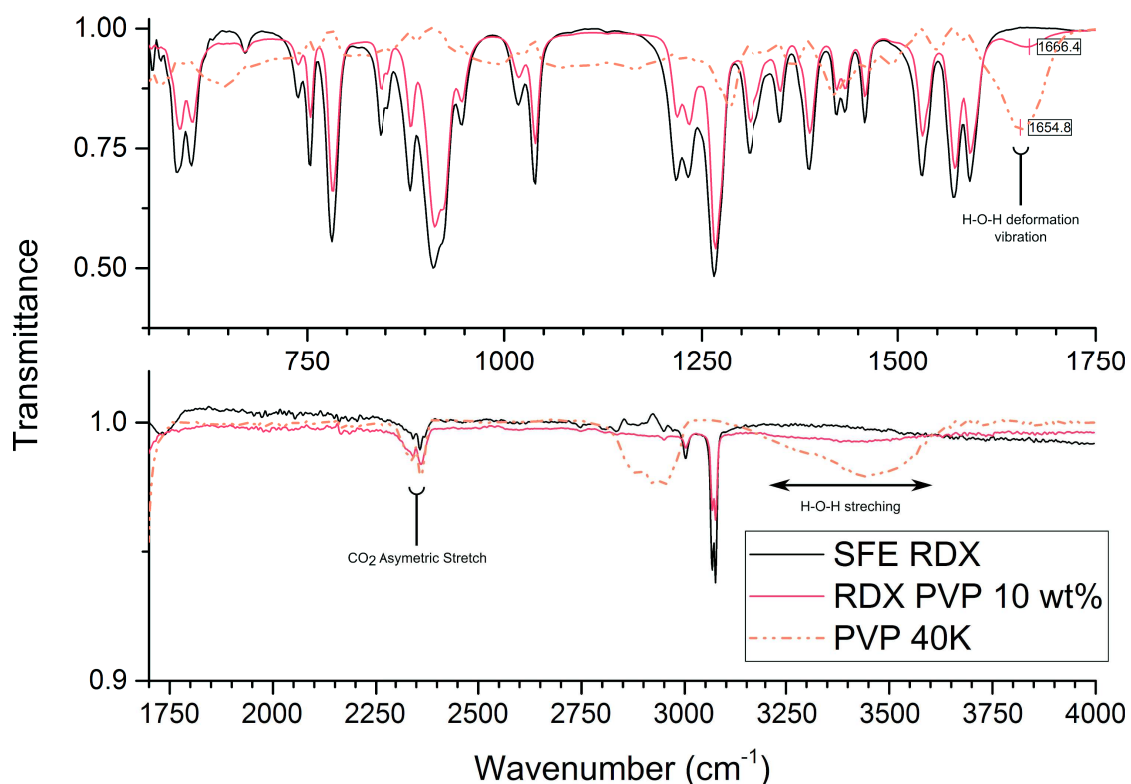


Figure 5.13 – FTIR spectra of the RDX samples processed with 10 wt% of PVP, compared to raw PVP 40K and pure RDX processed by SFE.

5.2.4 Sensitivity

In general, samples of nano-RDX have lower sensitivities with the addition of polymers as shown in the Figure 5.14. Due to the reliability issues raised by the submicrometer scale of the powders tested on macro or micron scale apparatus (Radacsi et al. 2013) and the inherent scattering of the results (Brown et al. 2015), the differences of one level higher or lower has to be moderated.

The threshold at the electrostatic discharge test is increased for all SFE processed RDX, and even further when adding at least 5 wt% of PVP (+300% then +700% compared to M5 RDX) or 10 wt% of PEG (+1160% compared to M5 RDX).

The addition of at least 1 wt% of PVP or PEG desensitizes the RDX toward friction, up to +57.5%. Taking into account the previously mentioned dispersions of sensitivity values, the slight decreased value for friction at 10 wt% for both polymers can be not significant enough, due to the inability of the apparatus to process more plasticized compositions or due to the lower thermal stability.

The micron size RDX with 10 wt% of PEG is twice insensitive at the impact

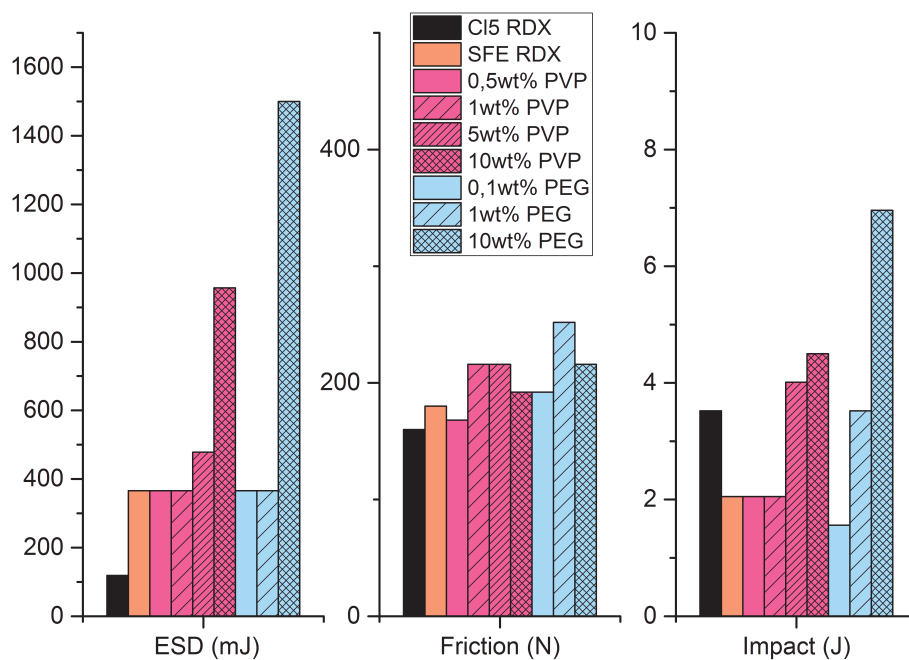


Figure 5.14 – Sensitivities of RDX processed with PVP and PEG compared with pure nano-RDX and the raw micron size RDX.

Sample	Impact test (J)	Friction (N)	ESD (mJ)
M5 RDX	3.52	160	119
SFE RDX	2.05	180	359
0.1 wt.%	1.56	192	366
1 wt.%	3.52	252	366
10 wt.%	6.96	216	1.5 J

Table 5.3 – Sensitivities of the RDX processed with PEG, compared with pure nano-RDX and the raw micron size RDX.

test than pure nano or micron size RDX; despite a morphology trending to be needle-like when adding PEG and so being more likely sensitive to impact as Chen et al. (2012) demonstrated, the sensitivity decreases due to the polymeric content and the size range.

With the exception of 10 wt% PVP samples, no loss of reactivity has been noticed during the sensitivity tests, the material has the same response as the pure nano and the raw micron size RDX. An explosion at the impact or discharge can be clearly heard with no residue left, and the friction produces an audible crackling with matter ejection; only the 10 wt% PVP samples exhibit a lower reactivity at impact with more residue left and the threshold value reported for impact corresponds to a partial ignition (at the interstice between the steel ring and the steel cylinder, therefore suggesting an ignition by friction).

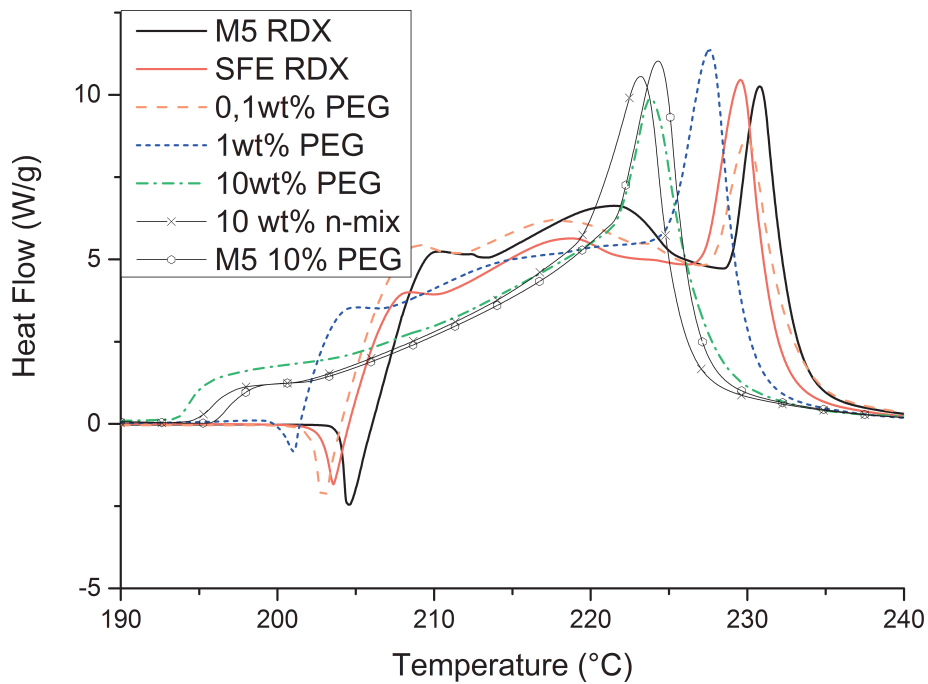
5.2.5 Comparison with mechanically mixed samples

Mechanical mixes with 10 wt% of PVP or PEG and nano or the raw micron-sized M5 RDX were done: DSC results can be seen in Figure 5.15. Figure 5.15a illustrates effect of the size since the decomposition peak of the 10wt% sample (5 μm) is between the nano (500 nm) and micron (7 μm) size pure RDX, while the fusion starts at lower temperature. That's the same phenomenon for the 0.1wt% sample comparable to pure nano and micron size pure RDX. For the PVP mixes in Figure 5.15b, the comparison between the 10wt% sample, the n-mix and the μ -mix ask the question of the distribution of polymer across the sample. We will focus on the distribution of polymer in another study when the Tip Enhanced Raman Spectroscopy (TERS) apparatus will be available.

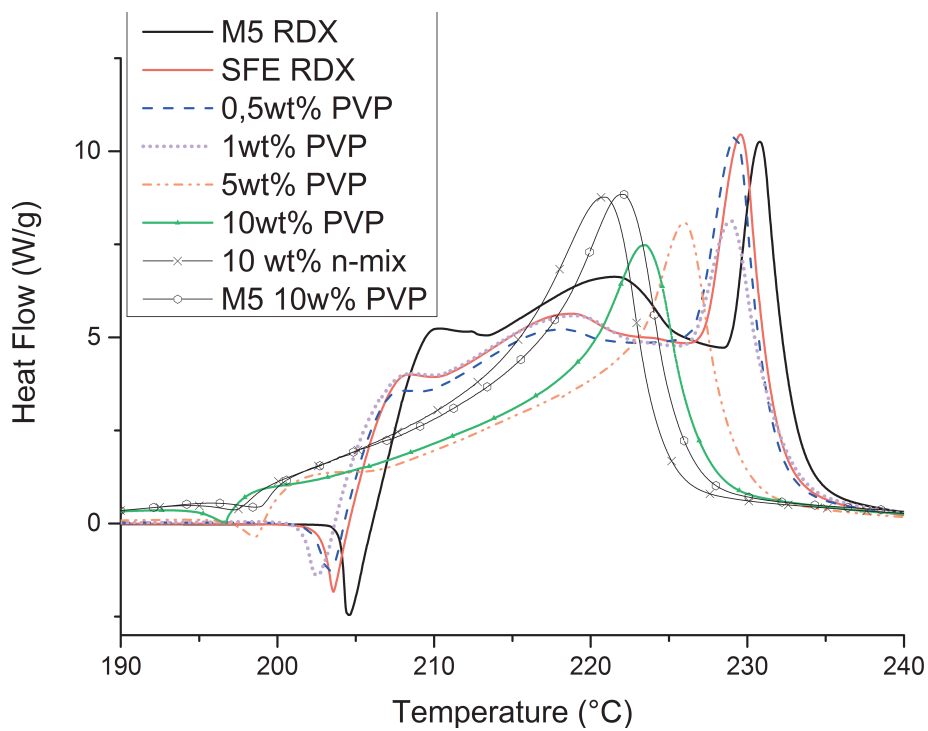
Sensitivity tests were conducted with those mechanic mixes: the n-mix of 10 wt% PEG is very insensitive (it did not react at 37 J) while the impact sensitivity of the n-mix of 10 wt% PVP is higher. So in the first case the humidification and coating by the liquid PEG could totally inhibit RDX, and in the second one, the issue comes from the difficult homogenisation of a micron size solid PVP with submicron RDX. This increases the need of a TERS apparatus to have much more reliable and precise interpretation.

5.3 Summary of the Chapter

The great versatility of the Spray Flash Evaporation allows the processing of solid (PVP 40K) and liquid (PEG 400) polymers to tune the particle size distribution of the final dried nano, submicron or micron-sized powder. PEG triggers the early nucleation of RDX with low nucleation rate leading to bigger particles up to 5 μm . PVP acts as a nucleation inhibitor and a growth inhibitor:



(a) RDX processed with PEG



(b) RDX processed with PVP

Figure 5.15 – DSC analysis of RDX samples processed with PVP and PEG: comparison of mechanical mixes with 10 wt% of PVP or PEG.

RDX nuclei are formed in less volume available due to the fission and flashing of droplets, and then the crystal growth is slowed, thus allowing the formation of much smaller particles at 160 nm with a spherical shape. The addition of PEG could have increased supersaturation to trigger nucleation at a maximal rate but our results show that the contribution of both the evaporation behaviour and the nucleation inhibition is more effective and probably the safest choice to reduce and stabilize the particle size and morphology.

Despite a lower thermal stability, the synthesized RDX composites exhibit reduced sensitivities in electrostatic discharge, friction and impact without loss of reactivity and are less prone to Ostwald ripening. The present work is a great advance in the processability of composite and organic compounds by the SFE technology. The sample synthesized here are also promising for the control of the reactive properties of RDX. Further studies should be performed by TERS to elucidate the question of the distribution of polymer across the sample.

Linking size of droplets, and so supersaturation, to particle size and kinetics of crystallisation is still of interest. In addition to PDA, experiments under the X-Ray beam from a particle accelerator would provide more information of the crystallisation kinetics; our application for beamtime at the ESRF has been recently approved and scheduled for the end of 2016. SAXS will provide information about existing nuclei in droplets as a function of space by scanning the spray and as a function of temperature

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Related Work

Innovations

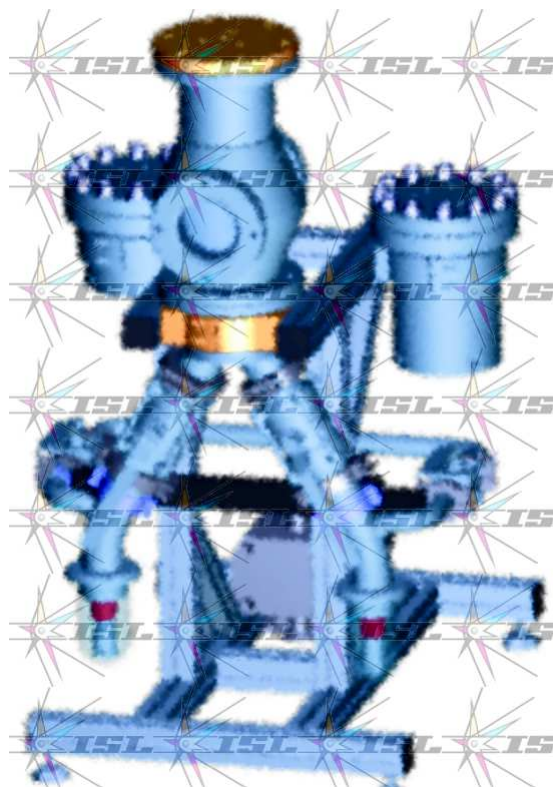


Figure 5.16 – New model of SFE with a reduced size.

SFE Apparatuses Several models of SFE were build prior to my arrival. In order to increase the number of SFE available, a new SFE model was designed with enhanced ergonomy and compactness in cooperation with Ing J. Urban from ISL. I designed and bought the hydraulic system and took care of the budget and assembly of those machines. With the PhD student Axel Le Brize, we performed the maintenance of all the SFE apparatuses and I manage the purchases and improvements on all models. To study the physico-chemical phenomena, a new vacuum chamber was designed for PDA and a whole second injection system was build on an existing apparatus. I have launched and managed the modernization of a laboratory to change the layout, to make available the use of the PDA mounted on an internally designed micrometer traverse and to enhance the whole ergonomy of the pre existing models of SFE.

SFE *in situ* measurements Additional equipments have to be purchase in order to quantify and study precisely the phenomena occurring in the SFE. The inherent risk of the use of energetic materials makes almost impossible –or at

least very limited– any scientific collaboration. I instigated this project which started by the challenging selection of an appropriate technology to measure on-line velocities and sizes. Then a sizeable budget was allocated from public funding thus delaying the effective acquisition of the PDA.

In the mean time, experiments under the X-Ray beam from a particle accelerator have been planned as part of my PhD project, in order to provide more information of the crystallisation; SAXS measurement will allow us to link existing nuclei in droplets in space by scanning the spray but also as a function of temperature. Thanks to Dr Spitzer who supported that project, our application for beamtime at the ESRF has been quite recently approved and scheduled for the end of 2016, after a long process of approval by an international committee and a Safety group.

With MCF Dr. Lobry and Dr. Bonnot, a project for *in situ* Fast Scanning Calorimetry on micro chip has also been started. The study aims to quantify the evaporation kinetics under vacuum of the metastable droplets in SFE, to analyse solid particles at different locations and so to map the crystallization and evaporation in or near an SFE spray. Dr. Bonnot conducted preliminary experiments of standard explosives dissolved in solvents, and the support system with fine controls has been designed.

Analysis Improvements The analysis of data acquired from various characterization techniques was improved. For instance, the use of the software Gwyddion increased the accuracy and the time spent on AFM images; the Rietveld method was introduced to colleagues to get more information from XRD patterns. A database of all experiments made from SFE was set to study reproducibility and perform statistical analysis

Published Work and Communication

Communications

- EuroPyro 2015, 41st International Pyrotechnic Seminar (Toulouse).
- 4th ISL Budding Science Colloquium (Saint Louis, 2015).
- European Congress and Exhibition on Advanced Materials and Processes EUROMAT 2015, B1.3 Section Nanocrystallisation (Warsaw).
- Material Weekend Warsaw 2015; a PhD student workshop from both E-MRS and FEMS societies.

- exhibitor at the 2016 Eurosatory, Defence and Security International Exhibition (572 exhibitors from 56 countries, 213 official delegations from 94 countries)
- 5th ISL Budding Science Colloquium (Saint Louis, 2016).
- Junior EUROMAT 2016 (Lausanne).
- 6th NANOstructures and nanomaterials SELF-Assembly (NanoSEA) (Giardini Naxos (ME), Italy 2016).
- 1 poster: 3rd ISL Budding Science Colloquium (2014)

Publications

- Blas, Lucia, Martin Klaumünzer, **Florent Pessina**, Silke Braun, and Denis Spitzer. "Nanostructuring of Pure and Composite-Based K6 Formulations with Low Sensitivities." *Propellants, Explosives, Pyrotechnics* 40, no. 6 (2015): 938–44.
- **Florent Pessina**, Fabien Schnell, and Denis Spitzer. "Tunable Continuous Production of RDX from Microns to Nanoscale Using Polymeric Additives." *Chemical Engineering Journal* 291 (May 1, 2016): 12–19. doi:10.1016/j.cej.2016.01.083.
- Martin Klaumünzer, **Florent Pessina**, and Denis Spitzer. "Indicating Inconsistency of Desensitizing High Explosives against Impact through Recrystallisation at the Nanoscale." *Journal of Energetic Materials*, July 1, 2016, 1–10. doi:10.1080/07370652.2016.1199610.
- Denis Spitzer, Vincent Pichot, **Florent Pessina**, Fabien Schnell, Martin Klaumünzer, and Lucia Blas. "Continuous and Reactive Nanocrystallisation: New Concepts and Processes for Dual-Use Advances." *Comptes Rendus Chimie*, July 2016. doi:10.1016/j.crci.2016.06.009.
- **Florent Pessina** and Denis Spitzer. "The longstanding challenge of the nano crystallization of 1,3,5-trinitroperhydro-1,3,5-triazine (RDX)" *Beilstein Journal of Nanotechnology* *Under Review*.

Patent

- Risse, Benedikt, Florent Pessina, and Denis Spitzer. Method for producing cocrystals by means of flash evaporation. WO 2016001445, issued January 2016.

Scientific courses

- Sensibilisation à la pyrotechnie 3PSC17C, Centre de Formation de la Défense (Bourges 2013)
- Advanced Functional Materials and Characterization, CNRS-EWHA Winter School (Strasbourg 2014)
- Nano-OptoMechanics, School in Physics (Strasbourg 2014)

Conclusion

Due to the difficult micronisation and nano crystallisation of classical organic explosives such as RDX, advances in insensitive munitions came mainly from new compounds such as NTO or optimizations of each step of the production process (Klapötke et al. 2016; Nouguez et al. 2016). The size reduction of energetic crystals is still of interest not only to produce particles under the critical hot-spot size but also to provide easier shaping and homogeneous energetic compositions. The extensive review of the crystallisation technique used on RDX performed in the Chapter 2 suggests that the Spray Flash Evaporation (SFE) is a well balanced method between spray drying unable to process particles lower than the micrometer, and the expensive batch Rapid Expansion of Supercritical Solutions (RESS) process. The crystallisation in solution is a competitive approach but limited by the drying conditions and its inability to process propellants, unlike the SFE technology (Le Brize et al. 2016).

The present research project was initially focused in the size reduction of crystals produced by this unique technique created in our laboratory. Many challenges were addressed starting by the difficult to commit characterizations of energetic materials, and of the spray itself. Then the crystallisation from SFE has been unveiled with supersaturation variations by solvent exchanges and by polymeric agents.

The nano-technology took off with the invention of the two crucial characterization methods, the Scanning Tunneling Microscopy (STM) and the Atomic Force Microscopy (AFM). The energetic materials are organic crystals where molecules are held together by weak forces; therefore energetic compounds exhibit high sensitivity towards characterization techniques providing energy to the sample. As a consequence, the pyrotechnic community experiences many limitations to assess accurately the particle morphology, their size, aggregation state etc. By trying several characterization techniques especially the microscopy ones, the Environmental Scanning Electron Microscopy (ESEM) has been found to be a suitable technique to process energetic material.

An original method where pellets are flattened then analysed by AFM was in

use previously (Spitzer et al. 2014) and also at the beginning of this present project. It was found that the size measured that way was not a function of the concentration in solution but more of the condition of preparation of the pellets. The compression breaks the brittle crystals with a critical pressure above which the particles reach an even smaller size; while using a microtome, the surface is milled and grooves appear. Sizes down to the crystallite size were found in those grooves. That phenomenon is much more pronounced for n-RDX processed by SFE than for raw micron-sized RDX, just as Spitzer et al. (2011) experienced about opacity and mechanical strength. Those properties could benefit to pressed charges to tune the apparent density and greatly improve homogeneity.

For the SFE process, particle size and shape depend on the crystallisation itself governed by the supersaturation. The degree of supersaturation is unique in each droplet and thus is a function of time and space. The restriction for *in situ* characterization of the droplets for SFE has been overcome by focusing on the chemical route to change the supersaturation and by designing a dual injection system. In that latter system, the persistence of droplet is questioned by using the cocrystal CL-20:HMX. Cocrystallisation occurs in any cases: by using a unique solution and nozzle, by using one solvent but two solutions and nozzles, and also by using two different solvents each one sprayed by one nozzle. Droplets effectively collide from both spray permitting the crystallisation; it is however not clear whether the nucleation occurs before the overlap or the Phase Solubility Diagram (PhSD) of the system does not allow the formation of the sole cocrystal. Further investigations will be performed to quantify the relative crystalline phases and the overlap.

The SFE versatility was again taken a step further within the introduction of solid and viscous polymers in solvent. Those polymers are food additives namely PolyVinylPyrrolidone (PVP) and PolyEthylene Glycol (PEG) and were successfully used to control crystallisation steps. PEG 400 triggers the early nucleation of RDX with low nucleation rate leading to bigger particles up to 5 μm . PVP 40K acts as a nucleation inhibitor and a growth inhibitor: RDX nuclei are formed in less volume available due to the fission and flashing of droplets; then the crystal growth is slowed, thus allowing the formation of much smaller particles at 160 nm with a narrow distribution and a spherical shape. The addition of PEG could have increased supersaturation to trigger nucleation at a maximal rate but results show that the contribution of both the evaporation behaviour and the nucleation inhibition is more effective and probably the surest choice to reduce and stabilize both particle size and morphology. Furthermore, those synthesized energetic composites are less sensitive.

The laboratory acquired very recently a Phase Doppler Analysis (PDA) in order to elucidate the question of supersaturation. Droplets size and velocity will be measured as a function of temperature but also in space within the spray. The dual nozzle system will also benefit from PDA analyses to define the evaporation behaviours while using two solvent or an anti-solvent. Pre-results show droplets of a few microns at high speed more than 100 m/s, suggesting the possible crystallisation from metastable systems.

To summarize, the submicron and nano scales bring to the pyrotechnic community new challenges for the characterization of nano energetic materials. Furthermore, this research project paved the way to global and deeper understanding of the crystallisation aspect of the SFE technology. New apparatuses and designs were explored and implemented as breakthrough for the SFE technology; they led to the control of particle size and shape, and to versatility and industrial-friendly enhancements of the SFE apparatuses.

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Appendix A

Rietveld refinement

A.1 Calibration

```
*****
** PROGRAM FullProf.2k (Version 5.50 - Dec2014-ILL JRC) **
*****
M U L T I  -- P A T T E R N
Rietveld, Profile Matching & Integrated Intensity
Refinement of X-ray and/or Neutron Data

Date: 17/02/2015   Time: 13:47:24.271

=> PCR file code: lab6 - Copie (22) - Copie
=> DAT file code: lab6.dat           -> Relative contribution: 1.0000

==> CONDITIONS OF THIS RUN FOR PATTERN No.: 1

=> Global Refinement of X-ray powder diffraction data
=> Global Refinement of X-ray powder diffraction data
Flat plate with PSD
=> Title: ALS 11-BM - NIST SRM 660a LaB6

=> Number of phases:      1
=> Number of excluded regions: 0
=> Number of scattering factors supplied: 0
=> March-Dollase model for preferred orientation
=> Conventional weights: w=1.0/Variance(yobs)
=> Asymmetry correction as in J.Appl.Cryst. 26,128(1993)
=> Background linearly interpolated between the 7 points given
=> The 5th default profile function was selected
=> Pseudo-Voigt function (ETA variable)
X-parameter correspond to: ETA=ETA0+X*2theta
pV(x)= ETA*L(x)+(1-ETA)*G(x)

==> INPUT/OUTPUT OPTIONS:

=> Generate bacground file *.bac
=> Generate file *.PRF for plot
=> Output Integrated Intensities
=> Output Correlation Matrix
=> Generate new input file *.PCR

=> Data supplied in free format for pattern: 1
=> Plot pattern at each cycle
=> Wavelengths: 1.54059 1.54431
=> Alpha2/Alpha1 ratio: 0.5000
=> Cos(Monochromator angle)= 1.0000
=> Asymmetry correction for angles lower than 90.000 degrees
=> Absorption correction (AC), muR-eff = 0.0000 0.0000
=> Base of peaks: 2.0*HW* 20.00

=> Number of cycles: 50
=> Relaxation factors ==> for coordinates: 1.00
=> for anisotropic temperature factors: 1.00
=> for halfwidth/strain/size parameters: 1.00
=> for lattice constants and propagation vectors: 1.00
=> EPS-value for convergence: 0.0
=> Background ==>
Position  Intensity
20.00    22.22    0.00
30.00    21.64    0.00
40.00    18.36    0.00
55.00    12.77    0.00
60.00     9.61    0.00
75.00    12.58    0.00
```

120.00 7.64 0.00

=> Number of Least-Squares parameters varied: 12

=>----->

=>-----> PATTERN number: 1

=>----->

=> Global parameters and codes ==>

=> Zero-point: -0.2111 11.0000

=> Displacement peak-shift parameter and code: 0.08 21.00

=> Transparency peak-shift parameter and code: 0.04 31.00

=> Reading Intensity data =>>

==> Angular range, step and number of points:

2Thmin: 17.540501 2Thmax: 152.554001 Step: 0.019332 No. of points: 6985

=> Phase No. 1

NIST SRM 660a LaB6

=>-----> Pattern# 1

=> Crystal Structure Refinement

=> The 7th profile function was selected for phase no. 1

=> Preferred orientation vector: 0.0000 0.0000 1.0000

=>-----> Data for PHASE: 1

=> Number of atoms: 2

=> Number of distance constraints: 0

=> Number of angle constraints: 0

=> Symmetry information on space group: P m 3 m

-> The multiplicity of the general position is: 48

-> The space group is Centric (-1 at origin)

-> Lattice type P: { 000 }

-> Reduced set of symmetry operators:

No.	IT	Symmetry symbol	Rotation part	Associated Translation
1:	(1)	1	-->	(x, y, z) + { 0.0000 0.0000 0.0000}
2:	(4)	2 (x, 0, 0)	-->	(x,-y,-z) + { 0.0000 0.0000 0.0000}
3:	(3)	2 (0, y, 0)	-->	(-x, y,-z) + { 0.0000 0.0000 0.0000}
4:	(2)	2 (0, 0, z)	-->	(-x,-y, z) + { 0.0000 0.0000 0.0000}
5:	(9)	3- (x, x, x)	-->	(y, z, x) + { 0.0000 0.0000 0.0000}
6:	(12)	3- (-x, x,-x)	-->	(-y,-z, x) + { 0.0000 0.0000 0.0000}
7:	(11)	3- (-x,-x, x)	-->	(y,-z,-x) + { 0.0000 0.0000 0.0000}
8:	(10)	3- (x,-x,-x)	-->	(-y, z,-x) + { 0.0000 0.0000 0.0000}
9:	(5)	3+ (x, x, x)	-->	(z, x, y) + { 0.0000 0.0000 0.0000}
10:	(8)	3+ (-x,-x, x)	-->	(-z, x,-y) + { 0.0000 0.0000 0.0000}
11:	(7)	3+ (x,-x,-x)	-->	(-z,-x, y) + { 0.0000 0.0000 0.0000}
12:	(6)	3+ (-x, x,-x)	-->	(z,-x,-y) + { 0.0000 0.0000 0.0000}
13:	(14)	2 (x,-x, 0)	-->	(-y,-x,-z) + { 0.0000 0.0000 0.0000}
14:	(15)	4- (0, 0, z)	-->	(y,-x, z) + { 0.0000 0.0000 0.0000}
15:	(16)	4+ (0, 0, z)	-->	(-y, x, z) + { 0.0000 0.0000 0.0000}
16:	(13)	2 (x, x, 0)	-->	(y, x,-z) + { 0.0000 0.0000 0.0000}
17:	(24)	2 (-x, 0, x)	-->	(-z,-y,-x) + { 0.0000 0.0000 0.0000}
18:	(21)	4+ (0, y, 0)	-->	(z, y,-x) + { 0.0000 0.0000 0.0000}
19:	(22)	2 (x, 0, x)	-->	(z,-y, x) + { 0.0000 0.0000 0.0000}
20:	(23)	4- (0, y, 0)	-->	(-z, y, x) + { 0.0000 0.0000 0.0000}
21:	(19)	2 (0, y,-y)	-->	(-x,-z,-y) + { 0.0000 0.0000 0.0000}
22:	(18)	2 (0, y, y)	-->	(-x, z, y) + { 0.0000 0.0000 0.0000}
23:	(17)	4- (x, 0, 0)	-->	(x, z,-y) + { 0.0000 0.0000 0.0000}
24:	(20)	4+ (x, 0, 0)	-->	(x,-z, y) + { 0.0000 0.0000 0.0000}

Information on Space Group:

=> Number of Space group: 221

=> Hermann-Mauguin Symbol: P m 3 m

=> Hall Symbol: -P 4 2 3

=> Table Setting Choice:

=> Setting Type: IT (Generated from Hermann-Mauguin symbol)

=> Crystal System: Cubic

=> Laue Class: m-3m

=> Point Group: m-3m

=> Bravais Lattice: P

=> Lattice Symbol: cP

=> Reduced Number of S.O.: 24

=> General multiplicity: 48

=> Centrosymmetry: Centric (-1 at origin)

=> Generators (exc. -1&L): 3

=> Asymmetric unit: 0.000 <= x <= 0.500

0.000 <= y <= 0.500

0.000 <= z <= 0.500

=> List of S.O. without inversion and lattice centring translations

=> SYMM(1): x,y,z => SYMM(2): x,-y,-z

=> SYMM(3): -x,y,-z => SYMM(4): -x,-y,z

=> SYMM(5): y,z,x => SYMM(6): -y,-z,x

=> SYMM(7): y,-z,-x => SYMM(8): -y,z,-x

```

=> SYMM( 9): z,x,y           => SYMM( 10): -z,x,-y
=> SYMM( 11): -z,-x,y        => SYMM( 12): z,-x,-y
=> SYMM( 13): y,x,z          => SYMM( 14): -y,x,-z
=> SYMM( 15): y,-x,-z       => SYMM( 16): -y,-x,z
=> SYMM( 17): z,y,x          => SYMM( 18): -z,-y,x
=> SYMM( 19): -z,y,-x       => SYMM( 20): z,-y,-x
=> SYMM( 21): x,z,y          => SYMM( 22): x,-z,-y
=> SYMM( 23): -x,-z,y       => SYMM( 24): -x,z,-y

=> Initial parameters ==>
Atom  Ntyp      X      Y      Z      B      occ.      in  fin  Spc  Mult
B11   B22   B33   B12   B13   B23
La    La      0.00000 0.00000 0.00000 0.41517 0.16666      0   0   0   1
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000
B     B      0.20319 0.50000 0.50000 0.26488 1.00000      0   0   0   6
Codes: 41.00000 0.00000 0.00000 0.00000 0.00000

=> IT IS ASSUMED THAT THE FIRST GIVEN SITE IS FULLY OCCUPIED
OR THE FIRST AND SECOND ATOMS ARE IN THE SAME SITE WITH TOTAL FULL OCCUPATION
(If this is not the case, change the order of atoms to obtain correct values for the content of the unit cell)
The given occupation factors have been obtained mutiplying m/M by 7.9997
-> Atom: La , Chemical element: LA Atomic Mass: 138.9055
-> Atom: B , Chemical element: B Atomic Mass: 10.8100
=> The given value of ATZ is 1630.08 the program has calculated: 13040.11
The value of ATZ given in the input PCR file will be used for quantitative analysis
=> The chemical content of the unit cell is:
1.0000 La + 6.0002 B
=> The normalized site occupation numbers in % are:
100.0000 La : 100.0040 B
=> The density (volumic mass) of the compound is: 4.717 g/cm3

=>-----> PROFILE PARAMETERS FOR PATTERN: 1

=> Overall scale factor: 0.125350E-03
=> ETA (p-Voigt) OR M (Pearson VII): 0.0000
=> Overall temperature factor: 0.000000
=> Halfwidth U,V,W: 0.00136 -0.00500 0.00391
=> X and Y parameters: 0.0639 0.0001
=> Direct cell parameters: 4.1550 4.1550 4.1550 90.0000 90.0000 90.0000
=> Preferred orientation parameters: 1.0000 0.0000
=> Asymmetry parameters : -0.03244 0.04207 0.00000 0.00000
=> Strain parameters : 0.00000 0.00000 0.00000
=> Size parameters : 0.00000 0.00000
=> Further shape parameters (S_L and D_L): 0.00000 0.00000
S_L is source width/detector distance
D_L is detector width/detector distance

==> CODEWORDS FOR PROFILE PARAMETERS of PATTERN# 1

=> Overall scale factor: 51.000
=> ETA (p-Voigt) OR M (Pearson VII): 0.000
=> Overall temperature factor: 0.000
=> Halfwidth U,V,W: 61.000 71.000 81.000
=> X and Y parameters: 101.000 110.000
=> Direct cell parameters: 0.000 0.000 0.000 0.000 0.000 0.000
=> Preferred orientation parameters: 0.000 0.000
=> Asymmetry parameters : 91.000 121.000 0.000 0.000
=> Strain parameters : 0.000 0.000 0.000
=> Size parameters : 0.000 0.000

=> Cell constraints according to Laue symmetry: m-3m

Metric information:
-----
=> Direct cell parameters:

a = 4.1550 b = 4.1550 c = 4.1550
alpha = 90.000 beta = 90.000 gamma = 90.000
Direct Cell Volume = 71.7313

=> Reciprocal cell parameters:

a*= 0.240675 b*= 0.240675 c*= 0.240675
alpha*= 90.000 beta*= 90.000 gamma*= 90.000
Reciprocal Cell Volume = 0.01394091

=> Direct and Reciprocal Metric Tensors:

GD GR
17.2639 0.0000 0.0000 0.057924 0.000000 0.000000
0.0000 17.2639 0.0000 0.000000 0.057924 0.000000
0.0000 0.0000 17.2639 0.000000 0.000000 0.057924

=> Cartesian frame: x // a; y is in the ab-plane; z is x ^ y

Crystal_to_Orthonormal_Matrix Orthonormal_to_Crystal_Matrix
Cr_Orth_cel Orth_Cr_cel
4.1550 0.0000 0.0000 0.240675 0.000000 0.000000

```

```
0.0000    4.1550    0.0000    0.000000    0.240675    0.000000
0.0000    0.0000    4.1550    0.000000    0.000000    0.240675
```

```
Busing-Levy B-matrix: Hc=B.H          Inverse of the Busing-Levy B-matrix
BL_M          BL_Minv
0.240675    0.000000    0.000000    4.1550    0.0000    0.0000
0.000000    0.240675    0.000000    0.0000    4.1550    0.0000
0.000000    0.000000    0.240675    0.0000    0.0000    4.1550
```

```
=> Laue symmetry m-3m will be used to generate HKL for pattern# 1
=> Reflections generated between S(1/d)min: 0.1975 A-1 and S(1/d)max: 1.2677 A-1
=>          dmax: 5.0642 A and          dmin: 0.7888 A
=> The number of reflections generated is: 30
=> The max. scatt. variable (gen.ref.) is: 155.1055
=> Scattering coefficients from internal table
```

```
=> X-ray scattering coeff. (A1, B1, A2,...C, f(0), Z, Dfp,Dfpp)
```

```
LA    20.5780    2.9482    19.5990    0.2445    11.3727    18.7726    3.2872    133.1240    2.1468    56.9837    57.0000    -1.7160  ↵
9.0360
B      2.0545    23.2185    1.3326    1.0210    1.0979    60.3498    0.7068    0.1403    -0.1932    4.9986    5.0000    0.0080  ↵
0.0040
```

```
-----
SYMBOLIC NAMES AND INITIAL VALUES OF PARAMETERS TO BE VARIED:
-----
```

```
-> Parameter number 1 -> Symbolic Name: Zero_pat1 -0.21106000
-> Parameter number 2 -> Symbolic Name: SyCos_pat1 0.76700002E-01
-> Parameter number 3 -> Symbolic Name: SySin_pat1 0.38720001E-01
-> Parameter number 4 -> Symbolic Name: X_B_ph1 0.20319000
-> Parameter number 5 -> Symbolic Name: Scale_ph1_pat1 0.12534999E-03
-> Parameter number 6 -> Symbolic Name: U-Cagl_ph1_pat1 0.13560000E-02
-> Parameter number 7 -> Symbolic Name: V-Cagl_ph1_pat1 -0.49999999E-02
-> Parameter number 8 -> Symbolic Name: W-Cagl_ph1_pat1 0.39100000E-02
-> Parameter number 9 -> Symbolic Name: Asym1_ph1_pat1 -0.32439999E-01
-> Parameter number 10 -> Symbolic Name: X-tan_ph1_pat1 0.63895002E-01
-> Parameter number 11 -> Symbolic Name: Y-cos_ph1_pat1 0.00000000
-> Parameter number 12 -> Symbolic Name: Asym2_ph1_pat1 0.42070001E-01
```

```
=> Zero counts at step no. 3 at 2theta/TOF/E(KeV): 17.5792 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 4 at 2theta/TOF/E(KeV): 17.5985 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 5 at 2theta/TOF/E(KeV): 17.6178 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 6 at 2theta/TOF/E(KeV): 17.6372 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 7 at 2theta/TOF/E(KeV): 17.6565 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 8 at 2theta/TOF/E(KeV): 17.6758 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 9 at 2theta/TOF/E(KeV): 17.6952 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 12 at 2theta/TOF/E(KeV): 17.7532 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 13 at 2theta/TOF/E(KeV): 17.7725 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 14 at 2theta/TOF/E(KeV): 17.7918 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 16 at 2theta/TOF/E(KeV): 17.8305 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 17 at 2theta/TOF/E(KeV): 17.8498 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 19 at 2theta/TOF/E(KeV): 17.8885 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 22 at 2theta/TOF/E(KeV): 17.9465 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 24 at 2theta/TOF/E(KeV): 17.9851 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 25 at 2theta/TOF/E(KeV): 18.0045 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 30 at 2theta/TOF/E(KeV): 18.1011 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 31 at 2theta/TOF/E(KeV): 18.1205 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 32 at 2theta/TOF/E(KeV): 18.1398 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 33 at 2theta/TOF/E(KeV): 18.1591 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 34 at 2theta/TOF/E(KeV): 18.1785 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 35 at 2theta/TOF/E(KeV): 18.1978 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 36 at 2theta/TOF/E(KeV): 18.2171 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 37 at 2theta/TOF/E(KeV): 18.2364 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 38 at 2theta/TOF/E(KeV): 18.2558 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 40 at 2theta/TOF/E(KeV): 18.2944 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 43 at 2theta/TOF/E(KeV): 18.3524 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 44 at 2theta/TOF/E(KeV): 18.3718 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 45 at 2theta/TOF/E(KeV): 18.3911 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 46 at 2theta/TOF/E(KeV): 18.4104 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 48 at 2theta/TOF/E(KeV): 18.4491 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 49 at 2theta/TOF/E(KeV): 18.4684 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 51 at 2theta/TOF/E(KeV): 18.5071 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 52 at 2theta/TOF/E(KeV): 18.5264 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 53 at 2theta/TOF/E(KeV): 18.5458 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 55 at 2theta/TOF/E(KeV): 18.5844 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 56 at 2theta/TOF/E(KeV): 18.6038 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 57 at 2theta/TOF/E(KeV): 18.6231 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 59 at 2theta/TOF/E(KeV): 18.6617 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 61 at 2theta/TOF/E(KeV): 18.7004 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 64 at 2theta/TOF/E(KeV): 18.7584 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 66 at 2theta/TOF/E(KeV): 18.7971 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 67 at 2theta/TOF/E(KeV): 18.8164 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 68 at 2theta/TOF/E(KeV): 18.8357 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 70 at 2theta/TOF/E(KeV): 18.8744 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 71 at 2theta/TOF/E(KeV): 18.8937 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 73 at 2theta/TOF/E(KeV): 18.9324 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 74 at 2theta/TOF/E(KeV): 18.9517 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 75 at 2theta/TOF/E(KeV): 18.9711 Intensity fixed to 1.0 and variance to 1E6
```



```

=> Square of FWHM(G) < 0 at 2theta: 130.522 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 131.126 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 135.929 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 135.929 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 136.618 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 136.618 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 99.705 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 99.705 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 100.033 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 100.033 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 103.728 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 103.728 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 104.081 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 104.081 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 107.821 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 108.202 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 112.011 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 112.422 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 116.329 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 116.776 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 120.815 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 121.304 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 130.522 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 131.126 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 135.929 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 135.929 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 136.618 for phase no. 1 -> Fixing to HG=1.0e-10
=> Square of FWHM(G) < 0 at 2theta: 136.618 for phase no. 1 -> Fixing to HG=1.0e-10

```

Standard deviations have to be multiplied by: 2.1538
(correlated residuals) See references:
-J.F.Berar & P.Lelann, J. Appl. Cryst. 24, 1-5 (1991)
-J.F.Berar, Acc. in Pow. Diff. II, NIST Sp.Pub. 846, 63(1992)

+++++

=> CYCLE No.: 50

=> Phase 1 Name: NIST SRM 660a LaB6

=> New parameters, shifts, and standard deviations

Atom	x	dx	sx	y	dy	sy	z	dz	sz	B	dB	sB	occ.
	docc.	socc.											
La	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.41517	0.00000	0.00000	
	0.16666	0.00000	0.00000										
B	0.20319	0.00001	0.00193	0.50000	0.00000	0.00000	0.50000	0.00000	0.00000	0.26488	0.00000	0.00000	
	1.00000	0.00000	0.00000										

==> PROFILE PARAMETERS FOR PATTERN# 1

```

=> Overall scale factor: 0.000125355 0.000000003 0.000000635
=> Eta(p-Voigt) or m(Pearson VII): 0.000000 0.000000 0.000000
=> Overall tem. factor: 0.000000 0.000000 0.000000
=> Halfwidth parameters:
0.001356 0.000000 0.000000
-0.005000 0.000000 0.000000
0.003910 0.000000 0.000000
=> Cell parameters:
4.154987 0.000000 0.000000
4.154987 0.000000 0.000000
4.154987 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
=> Preferred orientation:
1.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Asymmetry parameters:
-0.032396 0.000130 0.031169
0.042064 0.000018 0.004032
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> X and Y parameters:
0.063891 -0.000003 0.001582
0.000083 0.000000 0.000000
=> Strain parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Size parameters (G,L):
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Further shape parameters (S_L and D_L):
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

```

==> GLOBAL PARAMETERS FOR PATTERN# 1

=> Zero-point: -0.2111 0.0000 0.0033
=> Cos(theta)-shift parameter : 0.0767 0.0000 0.0034
=> Sin(2theta)-shift parameter : 0.0387 0.0000 0.0025

==> RELIABILITY FACTORS WITH ALL NON-EXCLUDED POINTS FOR PATTERN: 1

=> R-Factors: 20.8 31.0 Chi2: 18.6 DW-Stat.: 1.2720 Patt#: 1
=> Expected : 7.20 1.9292
=> Deviance : 0.187E+06 Dev*: 26.62
=> GoF-index: 4.3 Sqrt(Residual/N)
=> N-P+C: 6973

SumYdif	SumYobs	SumYcal	SumYobsSQ	Residual	Condition
0.2802E+06	0.1347E+07	0.1232E+07	0.1347E+07	0.1296E+06	0.5539E+19

=> Conventional Rietveld Rp,Rwp,Re and Chi2: 22.2 32.2 7.47 18.59
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2): 0.1263E+07 0.1250E+07

=> N-sigma of the GoF: 1038.716

==> RELIABILITY FACTORS FOR POINTS WITH BRAGG CONTRIBUTIONS FOR PATTERN: 1

=> R-Factors: 18.1 27.0 Chi2: 20.7 DW-Stat.: 1.7601 Patt#: 1
=> Expected : 5.94 1.9131
=> Deviance : 0.115E+06 Dev*: 25.16
=> GoF-index: 4.5 Sqrt(Residual/N)
=> N-P+C: 4520

SumYdif	SumYobs	SumYcal	SumYobsSQ	Residual	Condition
0.2316E+06	0.1282E+07	0.1196E+07	0.1282E+07	0.9369E+05	0.5539E+19

=> Conventional Rietveld Rp,Rwp,Re and Chi2: 18.8 27.8 6.10 20.73
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2): 0.1234E+07 0.1214E+07

=> N-sigma of the GoF: 937.871

=> Global user-weighted Chi2 (Bragg contrib.): 28.7

=> Parameters with Correlation greater than 50% ==>

-> Correlation of parameter: SyCos_pat1 with: Asym1_phi_pat1 -> 59%
-> Correlation of parameter: U-Cagl_phi_pat1 with: W-Cagl_phi_pat1 -> 97%
-> Correlation of parameter: Asym1_phi_pat1 with: Asym2_phi_pat1 -> 78%

Pattern# 1 Phase No: 1 Phase name: NIST SRM 660a LaB6

No.	Code	H	K	L	Mult	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	✓
		d-hkl			CORR									
1	1	1	0	0	6	0.061502	21.368	1797.6	1521.0	249.828	0.054909	0.012139	0.251880	✓
		4.154987				165.860336								
2	1	1	1	0	12	0.061195	30.399	2934.7	2710.7	207.324	0.051494	0.017445	0.353212	✓
		2.938020				157.740463								
3	1	1	1	1	8	0.061081	37.460	1202.4	1216.5	52.185	0.048689	0.021752	0.430965	✓
		2.398883				66.773720								
4	1	2	0	0	6	0.061089	43.528	608.9	699.3	107.291	0.046151	0.025598	0.496798	✓
		2.077493				35.848160								
5	1	2	1	0	24	0.061194	48.981	1366.4	1486.0	130.218	0.043746	0.029197	0.555200	✓
		1.858167				109.784355								
6	1	2	1	1	24	0.061383	54.016	718.7	764.6	61.204	0.041398	0.032660	0.608466	✓
		1.696266				87.862114								
7	1	2	2	0	12	0.062005	63.251	258.8	307.7	73.329	0.036676	0.039444	0.704498	✓
		1.469010				30.818932								
8	1	2	2	1	24	0.062452	67.583	685.8	728.3	47.546	0.034222	0.042859	0.748658	✓
		1.384996				53.468040								
9	1	3	0	0	6	0.062452	67.583	64.2	68.2	4.452	0.034222	0.042859	0.748658	✓
		1.384996				13.367010								
10	1	3	1	0	24	0.063010	71.784	526.5	579.4	64.701	0.031651	0.046340	0.790745	✓
		1.313922				47.309349								
11	1	3	1	1	24	0.063710	75.885	328.0	394.7	87.832	0.028913	0.049921	0.830880	✓
		1.252776				42.641338								
12	1	2	2	2	8	0.064590	79.914	56.5	80.4	61.407	0.025937	0.053640	0.868999	✓
		1.199441				13.040545								
13	1	3	2	0	24	0.065710	83.893	215.7	254.5	53.076	0.022620	0.057534	0.904843	✓
		1.152386				36.518417								
14	1	3	2	1	48	0.067145	87.842	440.7	517.2	95.924	0.018773	0.061647	0.937958	✓
		1.110467				69.344658								
15	1	4	0	0	6	0.071370	95.729	78.4	107.3	64.667	0.006325	0.070749	0.993505	✓
		1.038747				8.212687								
16	1	3	2	2	24	0.075877	99.705	230.5	275.6	55.802	0.000000	0.075877	1.000000	✓

17	1	4	1	0	24	0.075877	99.705	153.8	183.9	37.232	0.000000	0.075877	1.000000	↙
	1.007732		32.758747											
18	1	3	3	0	12	0.081515	103.728	149.2	177.3	36.422	0.000000	0.081515	1.000000	↙
	0.979340		16.589645											
19	1	4	1	1	24	0.081515	103.728	180.6	214.6	44.076	0.000000	0.081515	1.000000	↙
	0.979340		33.179291											
20	1	3	3	1	24	0.087795	107.821	141.2	182.3	68.989	0.000000	0.087795	1.000000	↙
	0.953219		34.118217											
21	1	4	2	0	24	0.094895	112.011	206.7	261.2	92.342	0.000000	0.094895	1.000000	↙
	0.929083		35.608879											
22	1	4	2	1	48	0.103065	116.329	435.8	522.1	114.945	0.000000	0.103065	1.000000	↙
	0.906693		75.439613											
23	1	3	3	2	24	0.112675	120.815	224.1	291.6	93.741	0.000000	0.112675	1.000000	↙
	0.885846		40.570278											
24	1	4	2	2	24	0.138865	130.522	165.4	232.8	116.853	0.000000	0.138865	1.000000	↙
	0.848133		49.438599											
25	1	4	3	0	24	0.158083	135.929	146.5	214.0	100.787	0.000000	0.158083	1.000000	↙
	0.830997		56.440228											
26	1	5	0	0	6	0.158083	135.929	48.4	70.7	33.271	0.000000	0.158083	1.000000	↙
	0.830997		14.110057											
27	1	4	3	1	48	0.189935	141.927	652.1	799.8	181.250	0.028438	0.185430	0.982242	↙
	0.814860		133.368210											
28	1	5	1	0	24	0.189935	141.927	258.1	316.6	71.748	0.028438	0.185430	0.982242	↙
	0.814860		66.684105											
29	1	3	3	3	8	0.244371	148.866	64.1	82.6	23.763	0.058602	0.229661	0.954600	↙
	0.799628		27.829784											
30	1	5	1	1	24	0.244371	148.866	448.9	577.8	166.343	0.058602	0.229661	0.954600	↙
	0.799628		83.489349											

 BRAGG R-Factors and weight fractions for Pattern # 1

=> Phase: 1 NIST SRM 660a LaB6
 => Bragg R-factor: 13.0 Vol: 71.731(0.000) Fract(%): 100.00(0.72)
 => Rf-factor= 8.65 ATZ: 1630.079 Brindley: 1.0000

 SYMBOLIC NAMES AND FINAL VALUES AND SIGMA OF REFINED PARAMETERS:

-> Parameter number	1 :	Zero_pat1	-0.21106540	(+/-	0.32565552E-02)
-> Parameter number	2 :	SyCos_pat1	0.76720364E-01	(+/-	0.33641579E-02)
-> Parameter number	3 :	SySin_pat1	0.38725469E-01	(+/-	0.24757127E-02)
-> Parameter number	4 :	X_B_ph1	0.20319004	(+/-	0.19287585E-02)
-> Parameter number	5 :	Scale_ph1_pat1	0.12535467E-03	(+/-	0.63530314E-06)
-> Parameter number	6 :	U-Cagl_ph1_pat1	0.13559998E-02	(+/-	0.38470202E-09)
-> Parameter number	7 :	V-Cagl_ph1_pat1	-0.49999999E-02	(+/-	0.13145328E-08)
-> Parameter number	8 :	W-Cagl_ph1_pat1	0.39100000E-02	(+/-	0.10740180E-08)
-> Parameter number	9 :	Asym1_ph1_pat1	-0.32395910E-01	(+/-	0.31169372E-01)
-> Parameter number	10 :	X-tan_ph1_pat1	0.63890785E-01	(+/-	0.15823194E-02)
-> Parameter number	11 :	Y-cos_ph1_pat1	0.00000000	(+/-	0.00000000)
-> Parameter number	12 :	Asym2_ph1_pat1	0.42063739E-01	(+/-	0.40319548E-02)

 => Number of bytes for floating point variables: 4
 => Dimensions of dynamic allocated arrays in this run of FullProf:

=> Total approximate array memory (dynamic + static): 107719993 bytes

MaxPOINT= 60000 Max.num. of points(+int. Inten.)/diffraction pattern
 MaxREFLT= 20000 Max.num. of reflections/diffraction pattern
 MaxPARAM= 300 Max.num. of refinable parameters
 MaxOVERL= 2096 Max.num. of overlapping reflections

 => Number of bytes for floating point arrays: 4
 => Dimensions of fixed arrays in this release of FullProf:

NPATT	=	80	Max.num. of powder diffraction patterns
NATS	=	830	Max.num. of atoms (all kind) in asymmetric unit
MPAR	=	1800	Max.num. of non atomic parameters/phase
IEXCL	=	30	Max.num. of excluded regions
IBACP	=	277	Max.num. of background points for interpolation
NPHT	=	16	Max.num. of phases
NMAGM	=	8	Max.num. of rotation-matrices sets for magnetic structure
NBASIS	=	12	Max.num. of basis functions associated to a single atom
NIREPS	=	9	Max.num. of irreducible representations to be combined
N_EQ	=	384	Max.num. of user-supplied symmetry operators/propagation vectors
NGL	=	300	Max.num. of global parameters/diffraction pattern
N_LINC	=	30	Max.num. of global linear restraints
NAT_P	=	64	Max.num. of atomic parameters per atom
NCONST	=	500	Max.num. of slack constraints per phase
N_SPE	=	16	Max.num. of different chemical species
N_FORM	=	60	Max.num. of scattering factor values in a table
NPR	=	150	Max.num. of points defining a numerical profile
INPR	=	25	Max.num. of different numerical peak shapes

```
NPRC   =      150 Max.num. of terms in the table for correcting intensities
NSOL   =      10 Max.num. of solutions to be stored in Montecarlo searches
```

```
CPU Time:      5.328 seconds
0.089 minutes
```

```
=> Run finished at:      Date: 17/02/2015   Time: 13:47:29.606
%\end{Verbatim}
```

A.2 Sample of n-RDX processed pure at 2 wt% in acetone

```
*****
** PROGRAM FullProf.2k (Version 5.60 - Jan2015-ILL JRC) **
*****
M U L T I  -- P A T T E R N
Rietveld, Profile Matching & Integrated Intensity
Refinement of X-ray and/or Neutron Data

Date: 15/06/2015   Time: 11:00:34.452

=> PCR file code: v203
=> DAT file code: v203.dat           -> Relative contribution: 1.0000

==> CONDITIONS OF THIS RUN FOR PATTERN No.: 1

=> Global Refinement of X-ray powder diffraction data
=> Global Refinement of X-ray powder diffraction data
Flat plate with PSD
=> Title:RDX

=> Number of phases:      1
=> Number of excluded regions:      0
=> Number of scattering factors supplied:      0
=> March-Dollase model for preferred orientation
=> Conventional weights: w=1.0/Variance(yobs)
=> Asymmetry correction as in J.Appl.Cryst. 26,128(1993)
=> Background refined by polynomial function
=> The 5th default profile function was selected
=> Pseudo-Voigt function (ETA variable)
X-parameter correspond to: ETA=ETA0+X*2theta
pV(x)= ETA*L(x)+(1-ETA)*G(x)

==> INPUT/OUTPUT OPTIONS:

=> Generate file *.PRF for plot
=> Output Integrated Intensities
=> Generate new input file *.PCR

=> Data supplied in free format for pattern: 1
=> Plot pattern at each cycle
=> Wavelengths: 1.54056 1.54439
=> Alpha2/Alpha1 ratio: 0.5000
=> Cos(Monochromator angle)= 1.0000
=> Asymmetry correction for angles lower than 90.000 degrees
=> Absorption correction (AC), muR-eff = 0.0000 0.0000
=> Base of peaks: 2.0*HW* 20.00

=> Number of cycles: 50
=> Relaxation factors ==> for coordinates: 1.00
=> for anisotropic temperature factors: 1.00
=> for halfwidth/strain/size parameters: 1.00
=> for lattice constants and propagation vectors: 1.00
=> EPS-value for convergence: 0.0
=> Instrumental Resolution read from file: xray-res.irf
=> Title of data: Approximate resolution function of a conventional X-ray diffractometer CuKalpha1,2

=> The resolution function is IRESOL: 1 for profile function # 5
Input resolution parameters:

U-inst   V-inst   W-inst   X-inst   Y-inst   Z-inst
0.00136  -0.00500  0.00391  0.06389  0.00008  0.00000
0.00136  -0.00500  0.00391  0.06389  0.00008  0.00000

=> Number of Least-Squares parameters varied: 60

=>----->
=>-----> PATTERN number: 1
=>----->
=> Global parameters and codes ==>
=> Zero-point: -0.2016 21.0000
=> Background parameters and codes ==>
=> Origin of polynomial at 2theta/TOF/E(KeV): 70.000
0.11847E+06 0.72376E+06 -47087. -0.18536E+07 -0.14029E+07 -35943.
0.00 0.00 0.00 0.00 0.00 0.00
=> Displacement peak-shift parameter and code: 0.00 0.00
=> Transparency peak-shift parameter and code: 0.00 0.00
```


=> Reading Intensity data =>>

==> Angular range, step and number of points:
 2Thmin: 10.000000 2Thmax: 49.998600 Step: 0.003700 No. of points: 10811

=> Phase No. 1
 rdx

=>-----> Pattern# 1
 => Crystal Structure Refinement
 => The 7th profile function was selected for phase no. 1
 => Preferred orientation vector: 0.0000 0.0000 1.0000

=>-----> Data for PHASE: 1
 => Number of atoms: 21
 => Number of distance constraints: 0
 => Number of angle constraints: 0

=> Symmetry information on space group: P b c a
 -> The multiplicity of the general position is: 8
 -> The space group is Centric (-1 at origin)
 -> Lattice type P: { 000 }
 -> Reduced set of symmetry operators:

No.	IT	Symmetry symbol	Rotation part	Associated Translation
1:	(1)	1	--> (x, y, z) + {	0.0000 0.0000 0.0000}
2:	(4)	2 (x, 0, 0)	--> (x,-y,-z) + {	0.5000 0.5000 0.0000}
3:	(3)	2 (0, y, 0)	--> (-x, y,-z) + {	0.0000 0.5000 0.5000}
4:	(2)	2 (0, 0, z)	--> (-x,-y, z) + {	0.5000 0.0000 0.5000}

Information on Space Group:

=> Number of Space group: 61
 => Hermann-Mauguin Symbol: P b c a
 => Hall Symbol: -P 2ac 2ab
 => Table Setting Choice:
 => Setting Type: IT (Generated from Hermann-Mauguin symbol)
 => Crystal System: Orthorhombic
 => Laue Class: mmm
 => Point Group: mmm
 => Bravais Lattice: P
 => Lattice Symbol: oP
 => Reduced Number of S.O.: 4
 => General multiplicity: 8
 => Centrosymmetry: Centric (-1 at origin)
 => Generators (exc. -1&L): 2
 => Asymmetric unit: 0.000 <= x <= 0.500
 0.000 <= y <= 0.500
 0.000 <= z <= 0.500

=> List of S.O. without inversion and lattice centring translations
 => SYMM(1): x,y,z => SYMM(2): x+1/2,-y+1/2,-z
 => SYMM(3): -x,y+1/2,-z+1/2 => SYMM(4): -x+1/2,-y,z+1/2

=> Initial parameters ==>

Atom	Ntyp	X	Y	Z	B	occ.	in	fin	Spc	Mult
B11	B22	B33	B12	B13	B23					
0(1)	0	0.56985	0.44154	0.26709	3.70830	1.00000	0	0	0	8
Codes:	81.00000	91.00000	101.00000	0.00000	0.00000					
0(2)	0	0.59912	0.23245	0.22393	4.41110	1.00000	0	0	0	8
Codes:	111.00000	121.00000	131.00000	0.00000	0.00000					
0(3)	0	0.47739	0.13249	-0.01670	4.98480	1.00000	0	0	0	8
Codes:	141.00000	151.00000	161.00000	0.00000	0.00000					
0(4)	0	0.34915	0.25989	-0.10972	4.76640	1.00000	0	0	0	8
Codes:	171.00000	181.00000	191.00000	0.00000	0.00000					
0(5)	0	0.30776	0.51770	-0.07890	5.32170	1.00000	0	0	0	8
Codes:	201.00000	211.00000	221.00000	0.00000	0.00000					
0(6)	0	0.42684	0.60012	0.05358	5.10850	1.00000	0	0	0	8
Codes:	231.00000	241.00000	251.00000	0.00000	0.00000					
N(1)	N	0.44586	0.33585	0.17311	2.73980	1.00000	0	0	0	8
Codes:	261.00000	271.00000	281.00000	0.00000	0.00000					
N(2)	N	0.32972	0.23290	0.05472	2.40240	1.00000	0	0	0	8
Codes:	291.00000	301.00000	311.00000	0.00000	0.00000					
N(3)	N	0.30485	0.45556	0.08268	2.59240	1.00000	0	0	0	8
Codes:	321.00000	331.00000	341.00000	0.00000	0.00000					
N(4)	N	0.53974	0.33264	0.23717	2.76530	1.00000	0	0	0	8
Codes:	351.00000	361.00000	371.00000	0.00000	0.00000					
N(5)	N	0.38533	0.20298	-0.04227	3.09700	1.00000	0	0	0	8
Codes:	381.00000	391.00000	401.00000	0.00000	0.00000					
N(6)	N	0.35655	0.54262	0.01049	3.43200	1.00000	0	0	0	8
Codes:	411.00000	421.00000	431.00000	0.00000	0.00000					
C(1)	C	0.34605	0.43642	0.19790	2.89510	1.00000	0	0	0	8
Codes:	441.00000	451.00000	461.00000	0.00000	0.00000					
C(2)	C	0.38722	0.21280	0.15754	2.70030	1.00000	0	0	0	8
Codes:	471.00000	481.00000	491.00000	0.00000	0.00000					
C(3)	C	0.23515	0.33775	0.05249	2.55740	1.00000	0	0	0	8

```

Codes: 501.00000 511.00000 521.00000 0.00000 0.00000
H(1A) H 0.40289 0.52403 0.20773 5.13220 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(1B) H 0.29071 0.42024 0.23991 4.84270 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(2A) H 0.44331 0.13918 0.14950 4.60580 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000
H(2B) H 0.31742 0.19390 0.20730 4.97430 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(3A) H 0.20936 0.35364 -0.02527 4.50050 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(3B) H 0.17213 0.32091 0.10070 3.92150 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000

```

=> IT IS ASSUMED THAT THE FIRST GIVEN SITE IS FULLY OCCUPIED
OR THE FIRST AND SECOND ATOMS ARE IN THE SAME SITE WITH TOTAL FULL OCCUPATION
(If this is not the case, change the order of atoms to obtain correct values for the content of the unit cell)
The given occupation factors have been obtained multiplying m/M by 1.0000

```

-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
=> The given value of ATZ is 1776.94 the program has calculated: 1776.94
The value of ATZ given in the input PCR file will be used for quantitative analysis
=> The chemical content of the unit cell is:
8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N +
8.0000 C + 8.0000 C + 8.0000 C + 8.0000 H + 8.0000 H +
8.0000 H + 8.0000 H + 8.0000 H +
8.0000 H
=> The normalized site occupation numbers in % are:
100.0000 O(1) : 100.0000 O(2) : 100.0000 O(3) : 100.0000 O(4) : 100.0000 O(5) :
100.0000 O(6) : 100.0000 N(1) : 100.0000 N(2) : 100.0000 N(3) : 100.0000 N(4) :
100.0000 N(5) : 100.0000 N(6) : 100.0000 C(1) : 100.0000 C(2) : 100.0000 C(3) :
100.0000 H(1A) : 100.0000 H(1B) : 100.0000 H(2A) : 100.0000 H(2B) : 100.0000 H(3A) :
100.0000 H(3B)

```

=> The density (volumic mass) of the compound is: 1.818 g/cm3

=>-----> PROFILE PARAMETERS FOR PATTERN: 1

```

=> Overall scale factor: 0.366470E-02
=> ETA (p-Voigt) OR M (Pearson VII): 0.0000
=> Overall temperature factor: 0.00000
=> Halfwidth U,V,W: -0.01481 0.00000 0.00000
=> X and Y parameters: 0.0000 0.0000
=> Direct cell parameters: 11.5606 10.6800 13.1449 90.0000 90.0000 90.0000
=> Preferred orientation parameters: 1.0000 0.0000
=> Asymmetry parameters : 0.20251 0.04985 0.00000 0.00000
=> Strain parameters : 0.00000 0.00000 0.00000
=> Size parameters : 0.01453 0.00000
=> Further shape parameters (S_L and D_L): 0.00000 0.00000
S_L is source width/detector distance
D_L is detector width/detector distance

```

==> CODEWORDS FOR PROFILE PARAMETERS of PATTERN# 1

```

=> Overall scale factor: 31.000
=> ETA (p-Voigt) OR M (Pearson VII): 0.000
=> Overall temperature factor: 0.000
=> Halfwidth U,V,W: 41.000 0.000 0.000
=> X and Y parameters: 0.000 0.000
=> Direct cell parameters: 51.000 61.000 71.000 0.000 0.000 0.000
=> Preferred orientation parameters: 0.000 0.000
=> Asymmetry parameters : 531.000 541.000 0.000 0.000
=> Strain parameters : 0.000 0.000 0.000
=> Size parameters : 11.000 551.000
=> The 18th model for size is used

```

=> Orthorhombic Anisotropic Broadening using Spherical Harmonics up
to 4-th order (Laue class: mmm, SPG:16-74, only lorentzian comp.)
Ylm's up to 4th order: Y00,Y20,Y22+,Y40,Y42+,Y44+
RJP - Ref: M. Jarvinen, J. Appl. C. (1993),p.527
=> Coefficients of Spherical Harmonics for anisotropic size

```

broadening for an orthorhombic lattice
Y00      Y20      Y22+      Y40      Y42+      Y44+
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
551.0000 561.0000 571.0000 581.0000 591.0000 601.0000

=> Cell constraints according to Laue symmetry: mmm

Metric information:
-----

=> Direct cell parameters:

a =      11.5606      b =      10.6800      c =      13.1449
alpha =      90.000      beta =      90.000      gamma =      90.000
Direct Cell Volume =      1622.9507

=> Reciprocal cell parameters:

a**=      0.086501      b**=      0.093633      c**=      0.076075
alpha**=      90.000      beta**=      90.000      gamma**=      90.000
Reciprocal Cell Volume =      0.00061616

=> Direct and Reciprocal Metric Tensors:

GD                      GR
133.6470      0.0000      0.0000      0.007482      0.000000      0.000000
0.0000      114.0614      0.0000      0.000000      0.008767      0.000000
0.0000      0.0000      172.7877      0.000000      0.000000      0.005787

=> Cartesian frame: x // a; y is in the ab-plane; z is x ^ y

Crystal_to_Orthonormal_Matrix      Orthonormal_to_Crystal Matrix
Cr_Orth_cel      Orth_Cr_cel
11.5606      0.0000      0.0000      0.086501      0.000000      0.000000
0.0000      10.6800      0.0000      0.000000      0.093633      0.000000
0.0000      0.0000      13.1449      0.000000      0.000000      0.076075

Busing-Levy B-matrix: Hc=B.H      Inverse of the Busing-Levy B-matrix
BL_M      BL_Minv
0.086501      0.000000      0.000000      11.5606      0.0000      0.0000
0.000000      0.093633      0.000000      0.0000      10.6800      0.0000
0.000000      0.000000      0.076075      0.0000      0.0000      13.1449

=> Laue symmetry mmm will be used to generate HKL for pattern# 1
=> Reflections generated between S(1/d)min: 0.1129 A-1 and S(1/d)max: 0.5976 A-1
=> dmmax: 8.8599 A and dmin: 1.6733 A
=> The number of reflections generated is: 183
=> The max. scatt. variable (gen.ref.) is: 54.8173
=> Scattering coefficients from internal table

=> X-ray scattering coeff. (A1, B1, A2,...C, f(0), Z, Dfp,Dfpp)

O      3.0485 13.2771 2.2868 5.7011 1.5463 0.3239 0.8670 32.9089 0.2508 7.9994 8.0000 0.0470 ↵
0.0320
N      12.2126 0.0057 3.1322 9.8933 2.0125 28.9975 1.1663 0.5826 -11.5290 6.9946 7.0000 0.0290 ↵
0.0180
C      2.3100 20.8439 1.0200 10.2075 1.5886 0.5687 0.8650 51.6512 0.2156 5.9992 6.0000 0.0170 ↵
0.0090
H      0.4930 10.5109 0.3229 26.1257 0.1402 3.1424 0.0408 57.7997 0.0030 1.0000 1.0000 0.0000 ↵
0.0000

-----
SYMBOLIC NAMES AND INITIAL VALUES OF PARAMETERS TO BE VARIED:
-----

-> Parameter number 1 -> Symbolic Name: G-Size_ph1_pat1 0.14526000E-01
-> Parameter number 2 -> Symbolic Name: Zero_pat1 -0.20156001
-> Parameter number 3 -> Symbolic Name: Scale_ph1_pat1 0.36647001E-02
-> Parameter number 4 -> Symbolic Name: U-Cagl_ph1_pat1 -0.14806000E-01
-> Parameter number 5 -> Symbolic Name: Cell_A_ph1_pat1 11.560578
-> Parameter number 6 -> Symbolic Name: Cell_B_ph1_pat1 10.679955
-> Parameter number 7 -> Symbolic Name: Cell_C_ph1_pat1 13.144872
-> Parameter number 8 -> Symbolic Name: X_0(1)_ph1 0.56985003
-> Parameter number 9 -> Symbolic Name: Y_0(1)_ph1 0.44154000
-> Parameter number 10 -> Symbolic Name: Z_0(1)_ph1 0.26708999
-> Parameter number 11 -> Symbolic Name: X_0(2)_ph1 0.59912002
-> Parameter number 12 -> Symbolic Name: Y_0(2)_ph1 0.23244999
-> Parameter number 13 -> Symbolic Name: Z_0(2)_ph1 0.22393000
-> Parameter number 14 -> Symbolic Name: X_0(3)_ph1 0.47738999
-> Parameter number 15 -> Symbolic Name: Y_0(3)_ph1 0.13248999
-> Parameter number 16 -> Symbolic Name: Z_0(3)_ph1 -0.16700000E-01
-> Parameter number 17 -> Symbolic Name: X_0(4)_ph1 0.34915000
-> Parameter number 18 -> Symbolic Name: Y_0(4)_ph1 0.25988999
-> Parameter number 19 -> Symbolic Name: Z_0(4)_ph1 -0.10972000
-> Parameter number 20 -> Symbolic Name: X_0(5)_ph1 0.30776000
-> Parameter number 21 -> Symbolic Name: Y_0(5)_ph1 0.51770002
-> Parameter number 22 -> Symbolic Name: Z_0(5)_ph1 -0.78900002E-01
-> Parameter number 23 -> Symbolic Name: X_0(6)_ph1 0.42684001
-> Parameter number 24 -> Symbolic Name: Y_0(6)_ph1 0.60012001

```

-> Parameter number	25	-> Symbolic Name:	Z_0(6)_ph1	0.53580001E-01
-> Parameter number	26	-> Symbolic Name:	X_N(1)_ph1	0.44586000
-> Parameter number	27	-> Symbolic Name:	Y_N(1)_ph1	0.33585000
-> Parameter number	28	-> Symbolic Name:	Z_N(1)_ph1	0.17310999
-> Parameter number	29	-> Symbolic Name:	X_N(2)_ph1	0.32971999
-> Parameter number	30	-> Symbolic Name:	Y_N(2)_ph1	0.23289999
-> Parameter number	31	-> Symbolic Name:	Z_N(2)_ph1	0.54719999E-01
-> Parameter number	32	-> Symbolic Name:	X_N(3)_ph1	0.30485001
-> Parameter number	33	-> Symbolic Name:	Y_N(3)_ph1	0.45556000
-> Parameter number	34	-> Symbolic Name:	Z_N(3)_ph1	0.82680002E-01
-> Parameter number	35	-> Symbolic Name:	X_N(4)_ph1	0.53974003
-> Parameter number	36	-> Symbolic Name:	Y_N(4)_ph1	0.33263999
-> Parameter number	37	-> Symbolic Name:	Z_N(4)_ph1	0.23717000
-> Parameter number	38	-> Symbolic Name:	X_N(5)_ph1	0.38532999
-> Parameter number	39	-> Symbolic Name:	Y_N(5)_ph1	0.20298000
-> Parameter number	40	-> Symbolic Name:	Z_N(5)_ph1	-0.42270001E-01
-> Parameter number	41	-> Symbolic Name:	X_N(6)_ph1	0.35655001
-> Parameter number	42	-> Symbolic Name:	Y_N(6)_ph1	0.54262000
-> Parameter number	43	-> Symbolic Name:	Z_N(6)_ph1	0.10490000E-01
-> Parameter number	44	-> Symbolic Name:	X_C(1)_ph1	0.34604999
-> Parameter number	45	-> Symbolic Name:	Y_C(1)_ph1	0.43641999
-> Parameter number	46	-> Symbolic Name:	Z_C(1)_ph1	0.19790000
-> Parameter number	47	-> Symbolic Name:	X_C(2)_ph1	0.38722000
-> Parameter number	48	-> Symbolic Name:	Y_C(2)_ph1	0.21280000
-> Parameter number	49	-> Symbolic Name:	Z_C(2)_ph1	0.15753999
-> Parameter number	50	-> Symbolic Name:	X_C(3)_ph1	0.23514999
-> Parameter number	51	-> Symbolic Name:	Y_C(3)_ph1	0.33774999
-> Parameter number	52	-> Symbolic Name:	Z_C(3)_ph1	0.52490000E-01
-> Parameter number	53	-> Symbolic Name:	Asym1_ph1_pat1	0.20251000
-> Parameter number	54	-> Symbolic Name:	Asym2_ph1_pat1	0.49849998E-01
-> Parameter number	55	-> Symbolic Name:	L-Size_ph1_pat1	0.00000000
-> Parameter number	56	-> Symbolic Name:	Size2_ph1_pat1	0.00000000
-> Parameter number	57	-> Symbolic Name:	Size3_ph1_pat1	0.00000000
-> Parameter number	58	-> Symbolic Name:	Size4_ph1_pat1	0.00000000
-> Parameter number	59	-> Symbolic Name:	Size5_ph1_pat1	0.00000000
-> Parameter number	60	-> Symbolic Name:	Size6_ph1_pat1	0.00000000

=> Zero counts at step no.	1	at 2theta/TOF/E(KeV):	10.0000	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	3	at 2theta/TOF/E(KeV):	10.0074	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	4	at 2theta/TOF/E(KeV):	10.0111	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	5	at 2theta/TOF/E(KeV):	10.0148	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	8	at 2theta/TOF/E(KeV):	10.0259	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	10	at 2theta/TOF/E(KeV):	10.0333	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	11	at 2theta/TOF/E(KeV):	10.0370	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	12	at 2theta/TOF/E(KeV):	10.0407	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	14	at 2theta/TOF/E(KeV):	10.0481	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	16	at 2theta/TOF/E(KeV):	10.0555	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	21	at 2theta/TOF/E(KeV):	10.0740	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	23	at 2theta/TOF/E(KeV):	10.0814	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	24	at 2theta/TOF/E(KeV):	10.0851	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	28	at 2theta/TOF/E(KeV):	10.0999	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	31	at 2theta/TOF/E(KeV):	10.1110	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	36	at 2theta/TOF/E(KeV):	10.1295	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	38	at 2theta/TOF/E(KeV):	10.1369	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	41	at 2theta/TOF/E(KeV):	10.1480	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	42	at 2theta/TOF/E(KeV):	10.1517	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	47	at 2theta/TOF/E(KeV):	10.1702	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	50	at 2theta/TOF/E(KeV):	10.1813	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	60	at 2theta/TOF/E(KeV):	10.2183	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	61	at 2theta/TOF/E(KeV):	10.2220	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	64	at 2theta/TOF/E(KeV):	10.2331	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	77	at 2theta/TOF/E(KeV):	10.2812	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	78	at 2theta/TOF/E(KeV):	10.2849	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	84	at 2theta/TOF/E(KeV):	10.3071	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	92	at 2theta/TOF/E(KeV):	10.3367	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	93	at 2theta/TOF/E(KeV):	10.3404	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	94	at 2theta/TOF/E(KeV):	10.3441	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	97	at 2theta/TOF/E(KeV):	10.3552	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	101	at 2theta/TOF/E(KeV):	10.3700	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	104	at 2theta/TOF/E(KeV):	10.3811	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	105	at 2theta/TOF/E(KeV):	10.3848	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	107	at 2theta/TOF/E(KeV):	10.3922	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	116	at 2theta/TOF/E(KeV):	10.4255	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	118	at 2theta/TOF/E(KeV):	10.4329	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	119	at 2theta/TOF/E(KeV):	10.4366	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	122	at 2theta/TOF/E(KeV):	10.4477	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	126	at 2theta/TOF/E(KeV):	10.4625	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	130	at 2theta/TOF/E(KeV):	10.4773	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	132	at 2theta/TOF/E(KeV):	10.4847	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	144	at 2theta/TOF/E(KeV):	10.5291	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	148	at 2theta/TOF/E(KeV):	10.5439	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	155	at 2theta/TOF/E(KeV):	10.5698	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	168	at 2theta/TOF/E(KeV):	10.6179	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	176	at 2theta/TOF/E(KeV):	10.6475	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	180	at 2theta/TOF/E(KeV):	10.6623	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	182	at 2theta/TOF/E(KeV):	10.6697	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	185	at 2theta/TOF/E(KeV):	10.6808	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	198	at 2theta/TOF/E(KeV):	10.7289	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	200	at 2theta/TOF/E(KeV):	10.7363	Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no.	204	at 2theta/TOF/E(KeV):	10.7511	Intensity fixed to 1.0 and variance to 1E6


```

O(4)      0.34889-0.00020 0.00060 0.25899 0.00047 0.00067 -0.11069 0.00089 0.00058 4.76640 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
O(5)      0.30778-0.00041 0.00055 0.51705 0.00000 0.00064 -0.07906 0.00024 0.00050 5.32170 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
O(6)      0.42722 0.00009 0.00051 0.60061 0.00022 0.00075 0.05273 0.00019 0.00053 5.10850 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(1)      0.44409-0.00072 0.00076 0.33100 0.00024 0.00099 0.17287-0.00033 0.00062 2.73980 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(2)      0.32742 0.00057 0.00094 0.23491 0.00001 0.00089 0.05328 0.00024 0.00072 2.40240 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(3)      0.30725 0.00026 0.00086 0.45634 0.00035 0.00082 0.08289 0.00044 0.00067 2.59240 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(4)      0.53933-0.00008 0.00068 0.33542 0.00005 0.00070 0.23515-0.00027 0.00068 2.76530 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(5)      0.38598-0.00021 0.00079 0.20331-0.00051 0.00092 -0.04141-0.00031 0.00080 3.09700 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(6)      0.35495 0.00025 0.00069 0.54361-0.00009 0.00092 0.00991-0.00094 0.00079 3.43200 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
C(1)      0.34679-0.00010 0.00085 0.43854 0.00078 0.00093 0.19868 0.00007 0.00074 2.89510 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
C(2)      0.38559-0.00021 0.00087 0.21305-0.00041 0.00094 0.15540 0.00145 0.00097 2.70030 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
C(3)      0.23576 0.00017 0.00071 0.34062-0.00031 0.00131 0.05232-0.00037 0.00063 2.55740 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(1A)     0.40289 0.00000 0.00000 0.52403 0.00000 0.00000 0.20773 0.00000 0.00000 5.13220 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(1B)     0.29071 0.00000 0.00000 0.42024 0.00000 0.00000 0.23991 0.00000 0.00000 4.84270 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(2A)     0.44331 0.00000 0.00000 0.13918 0.00000 0.00000 0.14950 0.00000 0.00000 4.60580 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(2B)     0.31742 0.00000 0.00000 0.19390 0.00000 0.00000 0.20730 0.00000 0.00000 4.97430 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(3A)     0.20936 0.00000 0.00000 0.35364 0.00000 0.00000 -0.02527 0.00000 0.00000 4.50050 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(3B)     0.17213 0.00000 0.00000 0.32091 0.00000 0.00000 0.10070 0.00000 0.00000 3.92150 0.00000 0.00000 ↵
1.00000 0.00000 0.00000

```

==> PROFILE PARAMETERS FOR PATTERN# 1

=> Overall scale factor: 0.003677659 -0.000000780 0.000011493

=> Eta(p-Voigt) or m(Pearson VII): 0.000000 0.000000 0.000000

=> Overall tem. factor: 0.000000 0.000000 0.000000

=> Halfwidth parameters:

0.014150 0.000261 0.003446

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

=> Cell parameters:

11.557671 0.000021 0.000273

10.676690 0.000017 0.000281

13.141932 0.000026 0.000305

90.000000 0.000000 0.000000

90.000000 0.000000 0.000000

90.000000 0.000000 0.000000

=> Preferred orientation:

1.000000 0.000000 0.000000

0.000000 0.000000 0.000000

=> Asymmetry parameters:

0.165592 -0.000072 0.008782

0.053462 -0.000027 0.001781

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

=> X and Y parameters:

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

=> Strain parameters:

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

=> Size parameters (G,L):

0.012007 -0.000010 0.000086

-0.025048 0.000745 0.004665

=> Further shape parameters (S_L and D_L):

0.000000 0.000000 0.000000

0.000000 0.000000 0.000000

=> Spherical Harmonics coeff.(size):

-0.025048 0.000745 0.004665 0.019418 -0.001630 0.013391 0.197667 0.002007 ↵

0.010955 0.000007 0.013803 -0.039622 -0.001868 0.013335 0.019753 0.000117 ↵

0.011426 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 ↵

0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 ↵

0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 ↵

==> GLOBAL PARAMETERS FOR PATTERN# 1

=> Zero-point: -0.2154 0.0001 0.0022

=> Background Polynomial Parameters ==>

0.11847E+06 0.0000 0.0000

```

0.72376E+06  0.0000  0.0000
-47087.      0.0000  0.0000
-0.18536E+07 0.0000  0.0000
-0.14029E+07 0.0000  0.0000
-35943.     0.0000  0.0000

=> Cos(theta)-shift parameter :  0.0000  0.0000  0.0000
=> Sin(2theta)-shift parameter :  0.0000  0.0000  0.0000

==> RELIABILITY FACTORS WITH ALL NON-EXCLUDED POINTS FOR PATTERN:  1

=> R-Factors:  14.1      23.3      Chi2:  263.      DW-Stat.:  0.3668  Patt#:  1
=> Expected :           1.44                      1.9515
=> Deviance :  0.530E+07  Dev*:  0.000
=> GoF-index:  16.      Sqrt(Residual/N)
=> N-P+C:  10751

=> SumYdif      SumYobs      SumYcal      SumWYobsSQ      Residual      Condition
0.7320E+07     0.5204E+08     0.4932E+08     0.5204E+08     0.2830E+07     0.9401E+11

=> Conventional Rietveld Rp,Rwp,Re and Chi2:  14.1      23.3      1.44      263.3
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2):  0.5204E+08     0.5204E+08

=> N-sigma of the GoF:  *****

==> RELIABILITY FACTORS FOR POINTS WITH BRAGG CONTRIBUTIONS FOR PATTERN:  1

=> R-Factors:  14.1      23.3      Chi2:  264.      DW-Stat.:  0.3676  Patt#:
=> Expected :           1.43                      1.9515
=> Deviance :  0.530E+07  Dev*:  NaN
=> GoF-index:  16.      Sqrt(Residual/N)
=> N-P+C:  10703

=> SumYdif      SumYobs      SumYcal      SumWYobsSQ      Residual      Condition
0.7314E+07     0.5204E+08     0.4932E+08     0.5203E+08     0.2825E+07     0.9401E+11

=> Conventional Rietveld Rp,Rwp,Re and Chi2:  14.1      23.3      1.43      263.9
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2):  0.5204E+08     0.5203E+08

=> N-sigma of the GoF:  19232.480

=> Global user-weighted Chi2 (Bragg contrib.):  264.

```

Pattern# 1 Phase No: 1 Phase name: rdx

No.	Code	H	K	L	Mult	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	✓
		d-hkl			CORR									
1	1	1	1	1	8	0.125905	13.135	7400.6	7435.7	37.146	0.125352	0.001030	0.011141	✓
	6.734526	599.986450												
2	1	0	0	2	2	0.135719	13.464	3914.7	4242.5	359.647	0.125367	0.019245	0.184427	✓
	6.570953	142.453094												
3	1	2	0	0	2	0.138997	15.320	432.2	496.0	73.923	0.125491	0.024955	0.230516	✓
	5.778825	109.673416												
4	1	1	0	2	4	0.130631	15.499	3895.5	3969.7	77.041	0.125506	0.009575	0.097605	✓
	5.712286	214.182709												
5	1	0	2	0	2	0.125689	16.593	2391.2	2407.5	16.614	0.125610	0.000147	0.001592	✓
	5.338336	93.177208												
6	1	2	1	0	4	0.135834	17.435	6610.1	6821.9	220.092	0.125705	0.018840	0.180585	✓
	5.082146	168.343307												
7	1	1	1	2	8	0.128285	17.594	890.0	967.3	84.113	0.125724	0.004778	0.050219	✓
	5.036711	330.477875												
8	1	0	2	1	4	0.125765	17.920	9551.0	9544.6	8.160	0.125765	0.000000	0.000001	✓
	4.945864	159.142273												
9	1	2	1	1	8	0.133015	18.705	87.1	108.7	29.086	0.125870	0.013337	0.132278	✓
	4.740059	291.393860												
10	1	1	2	1	8	0.127286	19.506	72.3	65.2	11.936	0.125990	0.002413	0.025729	✓
	4.547022	267.251007												
11	1	2	0	2	4	0.131441	20.449	6928.3	7170.5	251.909	0.126144	0.009894	0.100171	✓
	4.339426	121.185120												
12	1	0	2	2	4	0.126957	21.428	478.9	532.6	59.672	0.126322	0.001181	0.012670	✓
	4.143332	109.990654												
13	1	2	1	2	8	0.131203	22.093	5415.9	5618.9	210.642	0.126453	0.008875	0.090252	✓
	4.020066	206.420044												
14	1	2	2	0	4	0.133632	22.657	1099.0	976.5	108.777	0.126570	0.013184	0.130233	✓
	3.921263	97.934937												
15	1	1	2	2	8	0.128155	22.781	185.1	182.9	2.276	0.126596	0.002904	0.030711	✓
	3.900279	193.656250												
16	1	1	1	3	8	0.133704	23.239	135.2	158.2	27.456	0.126696	0.013083	0.129202	✓
	3.824453	185.759048												
17	1	2	2	1	8	0.132625	23.658	894.3	1020.2	143.528	0.126791	0.010897	0.109076	✓
	3.757561	178.948746												
18	1	3	1	1	8	0.139661	25.476	7116.8	7401.6	295.258	0.127241	0.023010	0.212609	✓
	3.493464	153.183014												

107	1	1	5	2	8	0.144726	45.301	4.0	8.0	7.976	0.136340	0.015646	0.142244	✓
	2.000154		43.714397											
108	1	4	3	3	8	0.148983	45.385	48.2	133.9	237.399	0.136396	0.023351	0.202813	✓
	1.996637		43.527786											
109	1	1	2	6	8	0.152351	45.402	15.6	45.2	85.406	0.136407	0.029381	0.246491	✓
	1.995937		43.488667											
110	1	2	3	5	8	0.147379	45.653	110.4	290.6	472.772	0.136575	0.020099	0.177704	✓
	1.985559		42.952629											
111	1	2	5	1	8	0.146777	45.786	26.0	74.3	137.757	0.136666	0.018829	0.167624	✓
	1.980102		42.675720											
112	1	3	4	3	8	0.147295	46.239	2.5	3.3	0.968	0.136975	0.019213	0.170313	✓
	1.961735		41.732731											
113	1	4	4	0	4	0.151994	46.267	1084.3	1397.4	402.098	0.136994	0.027700	0.233777	✓
	1.960631		20.838533											
114	1	2	4	4	8	0.146202	46.530	7.1	19.9	35.734	0.137177	0.016829	0.151086	✓
	1.950139		41.143612											
115	1	4	4	1	8	0.152075	46.809	423.6	524.9	125.033	0.137371	0.027174	0.229487	✓
	1.939170		40.591351											
116	1	6	0	0	2	0.162899	47.141	3.2	13.1	40.673	0.137605	0.045561	0.347164	✓
	1.926275		9.985799											
117	1	5	3	1	8	0.156524	47.363	324.0	462.4	196.551	0.137763	0.034363	0.278069	✓
	1.917771		39.521759											
118	1	2	5	2	8	0.147731	47.411	87.0	110.0	29.080	0.137798	0.018504	0.163835	✓
	1.915934		39.433163											
119	1	4	1	5	8	0.151386	47.493	4.7	6.7	2.766	0.137856	0.025063	0.213579	✓
	1.912836		39.274673											
120	1	2	2	6	8	0.153063	47.509	1.8	2.7	1.322	0.137868	0.028056	0.235041	✓
	1.912226		39.244450											

No.	Code	H	K	L	Mult	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	✓
		d-hkl			CORR									
121	1	5	2	3	8	0.154413	47.590	13.1	26.9	28.187	0.137926	0.030357	0.250960	✓
	1.909163		39.094662											
122	1	3	0	6	4	0.153864	47.724	28.3	87.7	183.311	0.138023	0.029210	0.242893	✓
	1.904096		19.421478											
123	1	6	1	0	4	0.163132	47.950	72.1	175.1	248.695	0.138186	0.044986	0.342748	✓
	1.895669		19.215900											
124	1	1	5	3	8	0.146969	48.008	14.8	35.8	50.545	0.138229	0.016303	0.145807	✓
	1.893506		38.329342											
125	1	5	0	4	4	0.154006	48.089	29.1	81.0	144.198	0.138288	0.028994	0.241001	✓
	1.890512		19.089468											
126	1	4	4	2	8	0.152597	48.408	49.8	88.8	69.344	0.138523	0.026048	0.219824	✓
	1.878781		37.612156											
127	1	6	1	1	8	0.162876	48.478	68.6	104.1	53.305	0.138574	0.043908	0.335755	✓
	1.876250		37.487667											
128	1	3	1	6	8	0.154167	48.525	253.2	358.7	148.539	0.138609	0.028710	0.238558	✓
	1.874519		37.402283											
129	1	0	4	5	4	0.148898	48.573	16.2	22.8	9.296	0.138645	0.019095	0.167568	✓
	1.872800		18.661100											
130	1	5	1	4	8	0.154620	48.885	487.1	674.0	257.052	0.138878	0.029039	0.240460	✓
	1.861554		36.780247											
131	1	5	3	2	8	0.156642	48.949	185.4	249.5	85.774	0.138925	0.032542	0.264187	✓
	1.859300		36.674236											
132	1	3	3	5	8	0.150943	49.112	0.4	0.4	0.059	0.139048	0.022101	0.190128	✓
	1.853503		36.396729											
133	1	4	3	4	8	0.151822	49.138	8.6	9.3	0.712	0.139068	0.023665	0.201750	✓
	1.852572		36.352833											
134	1	3	5	1	8	0.151793	49.238	37.1	36.7	0.448	0.139144	0.023474	0.200252	✓
	1.849062		36.189026											
135	1	1	4	5	8	0.149623	49.248	0.8	0.8	0.013	0.139151	0.019497	0.170146	✓
	1.848687		36.168797											
136	1	6	0	2	4	0.162073	49.254	317.4	315.1	2.426	0.139156	0.041565	0.320818	✓
	1.848485		18.078987											
137	1	1	3	6	8	0.153527	49.453	489.8	438.0	45.944	0.139307	0.026315	0.220682	✓
	1.841518		35.827904											
138	1	4	2	5	8	0.153203	49.875	91.5	89.2	2.564	0.139632	0.025146	0.211847	✓
	1.826896		35.140564											
139	1	1	1	7	8	0.161109	49.907	72.2	71.7	0.776	0.139656	0.039063	0.304740	✓
	1.825828		35.089111											
140	1	3	4	4	8	0.150733	49.943	0.0	0.0	0.000	0.139684	0.020556	0.177695	✓
	1.824592		35.034904											
141	1	2	5	3	8	0.149882	50.031	211.6	217.3	5.734	0.139753	0.018869	0.164628	✓
	1.821587		34.896233											
142	1	6	1	2	8	0.162498	50.037	0.3	0.3	0.006	0.139757	0.041274	0.318004	✓
	1.821389		34.884033											

BRAGG R-Factors and weight fractions for Pattern # 1

=> Phase: 1 rdx
=> Bragg R-factor: 6.97 Vol: 1621.684(0.069) Fract(%): 100.00(0.44)
=> Rf-factor= 9.79 ATZ: 1776.939 Brindley: 1.0000

SYMBOLIC NAMES AND FINAL VALUES AND SIGMA OF REFINED PARAMETERS:

-> Parameter number 1 : G-Size_ph1_pat1 0.12007418E-01(+/- 0.85642365E-04)

```

-> Parameter number 2 : Zero_pat1 -0.21540712 ( +/- 0.21793407E-02 )
-> Parameter number 3 : Scale_ph1_pat1 0.36776587E-02( +/- 0.11493407E-04 )
-> Parameter number 4 : U-Cagl_ph1_pat1 0.14149698E-01( +/- 0.34455676E-02 )
-> Parameter number 5 : Cell_A_ph1_pat1 11.557671 ( +/- 0.27274666E-03 )
-> Parameter number 6 : Cell_B_ph1_pat1 10.676690 ( +/- 0.28143937E-03 )
-> Parameter number 7 : Cell_C_ph1_pat1 13.141932 ( +/- 0.30492945E-03 )
-> Parameter number 8 : X_0(1)_ph1 0.57030642 ( +/- 0.50944550E-03 )
-> Parameter number 9 : Y_0(1)_ph1 0.44054043 ( +/- 0.58024272E-03 )
-> Parameter number 10 : Z_0(1)_ph1 0.26806968 ( +/- 0.53565676E-03 )
-> Parameter number 11 : X_0(2)_ph1 0.59821874 ( +/- 0.59325760E-03 )
-> Parameter number 12 : Y_0(2)_ph1 0.23070036 ( +/- 0.58002409E-03 )
-> Parameter number 13 : Z_0(2)_ph1 0.22521888 ( +/- 0.52235578E-03 )
-> Parameter number 14 : X_0(3)_ph1 0.47699246 ( +/- 0.58257120E-03 )
-> Parameter number 15 : Y_0(3)_ph1 0.13119514 ( +/- 0.53428166E-03 )
-> Parameter number 16 : Z_0(3)_ph1 -0.16466578E-01( +/- 0.51274599E-03 )
-> Parameter number 17 : X_0(4)_ph1 0.34888738 ( +/- 0.59821649E-03 )
-> Parameter number 18 : Y_0(4)_ph1 0.25898808 ( +/- 0.66673080E-03 )
-> Parameter number 19 : Z_0(4)_ph1 -0.11068642 ( +/- 0.58052666E-03 )
-> Parameter number 20 : X_0(5)_ph1 0.30777898 ( +/- 0.54655079E-03 )
-> Parameter number 21 : Y_0(5)_ph1 0.51705146 ( +/- 0.63611532E-03 )
-> Parameter number 22 : Z_0(5)_ph1 -0.79056025E-01( +/- 0.50401402E-03 )
-> Parameter number 23 : X_0(6)_ph1 0.42721874 ( +/- 0.51176769E-03 )
-> Parameter number 24 : Y_0(6)_ph1 0.60060859 ( +/- 0.74724230E-03 )
-> Parameter number 25 : Z_0(6)_ph1 0.52727856E-01( +/- 0.53174264E-03 )
-> Parameter number 26 : X_N(1)_ph1 0.44408569 ( +/- 0.76306117E-03 )
-> Parameter number 27 : Y_N(1)_ph1 0.33099678 ( +/- 0.98512415E-03 )
-> Parameter number 28 : Z_N(1)_ph1 0.17287177 ( +/- 0.62338362E-03 )
-> Parameter number 29 : X_N(2)_ph1 0.32741672 ( +/- 0.94491179E-03 )
-> Parameter number 30 : Y_N(2)_ph1 0.23490509 ( +/- 0.88645355E-03 )
-> Parameter number 31 : Z_N(2)_ph1 0.53277619E-01( +/- 0.72490342E-03 )
-> Parameter number 32 : X_N(3)_ph1 0.30725399 ( +/- 0.85900084E-03 )
-> Parameter number 33 : Y_N(3)_ph1 0.45634460 ( +/- 0.81957324E-03 )
-> Parameter number 34 : Z_N(3)_ph1 0.82887992E-01( +/- 0.67181664E-03 )
-> Parameter number 35 : X_N(4)_ph1 0.53932601 ( +/- 0.68082550E-03 )
-> Parameter number 36 : Y_N(4)_ph1 0.33542445 ( +/- 0.69672387E-03 )
-> Parameter number 37 : Z_N(4)_ph1 0.23514608 ( +/- 0.67948614E-03 )
-> Parameter number 38 : X_N(5)_ph1 0.38598049 ( +/- 0.79134514E-03 )
-> Parameter number 39 : Y_N(5)_ph1 0.20331475 ( +/- 0.91921864E-03 )
-> Parameter number 40 : Z_N(5)_ph1 -0.41405533E-01( +/- 0.79785188E-03 )
-> Parameter number 41 : X_N(6)_ph1 0.35495391 ( +/- 0.68654644E-03 )
-> Parameter number 42 : Y_N(6)_ph1 0.54360700 ( +/- 0.92109625E-03 )
-> Parameter number 43 : Z_N(6)_ph1 0.99107744E-02( +/- 0.78920758E-03 )
-> Parameter number 44 : X_C(1)_ph1 0.34678712 ( +/- 0.84853295E-03 )
-> Parameter number 45 : Y_C(1)_ph1 0.43853557 ( +/- 0.93395612E-03 )
-> Parameter number 46 : Z_C(1)_ph1 0.19867958 ( +/- 0.73884765E-03 )
-> Parameter number 47 : X_C(2)_ph1 0.38558781 ( +/- 0.87032176E-03 )
-> Parameter number 48 : Y_C(2)_ph1 0.21305369 ( +/- 0.93864364E-03 )
-> Parameter number 49 : Z_C(2)_ph1 0.15540366 ( +/- 0.96520188E-03 )
-> Parameter number 50 : X_C(3)_ph1 0.23576419 ( +/- 0.71329746E-03 )
-> Parameter number 51 : Y_C(3)_ph1 0.34061772 ( +/- 0.13099160E-02 )
-> Parameter number 52 : Z_C(3)_ph1 0.52318119E-01( +/- 0.63173153E-03 )
-> Parameter number 53 : Asym1_ph1_pat1 0.16559245 ( +/- 0.87822555E-02 )
-> Parameter number 54 : Asym2_ph1_pat1 0.53462289E-01( +/- 0.17806906E-02 )
-> Parameter number 55 : L-Size_ph1_pat1 -0.25047939E-01( +/- 0.46645673E-02 )
-> Parameter number 56 : Size2_ph1_pat1 0.19417906E-01( +/- 0.13390562E-01 )
-> Parameter number 57 : Size3_ph1_pat1 0.19766724 ( +/- 0.10954754E-01 )
-> Parameter number 58 : Size4_ph1_pat1 0.21014285 ( +/- 0.13802625E-01 )
-> Parameter number 59 : Size5_ph1_pat1 -0.39622393E-01( +/- 0.13335176E-01 )
-> Parameter number 60 : Size6_ph1_pat1 0.19753376E-01( +/- 0.11426117E-01 )

```

```

-----
=> Number of bytes for floating point variables: 4
=> Dimensions of dynamic allocated arrays in this run of FullProf:
-----

```

```

=> Total approximate array memory (dynamic + static): 107719993 bytes

```

```

MaxPOINT= 60000 Max.num. of points(+int. Inten.)/diffraction pattern
MaxREFLT= 20000 Max.num. of reflections/diffraction pattern
MaxPARAM= 300 Max.num. of refinable parameters
MaxOVERL= 2096 Max.num. of overlapping reflections

```

```

-----
=> Number of bytes for floating point arrays: 4
=> Dimensions of fixed arrays in this release of FullProf:
-----

```

```

NPATT = 80 Max.num. of powder diffraction patterns
NATS = 830 Max.num. of atoms (all kind) in asymmetric unit
MPAR = 1800 Max.num. of non atomic parameters/phase
IEXCL = 30 Max.num. of excluded regions
IBACP = 277 Max.num. of background points for interpolation
NPHT = 16 Max.num. of phases
NMAGM = 8 Max.num. of rotation-matrices sets for magnetic structure
NBASIS = 12 Max.num. of basis functions associated to a single atom
NIREPS = 9 Max.num. of irreducible representations to be combined
N_EQ = 384 Max.num. of user-supplied symmetry operators/propagation vectors
NGL = 300 Max.num. of global parameters/diffraction pattern
N_LINC = 30 Max.num. of global linear restraints
NAT_P = 64 Max.num. of atomic parameters per atom

```

```

NCONST =      500 Max.num. of slack constraints per phase
N_SPE   =      16 Max.num. of different chemical species
N_FORM  =      60 Max.num. of scattering factor values in a table
NPR     =     150 Max.num. of points defining a numerical profile
INPR    =      25 Max.num. of different numerical peak shapes
NPRC    =     150 Max.num. of terms in the table for correcting intensities
NSOL    =      10 Max.num. of solutions to be stored in Montecarlo searches

```

```

CPU Time:   96.906 seconds
1.615 minutes

```

```
=> Run finished at:      Date: 15/06/2015   Time: 11:02:11.361
```

A.3 Sample of n-RDX processed pure at 3 wt% in acetone

```

*****
** PROGRAM FullProf.2k (Version 5.50 - Dec2014-ILL JRC) **
*****

```

```

M U L T I  -- P A T T E R N
Rietveld, Profile Matching & Integrated Intensity
Refinement of X-ray and/or Neutron Data

```

```
Date: 18/02/2015   Time: 13:16:26.953
```

```
=> PCR file code: 3b
=> DAT file code: 3b.dat          -> Relative contribution: 1.0000
```

```
==> CONDITIONS OF THIS RUN FOR PATTERN No.: 1
```

```
=> Global Refinement of X-ray powder diffraction data
=> Global Refinement of X-ray powder diffraction data
Flat plate with PSD
=> Title:RDX

```

```
=> Number of phases:      1
=> Number of excluded regions:      0
=> Number of scattering factors supplied:      0
=> March-Dollase model for preferred orientation
=> Conventional weights: w=1.0/Variance(yobs)
=> Asymmetry correction as in J.Appl.Cryst. 26,128(1993)
=> Background linearly interpolated between the      6 points given
=> The      5th default profile function was selected
=> Pseudo-Voigt function (ETA variable)
X-parameter correspond to: ETA=ETA0+X*2theta
pV(x)= ETA*L(x)+(1-ETA)*G(x)

```

```
==> INPUT/OUTPUT OPTIONS:
```

```
=> Generate file *.PRF for plot
=> Output Integrated Intensities
=> Generate new input file *.PCR

```

```
=> Data supplied in free format for pattern: 1
=> Plot pattern at each cycle
=> Wavelengths: 1.54056 1.54439
=> Alpha2/Alpha1 ratio: 0.5000
=> Cos(Monochromator angle)= 1.0000
=> Asymmetry correction for angles lower than 90.000 degrees
=> Absorption correction (AC), muR-eff = 0.0000 0.0000
=> Base of peaks: 2.0*HW* 20.00

```

```
=> Number of cycles: 50
=> Relaxation factors ==> for coordinates: 1.00
=> for anisotropic temperature factors: 1.00
=> for halfwidth/strain/size parameters: 1.00
=> for lattice constants and propagation vectors: 1.00
=> EPS-value for convergence: 0.0
=> Background ==>

```

Position	Intensity	
15.00	16.91	0.00
20.00	-27.69	0.00
25.00	30.87	0.00
30.00	13.02	0.00
35.00	-2.55	0.00
38.00	37.25	0.00

```
=> Instrumental Resolution read from file: xray-res.irf
=> Title of data: Approximate resolution function of a conventional X-ray diffractometer CuKalpha1,2

```

```
=> The resolution function is IRESOL: 1 for profile function # 5
Input resolution parameters:

```

U-inst	V-inst	W-inst	X-inst	Y-inst	Z-inst
0.00136	-0.00500	0.00391	0.06389	0.00008	0.00000
0.00136	-0.00500	0.00391	0.06389	0.00008	0.00000

```

=> Number of Least-Squares parameters varied:      5

=>----->
=>-----> PATTERN number:  1
=>----->
=> Global parameters and codes ==>
=> Zero-point:      -0.0410    0.0000
=> Displacement peak-shift parameter and code:  -0.10    0.00
=> Transparency peak-shift parameter and code:   0.26    0.00

=> Reading Intensity data =>>

==> Angular range, step and number of points:
2Thmin:      12.113000  2Thmax:      38.910702  Step:      0.024900  No. of points:  1077
-----
=> Phase No. 1
rdx
-----
=>-----> Pattern#  1
=> Crystal Structure Refinement
=> The 7th profile function was selected for phase no.  1
=> Preferred orientation vector:  0.0000  0.0000  1.0000

=>-----> Data for PHASE: 1
=> Number of atoms:  21
=> Number of distance constraints:  0
=> Number of angle constraints:  0

=> Symmetry information on space group: P b c a
-> The multiplicity of the general position is:  8
-> The space group is Centric (-1 at origin)
-> Lattice type P: { 000 }
-> Reduced set of symmetry operators:

No.  IT  Symmetry symbol  Rotation part  Associated Translation
1: ( 1)  1  --> ( x, y, z) + { 0.0000  0.0000  0.0000}
2: ( 4)  2 ( x, 0, 0) --> ( x,-y,-z) + { 0.5000  0.5000  0.0000}
3: ( 3)  2 ( 0, y, 0) --> (-x, y,-z) + { 0.0000  0.5000  0.5000}
4: ( 2)  2 ( 0, 0, z) --> (-x,-y, z) + { 0.5000  0.0000  0.5000}

Information on Space Group:
-----
=> Number of Space group:  61
=> Hermann-Mauguin Symbol: P b c a
=> Hall Symbol: -P 2ac 2ab
=> Table Setting Choice:
=> Setting Type: IT (Generated from Hermann-Mauguin symbol)
=> Crystal System: Orthorhombic
=> Laue Class: mmm
=> Point Group: mmm
=> Bravais Lattice: P
=> Lattice Symbol: oP
=> Reduced Number of S.O.:  4
=> General multiplicity:  8
=> Centrosymmetry: Centric (-1 at origin)
=> Generators (exc. -1&L):  2
=> Asymmetric unit:  0.000 <= x <=  0.500
0.000 <= y <=  0.500
0.000 <= z <=  0.500

=> List of S.O. without inversion and lattice centring translations
=> SYMM( 1): x,y,z          => SYMM( 2): x+1/2,-y+1/2,-z
=> SYMM( 3): -x,y+1/2,-z+1/2  => SYMM( 4): -x+1/2,-y,z+1/2

=> Initial parameters ==>
Atom  Ntyp      X      Y      Z      B      occ.      in  fin  Spc  Mult
B11   B22      B33      B12      B13      B23
O(1)  0          0.56846  0.43427  0.26465  3.70830  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
O(2)  0          0.59453  0.24040  0.23053  4.41110  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
O(3)  0          0.47340  0.13880  -0.02250  4.98480  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
O(4)  0          0.35580  0.24950  -0.11238  4.76640  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
O(5)  0          0.31810  0.53030  -0.06806  5.32170  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
O(6)  0          0.42860  0.60110  0.04920  5.10850  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
N(1)  N          0.43638  0.33385  0.17584  2.73980  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
N(2)  N          0.32231  0.23197  0.05389  2.40240  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
N(3)  N          0.29900  0.45348  0.08838  2.59240  1.00000  0  0  0  8
Codes: 0.00000  0.00000  0.00000  0.00000  0.00000  0.00000
N(4)  N          0.53777  0.33516  0.22628  2.76530  1.00000  0  0  0  8

```



```

Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
N(5) N 0.38834 0.20759 -0.03308 3.09700 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
N(6) N 0.35299 0.52971 0.01650 3.43200 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
C(1) C 0.35799 0.43950 0.18450 2.89510 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000
C(2) C 0.38140 0.21557 0.14950 2.70030 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
C(3) C 0.24458 0.33936 0.05038 2.55740 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(1A) H 0.40289 0.52403 0.20773 5.13220 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000
H(1B) H 0.29071 0.42024 0.23991 4.84270 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(2A) H 0.44331 0.13918 0.14950 4.60580 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(2B) H 0.31742 0.19390 0.20730 4.97430 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000
H(3A) H 0.20936 0.35364 -0.02527 4.50050 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(3B) H 0.17213 0.32091 0.10070 3.92150 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000

```

=> IT IS ASSUMED THAT THE FIRST GIVEN SITE IS FULLY OCCUPIED
OR THE FIRST AND SECOND ATOMS ARE IN THE SAME SITE WITH TOTAL FULL OCCUPATION
(If this is not the case, change the order of atoms to obtain correct values for the content of the unit cell)
The given occupation factors have been obtained multiplying m/M by 1.0000

```

-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080

```

=> The given value of ATZ is 1776.94 the program has calculated: 1776.94
The value of ATZ given in the input PCR file will be used for quantitative analysis

=> The chemical content of the unit cell is:

```

8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 C + 8.0000 C + 8.0000 C + 8.0000 H + 8.0000 H +
8.0000 H + 8.0000 H + 8.0000 H +
8.0000 H

```

=> The normalized site occupation numbers in % are:

```

100.0000 O(1) : 100.0000 O(2) : 100.0000 O(3) : 100.0000 O(4) : 100.0000 O(5) :
100.0000 O(6) : 100.0000 N(1) : 100.0000 N(2) : 100.0000 N(3) : 100.0000 N(4) :
100.0000 N(5) : 100.0000 N(6) : 100.0000 C(1) : 100.0000 C(2) : 100.0000 C(3) :
100.0000 H(1A) : 100.0000 H(1B) : 100.0000 H(2A) : 100.0000 H(2B) : 100.0000 H(3A) :
100.0000 H(3B)

```

=> The density (volumic mass) of the compound is: 1.785 g/cm3

=>-----> PROFILE PARAMETERS FOR PATTERN: 1

```

=> Overall scale factor: 0.666440E-03
=> ETA (p-Voigt) OR M (Pearson VII): 0.0000
=> Overall temperature factor: 0.00000
=> Halfwidth U,V,W: -0.00587 0.00000 0.00000
=> X and Y parameters: 0.0000 0.0000
=> Direct cell parameters: 11.6304 10.7431 13.2279 90.0000 90.0000 90.0000
=> Preferred orientation parameters: 1.0000 0.0000
=> Asymmetry parameters : -0.21721 0.00510 0.00000 0.00000
=> Strain parameters : 0.00000 0.00000 0.00000
=> Size parameters : 0.00000 0.00000
=> Further shape parameters (S_L and D_L): 0.00000 0.00000
S_L is source width/detector distance
D_L is detector width/detector distance

```

==> CODEWORDS FOR PROFILE PARAMETERS of PATTERN# 1

```

=> Overall scale factor: 11.000
=> ETA (p-Voigt) OR M (Pearson VII): 0.000
=> Overall temperature factor: 0.000
=> Halfwidth U,V,W: 21.000 0.000 0.000
=> X and Y parameters: 0.000 0.000
=> Direct cell parameters: 0.000 0.000 0.000 0.000 0.000 0.000
=> Preferred orientation parameters: 0.000 0.000

```

```
=> Asymmetry parameters      :   41.000  51.000  0.000  0.000
=> Strain parameters         :     0.000   0.000   0.000
=> Size parameters           :     31.000   0.000
```

```
=> Cell constraints according to Laue symmetry: mmm
```

```
Metric information:
```

```
=> Direct cell parameters:
```

```
a =      11.6304      b =      10.7431      c =      13.2279
alpha =     90.000    beta =     90.000    gamma =     90.000
Direct Cell Volume =    1652.7814
```

```
=> Reciprocal cell parameters:
```

```
a**=    0.085981    b**=    0.093083    c**=    0.075598
alpha**=  90.000    beta**=  90.000    gamma**=  90.000
Reciprocal Cell Volume =    0.00060504
```

```
=> Direct and Reciprocal Metric Tensors:
```

```
GD                                GR
135.2666      0.0000      0.0000      0.007393      0.000000      0.000000
0.0000      115.4133      0.0000      0.000000      0.008665      0.000000
0.0000      0.0000      174.9783      0.000000      0.000000      0.005715
```

```
=> Cartesian frame: x // a; y is in the ab-plane; z is x ^ y
```

```
Crystal_to_Orthonormal_Matrix      Orthonormal_to_Crystal Matrix
Cr_Orth_cel                          Orth_Cr_cel
11.6304      0.0000      0.0000      0.085981      0.000000      0.000000
0.0000      10.7431      0.0000      0.000000      0.093083      0.000000
0.0000      0.0000      13.2279      0.000000      0.000000      0.075598
```

```
Busing-Levy B-matrix: Hc=B.H          Inverse of the Busing-Levy B-matrix
BL_M                                    BL_Minv
0.085981      0.000000      0.000000      11.6304      0.0000      0.0000
0.000000      0.093083      0.000000      0.0000      10.7431      0.0000
0.000000      0.000000      0.075598      0.0000      0.0000      13.2279
```

```
=> Laue symmetry mmm will be used to generate HKL for pattern# 1
=> Reflections generated between S(1/d)min: 0.1366 A-1 and S(1/d)max: 0.4324 A-1
=> dmax: 7.3188 A and dmin: 2.3127 A
=> The number of reflections generated is: 69
=> The max. scatt. variable (gen.ref.) is: 38.9107
=> Scattering coefficients from internal table
```

```
=> X-ray scattering coeff. (A1, B1, A2,...C, f(0), Z, Dfp,Dfpp)
```

O	3.0485	13.2771	2.2868	5.7011	1.5463	0.3239	0.8670	32.9089	0.2508	7.9994	8.0000	0.0470	↗
	0.0320												
N	12.2126	0.0057	3.1322	9.8933	2.0125	28.9975	1.1663	0.5826	-11.5290	6.9946	7.0000	0.0290	↗
	0.0180												
C	2.3100	20.8439	1.0200	10.2075	1.5886	0.5687	0.8650	51.6512	0.2156	5.9992	6.0000	0.0170	↗
	0.0090												
H	0.4930	10.5109	0.3229	26.1257	0.1402	3.1424	0.0408	57.7997	0.0030	1.0000	1.0000	0.0000	↗
	0.0000												

```
-----
SYMBOLIC NAMES AND INITIAL VALUES OF PARAMETERS TO BE VARIED:
-----
```

```
-> Parameter number 1 -> Symbolic Name: Scale_phi_pat1 0.66644000E-03
-> Parameter number 2 -> Symbolic Name: U-Cagl_phi_pat1 -0.58700000E-02
-> Parameter number 3 -> Symbolic Name: G-Size_phi_pat1 0.00000000
-> Parameter number 4 -> Symbolic Name: Asym1_phi_pat1 -0.21720999
-> Parameter number 5 -> Symbolic Name: Asym2_phi_pat1 0.51000002E-02
```

```
=> Zero counts at step no. 3 at 2theta/TOF/E(KeV): 12.1628 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 4 at 2theta/TOF/E(KeV): 12.1877 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 5 at 2theta/TOF/E(KeV): 12.2126 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 6 at 2theta/TOF/E(KeV): 12.2375 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 9 at 2theta/TOF/E(KeV): 12.3122 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 10 at 2theta/TOF/E(KeV): 12.3371 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 11 at 2theta/TOF/E(KeV): 12.3620 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 14 at 2theta/TOF/E(KeV): 12.4367 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 15 at 2theta/TOF/E(KeV): 12.4616 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 22 at 2theta/TOF/E(KeV): 12.6359 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 61 at 2theta/TOF/E(KeV): 13.6070 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 62 at 2theta/TOF/E(KeV): 13.6319 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 69 at 2theta/TOF/E(KeV): 13.8062 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 77 at 2theta/TOF/E(KeV): 14.0054 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 79 at 2theta/TOF/E(KeV): 14.0552 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 81 at 2theta/TOF/E(KeV): 14.1050 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 86 at 2theta/TOF/E(KeV): 14.2295 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 87 at 2theta/TOF/E(KeV): 14.2544 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 93 at 2theta/TOF/E(KeV): 14.4038 Intensity fixed to 1.0 and variance to 1E6
```


=> Optimizations for routine tasks applied:
=> Calculation mode for patter#: 1 CM_PSEUDO_VOIGT

Standard deviations have to be multiplied by: 3.5344
(correlated residuals) See references:
-J.F.Berar & P.Lelann, J. Appl. Cryst. 24, 1-5 (1991)
-J.F.Berar, Acc. in Pow. Diff. II, NIST Sp.Pub. 846, 63(1992)

=====
=> CYCLE No.: 18
=> Convergence reached at this CYCLE !!!!
=> Parameter shifts set to zero

=> Phase 1 Name: rdx

=====
=> New parameters, shifts, and standard deviations

Atom	x docc.	dx socc.	sx	y	dy	sy	z	dz	sz	B	dB	sB	occ.
O(1)	0.56846	0.00000	0.00000	0.43427	0.00000	0.00000	0.26465	0.00000	0.00000	3.70830	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
O(2)	0.59453	0.00000	0.00000	0.24040	0.00000	0.00000	0.23053	0.00000	0.00000	4.41110	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
O(3)	0.47340	0.00000	0.00000	0.13880	0.00000	0.00000	-0.02250	0.00000	0.00000	4.98480	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
O(4)	0.35580	0.00000	0.00000	0.24950	0.00000	0.00000	-0.11238	0.00000	0.00000	4.76640	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
O(5)	0.31810	0.00000	0.00000	0.53030	0.00000	0.00000	-0.06806	0.00000	0.00000	5.32170	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
O(6)	0.42860	0.00000	0.00000	0.60110	0.00000	0.00000	0.04920	0.00000	0.00000	5.10850	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
N(1)	0.43638	0.00000	0.00000	0.33385	0.00000	0.00000	0.17584	0.00000	0.00000	2.73980	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
N(2)	0.32231	0.00000	0.00000	0.23197	0.00000	0.00000	0.05389	0.00000	0.00000	2.40240	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
N(3)	0.29900	0.00000	0.00000	0.45348	0.00000	0.00000	0.08838	0.00000	0.00000	2.59240	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
N(4)	0.53777	0.00000	0.00000	0.33516	0.00000	0.00000	0.22628	0.00000	0.00000	2.76530	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
N(5)	0.38834	0.00000	0.00000	0.20759	0.00000	0.00000	-0.03308	0.00000	0.00000	3.09700	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
N(6)	0.35299	0.00000	0.00000	0.52971	0.00000	0.00000	0.01650	0.00000	0.00000	3.43200	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
C(1)	0.35799	0.00000	0.00000	0.43950	0.00000	0.00000	0.18450	0.00000	0.00000	2.89510	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
C(2)	0.38140	0.00000	0.00000	0.21557	0.00000	0.00000	0.14950	0.00000	0.00000	2.70030	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
C(3)	0.24458	0.00000	0.00000	0.33936	0.00000	0.00000	0.05038	0.00000	0.00000	2.55740	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
H(1A)	0.40289	0.00000	0.00000	0.52403	0.00000	0.00000	0.20773	0.00000	0.00000	5.13220	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
H(1B)	0.29071	0.00000	0.00000	0.42024	0.00000	0.00000	0.23991	0.00000	0.00000	4.84270	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
H(2A)	0.44331	0.00000	0.00000	0.13918	0.00000	0.00000	0.14950	0.00000	0.00000	4.60580	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
H(2B)	0.31742	0.00000	0.00000	0.19390	0.00000	0.00000	0.20730	0.00000	0.00000	4.97430	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
H(3A)	0.20936	0.00000	0.00000	0.35364	0.00000	0.00000	-0.02527	0.00000	0.00000	4.50050	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
H(3B)	0.17213	0.00000	0.00000	0.32091	0.00000	0.00000	0.10070	0.00000	0.00000	3.92150	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										

==> PROFILE PARAMETERS FOR PATTERN# 1

=> Overall scale factor: 0.000451821 0.000000000 0.000003839
=> Eta(p-Voigt) or m(Pearson VII): 0.000000 0.000000 0.000000
=> Overall tem. factor: 0.000000 0.000000 0.000000
=> Halfwidth parameters:
-0.004847 0.000000 0.013262
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Cell parameters:
11.630419 0.000000 0.000000
10.743058 0.000000 0.000000
13.227938 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
=> Preferred orientation:
1.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Asymmetry parameters:
0.032918 0.000000 0.006054
0.042103 0.000000 0.003202

```

0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> X and Y parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Strain parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Size parameters (G,L):
0.010384 0.000000 0.000253
0.000000 0.000000 0.000000
=> Further shape parameters (S_L and D_L):
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

```

==> GLOBAL PARAMETERS FOR PATTERN# 1

```

=> Zero-point:      -0.0410    0.0000    0.0000
=> Cos(theta)-shift parameter :  -0.1020  0.0000  0.0000
=> Sin(2theta)-shift parameter :   0.2630  0.0000  0.0000

```

==> RELIABILITY FACTORS WITH ALL NON-EXCLUDED POINTS FOR PATTERN: 1

```

=> R-Factors:      20.1      26.6      Chi2:  68.3      DW-Stat.:  0.7185      Patt#:  1
=> Expected :           3.22                      1.8193
=> Deviance : 0.870E+05      Dev*:    81.04
=> GoF-index:   8.2          Sqrt(Residual/N)
=> N-P+C:    1072

```

```

=>      SumYdif      SumYobs      SumYcal      SumwYobsSQ      Residual      Condition
0.2080E+06    0.1034E+07    0.9677E+06    0.1034E+07    0.7325E+05    0.1251E+08

```

```

=> Conventional Rietveld Rp,Rwp,Re and Chi2:  20.3      26.8      3.24      68.33
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2):  0.1024E+07    0.1020E+07

```

=> N-sigma of the GoF: 1558.821

==> RELIABILITY FACTORS FOR POINTS WITH BRAGG CONTRIBUTIONS FOR PATTERN: 1

```

=> R-Factors:      20.1      26.6      Chi2:  68.3      DW-Stat.:  0.7185      Patt#:
=> Expected :           3.22                      1.8193
=> Deviance : 0.870E+05      Dev*:    81.04
=> GoF-index:   8.2          Sqrt(Residual/N)
=> N-P+C:    1072

```

```

=>      SumYdif      SumYobs      SumYcal      SumwYobsSQ      Residual      Condition
0.2080E+06    0.1034E+07    0.9677E+06    0.1034E+07    0.7325E+05    0.1251E+08

```

```

=> Conventional Rietveld Rp,Rwp,Re and Chi2:  20.3      26.8      3.24      68.33
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2):  0.1024E+07    0.1020E+07

```

=> N-sigma of the GoF: 1558.821

=> Global user-weighted Chi2 (Bragg contrib.): 68.3

Pattern# 1 Phase No: 1 Phase name: rdx

No.	Code	H d-hkl	K	L	Mult CORR	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	✓
1	1	1	1	1	8	0.121476	13.052	1251.5	994.7	209.519	0.117519	0.007393	0.081390	✓
		6.777159			607.424438									
2	1	0	0	2	2	0.121533	13.376	615.4	524.7	81.556	0.117477	0.007575	0.083321	✓
		6.613969			144.491653									
3	1	2	0	0	2	0.121864	15.223	83.3	51.4	26.997	0.117249	0.008622	0.094298	✓
		5.815209			111.037720									
4	1	1	0	2	4	0.121897	15.399	794.1	560.8	173.189	0.117228	0.008722	0.095336	✓
		5.749331			216.941605									
5	1	0	2	0	2	0.122102	16.489	378.8	358.2	27.066	0.117101	0.009342	0.101767	✓
		5.371529			94.315758									
6	1	2	1	0	4	0.122263	17.326	976.1	922.9	64.119	0.117007	0.009818	0.106679	✓
		5.114053			170.442551									
7	1	1	1	2	8	0.122294	17.481	128.0	136.4	9.973	0.116990	0.009907	0.107586	✓
		5.069075			334.714142									
8	1	0	2	1	4	0.122358	17.807	1572.9	1430.3	156.574	0.116955	0.010093	0.109498	✓
		4.976847			161.115646									
9	1	2	1	1	8	0.122514	18.586	23.0	13.8	34.306	0.116872	0.010539	0.114047	✓
		4.769984			295.069672									
10	1	1	2	1	8	0.122677	19.384	22.5	18.6	46.407	0.116789	0.010996	0.118687	✓
		4.575528			270.592194									
11	1	2	0	2	4	0.122872	20.318	980.1	1062.1	132.544	0.116696	0.011533	0.124103	✓

12	4.367220	122.753159										
	1 0	2 2 4	0.123082	21.291	68.1	86.2	33.725	0.116603	0.012094	0.129725	↔	
	4.169635	111.398773										
13	1 2	1 2 8	0.123227	21.952	775.6	843.0	85.375	0.116543	0.012476	0.133524	↔	
	4.045709	209.094452										
14	1 2	2 0 4	0.123352	22.515	144.3	135.0	23.581	0.116493	0.012802	0.136755	↔	
	3.945786	99.174377										
15	1 1	2 2 8	0.123379	22.635	39.2	34.2	6.470	0.116482	0.012872	0.137447	↔	
	3.925016	196.149139										
16	1 1	1 3 8	0.123482	23.087	27.2	20.6	9.583	0.116443	0.013134	0.140032	↔	
	3.849222	188.221832										
17	1 2	2 1 8	0.123579	23.509	148.2	155.7	46.760	0.116408	0.013379	0.142440	↔	
	3.781150	181.234940										
18	1 3	1 1 8	0.124006	25.314	902.6	1096.9	241.947	0.116265	0.014433	0.152701	↔	
	3.515492	155.173340										
19	1 0	2 3 4	0.124205	26.125	37.3	64.9	47.910	0.116206	0.014909	0.157288	↔	
	3.408129	72.593018										
20	1 2	2 2 8	0.124243	26.278	9.1	16.6	13.432	0.116195	0.014999	0.158154	↔	
	3.388580	143.401276										
21	1 3	0 2 4	0.124331	26.630	6.6	9.1	3.570	0.116170	0.015206	0.160138	↔	
	3.344589	69.711670										
22	1 2	1 3 8	0.124341	26.672	146.0	189.7	56.634	0.116167	0.015231	0.160373	↔	
	3.339449	138.961929										
23	1 1	3 1 8	0.124395	26.886	522.6	614.0	107.796	0.116153	0.015357	0.161577	↔	
	3.313359	136.631302										
24	1 0	0 4 2	0.124408	26.939	325.3	373.2	55.441	0.116149	0.015388	0.161874	↔	
	3.306984	34.016178										
25	1 1	2 3 8	0.124486	27.244	146.1	200.2	74.655	0.116129	0.015568	0.163591	↔	
	3.270598	132.851700										
26	1 3	1 2 8	0.124659	27.916	3.2	0.3	16.861	0.116086	0.015966	0.167359	↔	
	3.193409	126.155663										
27	1 1	0 4 4	0.124688	28.028	0.1	0.2	1.590	0.116079	0.016032	0.167986	↔	
	3.180897	62.542797										
28	1 3	2 1 8	0.124991	29.175	586.2	784.3	264.693	0.116011	0.016713	0.174392	↔	
	3.058400	114.835915										
29	1 1	1 4 8	0.125013	29.257	889.3	1121.2	292.295	0.116006	0.016762	0.174849	↔	
	3.050011	114.149055										
30	1 2	3 0 4	0.125015	29.265	451.7	568.8	147.410	0.116006	0.016767	0.174891	↔	
	3.049236	57.042862										
31	1 1	3 2 8	0.125041	29.359	3.1	4.2	1.385	0.116000	0.016823	0.175419	↔	
	3.039620	113.300980										
32	1 2	3 1 8	0.125229	30.050	0.6	0.2	4.321	0.115963	0.017235	0.179258	↔	
	2.971314	107.799812										
33	1 2	2 3 8	0.125318	30.374	402.2	432.9	37.902	0.115947	0.017429	0.181055	↔	
	2.940360	105.349037										
34	1 4	0 0 2	0.125415	30.724	184.3	205.1	23.261	0.115929	0.017639	0.182997	↔	
	2.907605	25.696112										
35	1 2	0 4 4	0.125517	31.085	253.8	305.4	61.928	0.115912	0.017856	0.184993	↔	
	2.874666	50.117661										
36	1 3	2 2 8	0.125629	31.483	56.1	69.9	17.217	0.115893	0.018095	0.187192	↔	
	2.839199	97.524094										
37	1 0	2 4 4	0.125705	31.749	6.4	7.4	1.141	0.115882	0.018255	0.188655	↔	
	2.816087	47.887966										
38	1 3	1 3 8	0.125725	31.818	61.1	76.2	18.666	0.115879	0.018297	0.189037	↔	
	2.810112	95.326462										
39	1 4	1 0 4	0.125737	31.859	134.1	171.3	47.391	0.115877	0.018321	0.189260	↔	
	2.806627	47.532345										
40	1 2	1 4 8	0.125838	32.208	431.3	549.7	150.424	0.115862	0.018532	0.191184	↔	
	2.776968	92.850838										
41	1 2	3 2 8	0.125865	32.302	465.1	587.6	154.278	0.115858	0.018589	0.191699	↔	
	2.769119	92.268997										
42	1 4	1 1 8	0.125948	32.587	48.8	55.6	7.746	0.115847	0.018762	0.193268	↔	
	2.745508	90.529259										
43	1 1	2 4 8	0.125979	32.691	36.1	43.5	8.932	0.115843	0.018825	0.193840	↔	
	2.736998	89.905861										
44	1 1	3 3 8	0.126102	33.107	290.6	312.4	24.459	0.115827	0.019077	0.196118	↔	
	2.703608	87.479691										
45	1 0	4 0 2	0.126169	33.333	63.6	77.5	17.300	0.115819	0.019214	0.197357	↔	
	2.685765	21.548969										
46	1 4	0 2 4	0.126262	33.643	6.6	5.4	19.513	0.115808	0.019403	0.199051	↔	
	2.661751	42.241043										
47	1 0	4 1 4	0.126380	34.034	45.1	56.9	27.961	0.115795	0.019641	0.201187	↔	
	2.632060	41.192669										
48	1 4	1 2 8	0.126582	34.692	66.2	78.5	15.767	0.115775	0.020043	0.204774	↔	
	2.583631	79.018021										
49	1 3	3 1 8	0.126597	34.742	306.6	360.7	66.180	0.115774	0.020074	0.205047	↔	
	2.580004	78.768509										
50	1 1	4 1 8	0.126653	34.922	0.0	0.0	0.002	0.115769	0.020184	0.206025	↔	
	2.567142	77.886520										
51	1 3	2 3 8	0.126686	35.027	280.9	388.9	149.247	0.115766	0.020248	0.206597	↔	
	2.559662	77.375694										
52	1 4	2 0 4	0.126698	35.064	41.3	57.5	22.622	0.115765	0.020271	0.206800	↔	
	2.557027	38.598064										
53	1 2	2 4 8	0.126798	35.386	0.0	0.0	0.038	0.115757	0.020468	0.208545	↔	
	2.534537	75.671524										
54	1 3	0 4 4	0.126884	35.655	86.7	101.1	20.860	0.115750	0.020634	0.210009	↔	
	2.515971	37.211742										
55	1 4	2 1 8	0.126909	35.735	20.1	23.9	5.495	0.115748	0.020683	0.210440	↔	
	2.510551	74.061028										
56	1 1	1 5 8	0.126919	35.767	0.1	0.2	0.035	0.115748	0.020703	0.210613	↔	

No.	Code	H d-hkl	K	L	Mult CORR	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	↗
57	1	2	3	3	8	0.126921	35.773	5.5	6.3	1.378	0.115747	0.020707	0.210647	↗
	2.507954													
58	1	0	4	2	4	0.127014	36.064	0.1	0.0	2.150	0.115741	0.020886	0.212219	↗
	2.488423													
59	1	3	1	4	8	0.127204	36.654	30.6	34.8	7.231	0.115730	0.021251	0.215410	↗
	2.449688													
60	1	3	3	2	8	0.127232	36.738	106.4	126.2	26.614	0.115728	0.021303	0.215862	↗
	2.444295													

BRAGG R-Factors and weight fractions for Pattern # 1

=> Phase: 1 rdx
=> Bragg R-factor: 17.2 Vol: 1652.781(0.000) Fract(%): 100.00(1.20)
=> Rf-factor= 9.62 ATZ: 1776.939 Brindley: 1.0000

SYMBOLIC NAMES AND FINAL VALUES AND SIGMA OF REFINED PARAMETERS:

-> Parameter number 1 : Scale_ph1_pat1 0.45182102E-03(+/- 0.38391618E-05)
-> Parameter number 2 : U-Cagl_ph1_pat1 -0.48470786E-02(+/- 0.13262363E-01)
-> Parameter number 3 : G-Size_ph1_pat1 0.10384443E-01(+/- 0.25276333E-03)
-> Parameter number 4 : Asym1_ph1_pat1 0.32917723E-01(+/- 0.60544414E-02)
-> Parameter number 5 : Asym2_ph1_pat1 0.42102702E-01(+/- 0.32015643E-02)

=> Number of bytes for floating point variables: 4
=> Dimensions of dynamic allocated arrays in this run of FullProf:

=> Total approximate array memory (dynamic + static): 10771993 bytes

MaxPOINT= 60000 Max.num. of points(+int. Inten.)/diffraction pattern
MaxREFLT= 20000 Max.num. of reflections/diffraction pattern
MaxPARAM= 300 Max.num. of refinable parameters
MaxOVERL= 2096 Max.num. of overlapping reflections

=> Number of bytes for floating point arrays: 4
=> Dimensions of fixed arrays in this release of FullProf:

NPATT = 80 Max.num. of powder diffraction patterns
NATS = 830 Max.num. of atoms (all kind) in asymmetric unit
MPAR = 1800 Max.num. of non atomic parameters/phase
IEXCL = 30 Max.num. of excluded regions
IBACP = 277 Max.num. of background points for interpolation
NPHT = 16 Max.num. of phases
NMAGM = 8 Max.num. of rotation-matrices sets for magnetic structure
NBASIS = 12 Max.num. of basis functions associated to a single atom
NIREPS = 9 Max.num. of irreducible representations to be combined
N_EQ = 384 Max.num. of user-supplied symmetry operators/propagation vectors
NGL = 300 Max.num. of global parameters/diffraction pattern
N_LINC = 30 Max.num. of global linear restraints
NAT_P = 64 Max.num. of atomic parameters per atom
NCONST = 500 Max.num. of slack constraints per phase
N_SPE = 16 Max.num. of different chemical species
N_FORM = 60 Max.num. of scattering factor values in a table
NPR = 150 Max.num. of points defining a numerical profile
INPR = 25 Max.num. of different numerical peak shapes
NPRC = 150 Max.num. of terms in the table for correcting intensities
NSOL = 10 Max.num. of solutions to be stored in Montecarlo searches

CPU Time: 6.645 seconds

0.111 minutes

=> Run finished at: Date: 18/02/2015 Time: 13:16:33.614

A.4 Sample of n-RDX processed with 0.1 wt% of PEG

```
*****
** PROGRAM FullProf.2k (Version 5.60 - Jan2015-ILL JRC) **
*****
```

```
M U L T I -- P A T T E R N
Rietveld, Profile Matching & Integrated Intensity
Refinement of X-ray and/or Neutron Data
```

Date: 06/07/2015 Time: 15:52:37.093

=> PCR file code: rpg4std2e

=> DAT file code: rpg4std2e.dat -> Relative contribution: 1.0000

==> CONDITIONS OF THIS RUN FOR PATTERN No.: 1

=> Global Refinement of X-ray powder diffraction data

=> Global Refinement of X-ray powder diffraction data

Flat plate with PSD

=> Title:RDX

=> Number of phases: 1

=> Number of excluded regions: 1

=> Number of scattering factors supplied: 0

=> March-Dollase model for preferred orientation

=> Conventional weights: w=1.0/Variance(yobs)

=> Asymmetry correction as in J.Appl.Cryst. 26,128(1993)

=> Background refined by polynomial function

=> The 7th default profile function was selected

=> T-C-H Pseudo-Voigt function

This function is convoluted with asymmetry due to axial

divergence as formulated by:

van Laar and Yelon, J. Appl. Cryst. 17, 47(1984).

and using the method of:

Finger, Cox and Jephcoat, J. Appl. Cryst. 27, 892 (1994).

Fortran 90 module adapted from function PROFVAL (in F77) :

L.W. Finger, J. Appl. Cryst. 31, 111 (1998).

==> INPUT/OUTPUT OPTIONS:

=> Generate file *.PRF for plot

=> Output Integrated Intensities

=> Generate new input file *.PCR

=> Data supplied in free format for pattern: 1

=> Plot pattern at each cycle

=> Wavelengths: 1.54056 1.54439

=> Alpha2/Alpha1 ratio: 0.5000

=> Cos(Monochromator angle)= 1.0000

=> Asymmetry correction for angles lower than 90.000 degrees

=> Absorption correction (AC), muR-eff = 0.0000 0.0000

=> Base of peaks: 2.0*HW* 20.00

=> Number of cycles: 50

=> Relaxation factors ==> for coordinates: 1.00

=> for anisotropic temperature factors: 1.00

=> for halfwidth/strain/size parameters: 1.00

=> for lattice constants and propagation vectors: 1.00

=> EPS-value for convergence: 0.0

=> Excluded regions for Pattern# 1

From to
39.0000 50.0000

=> Instrumental Resolution read from file: xray-res.irf

=> Title of data: Approximate resolution function of a conventional X-ray diffractometer CuKalpha1,2

=> The resolution function is IRESOL: 1 for profile function # 7

Input resolution parameters:

U-inst	V-inst	W-inst	X-inst	Y-inst	Z-inst
0.00136	-0.00500	0.00391	0.06389	0.00008	0.00000
0.00136	-0.00500	0.00391	0.06389	0.00008	0.00000

=> Number of Least-Squares parameters varied: 58

=>----->

=>-----> PATTERN number: 1

=>----->

=> Global parameters and codes ==>

=> Zero-point: -0.3162 541.0000

```

=> Background parameters and codes ==>
=> Origin of polynomial at 2theta/TOF/E(KeV): 40.000
0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
0.00 0.00 0.00 0.00 0.00 0.00
=> Displacement peak-shift parameter and code: 0.00 0.00
=> Transparency peak-shift parameter and code: 0.00 0.00

=> Reading Intensity data ==>

==> Angular range, step and number of points:
2Thmin: 12.000000 2Thmax: 39.002102 Step: 0.007400 No. of points: 3650
-----
=> Phase No. 1
rdx
-----
=>-----> Pattern# 1
=> Crystal Structure Refinement
=> Preferred orientation vector: 0.0000 0.0000 1.0000

=>-----> Data for PHASE: 1
=> Number of atoms: 21
=> Number of distance constraints: 0
=> Number of angle constraints: 0

=> Symmetry information on space group: P b c a
-> The multiplicity of the general position is: 8
-> The space group is Centric (-1 at origin)
-> Lattice type P: { 000 }
-> Reduced set of symmetry operators:

No. IT Symmetry symbol Rotation part Associated Translation
1: ( 1) 1 --> ( x, y, z) + { 0.0000 0.0000 0.0000}
2: ( 4) 2 ( x, 0, 0) --> ( x,-y,-z) + { 0.5000 0.5000 0.0000}
3: ( 3) 2 ( 0, y, 0) --> (-x, y,-z) + { 0.0000 0.5000 0.5000}
4: ( 2) 2 ( 0, 0, z) --> (-x,-y, z) + { 0.5000 0.0000 0.5000}

Information on Space Group:
-----
=> Number of Space group: 61
=> Hermann-Mauguin Symbol: P b c a
=> Hall Symbol: -P 2ac 2ab
=> Setting Type: IT (Generated from Hermann-Mauguin symbol)
=> Crystal System: Orthorhombic
=> Laue Class: mmm
=> Point Group: mmm
=> Bravais Lattice: P
=> Lattice Symbol: oP
=> Reduced Number of S.O.: 4
=> General multiplicity: 8
=> Centrosymmetry: Centric (-1 at origin)
=> Generators (exc. -1&L): 2
=> Asymmetric unit: 0.000 <= x <= 0.500
0.000 <= y <= 0.500
0.000 <= z <= 0.500

=> List of S.O. without inversion and lattice centring translations
=> SYMM( 1): x,y,z => SYMM( 2): x+1/2,-y+1/2,-z
=> SYMM( 3): -x,y+1/2,-z+1/2 => SYMM( 4): -x+1/2,-y,z+1/2

=> Initial parameters ==>
Atom Ntyp X Y Z B occ. in fin Spc Mult
B11 B22 B33 B12 B13 B23
O(1) 0 0.57608 0.43936 0.27021 3.70830 1.00000 0 0 0 8
Codes: 71.00000 81.00000 91.00000 0.00000 0.00000
O(2) 0 0.59405 0.22852 0.22899 4.41110 1.00000 0 0 0 8
Codes: 101.00000 111.00000 121.00000 0.00000 0.00000
O(3) 0 0.47165 0.13110 -0.01874 4.98480 1.00000 0 0 0 8
Codes: 131.00000 141.00000 151.00000 0.00000 0.00000
O(4) 0 0.34305 0.25796 -0.11691 4.76640 1.00000 0 0 0 8
Codes: 161.00000 171.00000 181.00000 0.00000 0.00000
O(5) 0 0.31082 0.51151 -0.07935 5.32170 1.00000 0 0 0 8
Codes: 191.00000 201.00000 211.00000 0.00000 0.00000
O(6) 0 0.42897 0.59176 0.05201 5.10850 1.00000 0 0 0 8
Codes: 221.00000 231.00000 241.00000 0.00000 0.00000
N(1) N 0.44550 0.33187 0.17883 2.73980 1.00000 0 0 0 8
Codes: 251.00000 261.00000 271.00000 0.00000 0.00000
N(2) N 0.33005 0.24334 0.05173 2.40240 1.00000 0 0 0 8
Codes: 281.00000 291.00000 301.00000 0.00000 0.00000
N(3) N 0.30372 0.45297 0.07981 2.59240 1.00000 0 0 0 8
Codes: 311.00000 321.00000 331.00000 0.00000 0.00000
N(4) N 0.53997 0.33764 0.23203 2.76530 1.00000 0 0 0 8
Codes: 341.00000 351.00000 361.00000 0.00000 0.00000
N(5) N 0.38995 0.20392 -0.04081 3.09700 1.00000 0 0 0 8
Codes: 371.00000 381.00000 391.00000 0.00000 0.00000
N(6) N 0.35080 0.55348 0.01182 3.43200 1.00000 0 0 0 8
Codes: 401.00000 411.00000 421.00000 0.00000 0.00000
C(1) C 0.34908 0.43663 0.19413 2.89510 1.00000 0 0 0 8

```

```

Codes: 431.00000 441.00000 451.00000 0.00000 0.00000
C(2) C 0.38479 0.21557 0.14692 2.70030 1.00000 0 0 0 8
Codes: 461.00000 471.00000 481.00000 0.00000 0.00000
C(3) C 0.23190 0.33513 0.04874 2.55740 1.00000 0 0 0 8
Codes: 491.00000 501.00000 511.00000 0.00000 0.00000
H(1A) H 0.40289 0.52403 0.20773 5.13220 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(1B) H 0.29071 0.42024 0.23991 4.84270 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(2A) H 0.44331 0.13918 0.14950 4.60580 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(2B) H 0.31742 0.19390 0.20730 4.97430 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(3A) H 0.20936 0.35364 -0.02527 4.50050 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000
H(3B) H 0.17213 0.32091 0.10070 3.92150 1.00000 0 0 0 8
Codes: 0.00000 0.00000 0.00000 0.00000 0.00000

```

=> IT IS ASSUMED THAT THE FIRST GIVEN SITE IS FULLY OCCUPIED
OR THE FIRST AND SECOND ATOMS ARE IN THE SAME SITE WITH TOTAL FULL OCCUPATION
(If this is not the case, change the order of atoms to obtain correct values for the content of the unit cell)
The given occupation factors have been obtained multiplying m/M by 1.0000

```

-> Atom: 0 , Chemical element: O Atomic Mass: 15.9994
-> Atom: 0 , Chemical element: O Atomic Mass: 15.9994
-> Atom: 0 , Chemical element: O Atomic Mass: 15.9994
-> Atom: 0 , Chemical element: O Atomic Mass: 15.9994
-> Atom: 0 , Chemical element: O Atomic Mass: 15.9994
-> Atom: 0 , Chemical element: O Atomic Mass: 15.9994
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080

```

=> The given value of ATZ is 1776.94 the program has calculated: 1776.94

The value of ATZ given in the input PCR file will be used for quantitative analysis

=> The chemical content of the unit cell is:

```

8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 C + 8.0000 C + 8.0000 C + 8.0000 H + 8.0000 H +
8.0000 H + 8.0000 H + 8.0000 H +
8.0000 H

```

=> The normalized site occupation numbers in % are:

```

100.0000 O(1) : 100.0000 O(2) : 100.0000 O(3) : 100.0000 O(4) : 100.0000 O(5) :
100.0000 O(6) : 100.0000 N(1) : 100.0000 N(2) : 100.0000 N(3) : 100.0000 N(4) :
100.0000 N(5) : 100.0000 N(6) : 100.0000 C(1) : 100.0000 C(2) : 100.0000 C(3) :
100.0000 H(1A) : 100.0000 H(1B) : 100.0000 H(2A) : 100.0000 H(2B) : 100.0000 H(3A) :
100.0000 H(3B)

```

=> The density (volumic mass) of the compound is: 1.826 g/cm3

=>-----> PROFILE PARAMETERS FOR PATTERN: 1

```

=> Overall scale factor: 0.766210E-03
=> ETA (p-Voigt) OR M (Pearson VII): 0.0000
=> Overall temperature factor: 0.00000
=> Halfwidth U,V,W: -0.02544 0.00000 0.00000
=> X and Y parameters: 0.0000 0.0000
=> Direct cell parameters: 11.5436 10.6639 13.1261 90.0000 90.0000 90.0000
=> Preferred orientation parameters: 1.0000 0.0000
=> Asymmetry parameters : 0.03402 0.04914 0.00000 0.00000
=> Strain parameters : 0.00000 0.00000 0.00000
=> Size parameters : 0.01022 -0.01068
=> Further shape parameters (S_L and D_L): 0.00000 0.00000
S_L is source width/detector distance
D_L is detector width/detector distance

```

==> CODEWORDS FOR PROFILE PARAMETERS of PATTERN# 1

```

=> Overall scale factor: 521.000
=> ETA (p-Voigt) OR M (Pearson VII): 0.000
=> Overall temperature factor: 0.000
=> Halfwidth U,V,W: 551.000 0.000 0.000
=> X and Y parameters: 0.000 0.000
=> Direct cell parameters: 531.000 561.000 571.000 0.000 0.000 0.000
=> Preferred orientation parameters: 0.000 0.000
=> Asymmetry parameters : 0.000 0.000 0.000 0.000
=> Strain parameters : 0.000 0.000 0.000
=> Size parameters : 581.000 11.000
=> The 18th model for size is used

```

=> Orthorhombic Anisotropic Broadening using Spherical Harmonics up

to 4-th order (Laue class: mmm, SPG:16-74, only lorentzian comp.)
 Ylm's up to 4th order: Y00,Y20,Y22+,Y40,Y42+,Y44+
 RJP - Ref: M. Jarvinen, J. Appl. C. (1993),p.527
 => Coefficients of Spherical Harmonics for anisotropic size
 broadening for an orthorhombic lattice

Y00	Y20	Y22+	Y40	Y42+	Y44+
-0.010678	-0.011090	0.072902	0.116701	-0.093789	0.019010
11.0000	21.0000	31.0000	41.0000	51.0000	61.0000

=> Cell constraints according to Laue symmetry: mmm

Metric information:

=> Direct cell parameters:

a = 11.5436 b = 10.6639 c = 13.1261
 alpha = 90.000 beta = 90.000 gamma = 90.000
 Direct Cell Volume = 1615.8197

=> Reciprocal cell parameters:

a* = 0.086628 b* = 0.093774 c* = 0.076184
 alpha* = 90.000 beta* = 90.000 gamma* = 90.000
 Reciprocal Cell Volume = 0.00061888

=> Direct and Reciprocal Metric Tensors:

GD			GR		
133.2541	0.0000	0.0000	0.007504	0.000000	0.000000
0.0000	113.7185	0.0000	0.000000	0.008794	0.000000
0.0000	0.0000	172.2956	0.000000	0.000000	0.005804

=> Cartesian frame: x // a; y is in the ab-plane; z is x ^ y

Crystal_to_Orthonormal_Matrix			Orthonormal_to_Crystal_Matrix		
Cr_Orth_cel			Orth_Cr_cel		
11.5436	0.0000	0.0000	0.086628	0.000000	0.000000
0.0000	10.6639	0.0000	0.000000	0.093774	0.000000
0.0000	0.0000	13.1261	0.000000	0.000000	0.076184

Busing-Levy B-matrix: Hc=B.H			Inverse of the Busing-Levy B-matrix		
BL_M			BL_Min		
0.086628	0.000000	0.000000	11.5436	0.0000	0.0000
0.000000	0.093774	0.000000	0.0000	10.6639	0.0000
0.000000	0.000000	0.076184	0.0000	0.0000	13.1261

=> Laue symmetry mmm will be used to generate HKL for pattern# 1
 => Reflections generated between S(1/d)min: 0.1354 A-1 and S(1/d)max: 0.4753 A-1
 => dmax: 7.3874 A and dmin: 2.1038 A
 => The number of reflections generated is: 91
 => The max. scatt. variable (gen.ref.) is: 42.9553
 => Scattering coefficients from internal table

=> X-ray scattering coeff. (A1, B1, A2,...C, f(0), Z, Dfp,Dfpp)

O	3.0485	13.2771	2.2868	5.7011	1.5463	0.3239	0.8670	32.9089	0.2508	7.9994	8.0000	0.0470	↙
	0.0320												
N	12.2126	0.0057	3.1322	9.8933	2.0125	28.9975	1.1663	0.5826	-11.5290	6.9946	7.0000	0.0290	↙
	0.0180												
C	2.3100	20.8439	1.0200	10.2075	1.5886	0.5687	0.8650	51.6512	0.2156	5.9992	6.0000	0.0170	↙
	0.0090												
H	0.4930	10.5109	0.3229	26.1257	0.1402	3.1424	0.0408	57.7997	0.0030	1.0000	1.0000	0.0000	↙
	0.0000												

 SYMBOLIC NAMES AND INITIAL VALUES OF PARAMETERS TO BE VARIED:

-> Parameter number	1	-> Symbolic Name:	L-Size_ph1_pat1	-0.10678000E-01
-> Parameter number	2	-> Symbolic Name:	Size2_ph1_pat1	-0.11090000E-01
-> Parameter number	3	-> Symbolic Name:	Size3_ph1_pat1	0.72902001E-01
-> Parameter number	4	-> Symbolic Name:	Size4_ph1_pat1	0.11670100
-> Parameter number	5	-> Symbolic Name:	Size5_ph1_pat1	-0.93788996E-01
-> Parameter number	6	-> Symbolic Name:	Size6_ph1_pat1	0.19010000E-01
-> Parameter number	7	-> Symbolic Name:	X_0(1)_ph1	0.57608002
-> Parameter number	8	-> Symbolic Name:	Y_0(1)_ph1	0.43935999
-> Parameter number	9	-> Symbolic Name:	Z_0(1)_ph1	0.27021000
-> Parameter number	10	-> Symbolic Name:	X_0(2)_ph1	0.59404999
-> Parameter number	11	-> Symbolic Name:	Y_0(2)_ph1	0.22852001
-> Parameter number	12	-> Symbolic Name:	Z_0(2)_ph1	0.22899000
-> Parameter number	13	-> Symbolic Name:	X_0(3)_ph1	0.47165000
-> Parameter number	14	-> Symbolic Name:	Y_0(3)_ph1	0.13110000
-> Parameter number	15	-> Symbolic Name:	Z_0(3)_ph1	-0.18740000E-01
-> Parameter number	16	-> Symbolic Name:	X_0(4)_ph1	0.34305000
-> Parameter number	17	-> Symbolic Name:	Y_0(4)_ph1	0.25795999
-> Parameter number	18	-> Symbolic Name:	Z_0(4)_ph1	-0.11691000
-> Parameter number	19	-> Symbolic Name:	X_0(5)_ph1	0.31082001
-> Parameter number	20	-> Symbolic Name:	Y_0(5)_ph1	0.51151001

```

-> Parameter number 21 -> Symbolic Name: Z_0(5)_ph1 -0.79350002E-01
-> Parameter number 22 -> Symbolic Name: X_0(6)_ph1 0.42897001
-> Parameter number 23 -> Symbolic Name: Y_0(6)_ph1 0.59175998
-> Parameter number 24 -> Symbolic Name: Z_0(6)_ph1 0.52010000E-01
-> Parameter number 25 -> Symbolic Name: X_N(1)_ph1 0.44549999
-> Parameter number 26 -> Symbolic Name: Y_N(1)_ph1 0.33186999
-> Parameter number 27 -> Symbolic Name: Z_N(1)_ph1 0.17883000
-> Parameter number 28 -> Symbolic Name: X_N(2)_ph1 0.33004999
-> Parameter number 29 -> Symbolic Name: Y_N(2)_ph1 0.24334000
-> Parameter number 30 -> Symbolic Name: Z_N(2)_ph1 0.51729999E-01
-> Parameter number 31 -> Symbolic Name: X_N(3)_ph1 0.30372000
-> Parameter number 32 -> Symbolic Name: Y_N(3)_ph1 0.45297000
-> Parameter number 33 -> Symbolic Name: Z_N(3)_ph1 0.79810001E-01
-> Parameter number 34 -> Symbolic Name: X_N(4)_ph1 0.53996998
-> Parameter number 35 -> Symbolic Name: Y_N(4)_ph1 0.33763999
-> Parameter number 36 -> Symbolic Name: Z_N(4)_ph1 0.23203000
-> Parameter number 37 -> Symbolic Name: X_N(5)_ph1 0.38995001
-> Parameter number 38 -> Symbolic Name: Y_N(5)_ph1 0.20392001
-> Parameter number 39 -> Symbolic Name: Z_N(5)_ph1 -0.40810000E-01
-> Parameter number 40 -> Symbolic Name: X_N(6)_ph1 0.35080001
-> Parameter number 41 -> Symbolic Name: Y_N(6)_ph1 0.55348003
-> Parameter number 42 -> Symbolic Name: Z_N(6)_ph1 0.11820000E-01
-> Parameter number 43 -> Symbolic Name: X_C(1)_ph1 0.34908000
-> Parameter number 44 -> Symbolic Name: Y_C(1)_ph1 0.43663001
-> Parameter number 45 -> Symbolic Name: Z_C(1)_ph1 0.19413000
-> Parameter number 46 -> Symbolic Name: X_C(2)_ph1 0.38479000
-> Parameter number 47 -> Symbolic Name: Y_C(2)_ph1 0.21557000
-> Parameter number 48 -> Symbolic Name: Z_C(2)_ph1 0.14692000
-> Parameter number 49 -> Symbolic Name: X_C(3)_ph1 0.23190001
-> Parameter number 50 -> Symbolic Name: Y_C(3)_ph1 0.33513001
-> Parameter number 51 -> Symbolic Name: Z_C(3)_ph1 0.48740000E-01
-> Parameter number 52 -> Symbolic Name: Scale_ph1_pat1 0.76621003E-03
-> Parameter number 53 -> Symbolic Name: Cell_A_ph1_pat1 11.543573
-> Parameter number 54 -> Symbolic Name: Zero_pat1 -0.31615999
-> Parameter number 55 -> Symbolic Name: U-Cagl_ph1_pat1 -0.25444999E-01
-> Parameter number 56 -> Symbolic Name: Cell_B_ph1_pat1 10.663886
-> Parameter number 57 -> Symbolic Name: Cell_C_ph1_pat1 13.126143
-> Parameter number 58 -> Symbolic Name: G-Size_ph1_pat1 0.10217000E-01

=> Zero counts at step no. 1 at 2theta/TOF/E(KeV): 12.0000 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 3 at 2theta/TOF/E(KeV): 12.0148 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 4 at 2theta/TOF/E(KeV): 12.0222 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 9 at 2theta/TOF/E(KeV): 12.0592 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 10 at 2theta/TOF/E(KeV): 12.0666 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 15 at 2theta/TOF/E(KeV): 12.1036 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 20 at 2theta/TOF/E(KeV): 12.1406 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 25 at 2theta/TOF/E(KeV): 12.1776 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 29 at 2theta/TOF/E(KeV): 12.2072 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 32 at 2theta/TOF/E(KeV): 12.2294 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 36 at 2theta/TOF/E(KeV): 12.2590 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 39 at 2theta/TOF/E(KeV): 12.2812 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 41 at 2theta/TOF/E(KeV): 12.2960 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 48 at 2theta/TOF/E(KeV): 12.3478 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 49 at 2theta/TOF/E(KeV): 12.3552 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 52 at 2theta/TOF/E(KeV): 12.3774 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 53 at 2theta/TOF/E(KeV): 12.3848 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 54 at 2theta/TOF/E(KeV): 12.3922 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 60 at 2theta/TOF/E(KeV): 12.4366 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 67 at 2theta/TOF/E(KeV): 12.4884 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 79 at 2theta/TOF/E(KeV): 12.5772 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 81 at 2theta/TOF/E(KeV): 12.5920 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 182 at 2theta/TOF/E(KeV): 13.3394 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 192 at 2theta/TOF/E(KeV): 13.4134 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 193 at 2theta/TOF/E(KeV): 13.4208 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 194 at 2theta/TOF/E(KeV): 13.4282 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 199 at 2theta/TOF/E(KeV): 13.4652 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 203 at 2theta/TOF/E(KeV): 13.4948 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 205 at 2theta/TOF/E(KeV): 13.5096 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 208 at 2theta/TOF/E(KeV): 13.5318 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 210 at 2theta/TOF/E(KeV): 13.5466 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 211 at 2theta/TOF/E(KeV): 13.5540 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 214 at 2theta/TOF/E(KeV): 13.5762 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 215 at 2theta/TOF/E(KeV): 13.5836 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 217 at 2theta/TOF/E(KeV): 13.5984 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 219 at 2theta/TOF/E(KeV): 13.6132 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 221 at 2theta/TOF/E(KeV): 13.6280 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 224 at 2theta/TOF/E(KeV): 13.6502 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 226 at 2theta/TOF/E(KeV): 13.6650 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 230 at 2theta/TOF/E(KeV): 13.6946 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 233 at 2theta/TOF/E(KeV): 13.7168 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 235 at 2theta/TOF/E(KeV): 13.7316 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 237 at 2theta/TOF/E(KeV): 13.7464 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 239 at 2theta/TOF/E(KeV): 13.7612 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 241 at 2theta/TOF/E(KeV): 13.7760 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 246 at 2theta/TOF/E(KeV): 13.8130 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 247 at 2theta/TOF/E(KeV): 13.8204 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 248 at 2theta/TOF/E(KeV): 13.8278 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 250 at 2theta/TOF/E(KeV): 13.8426 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 254 at 2theta/TOF/E(KeV): 13.8722 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 263 at 2theta/TOF/E(KeV): 13.9388 Intensity fixed to 1.0 and variance to 1E6

```


N(3)	0.30317-0.00024	0.00212	0.45272-0.00105	0.00286	0.07823-0.00117	0.00295	2.59240	0.00000	0.00000	↙			
	1.00000	0.00000	0.00000										
N(4)	0.54016	0.00004	0.00120	0.33696-0.00050	0.00200	0.23162-0.00032	0.00145	2.76530	0.00000	0.00000	↙		
	1.00000	0.00000	0.00000										
N(5)	0.38838	0.00000	0.00167	0.20531	0.00023	0.00223	-0.03977-0.00035	0.00168	3.09700	0.00000	0.00000	↙	
	1.00000	0.00000	0.00000										
N(6)	0.35084-0.00040	0.00174	0.55483	0.00053	0.00274	0.01185	0.00034	0.00170	3.43200	0.00000	0.00000	↙	
	1.00000	0.00000	0.00000										
C(1)	0.34746-0.00103	0.00277	0.43892	0.00117	0.00301	0.19352-0.00048	0.00175	2.89510	0.00000	0.00000	↙		
	1.00000	0.00000	0.00000										
C(2)	0.38532	0.00068	0.00240	0.21724	0.00058	0.00218	0.14879	0.00076	0.00247	2.70030	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										
C(3)	0.23213-0.00011	0.00129	0.33451-0.00112	0.00396	0.04931	0.00009	0.00116	2.55740	0.00000	0.00000	↙		
	1.00000	0.00000	0.00000										
H(1A)	0.40289	0.00000	0.00000	0.52403	0.00000	0.00000	0.20773	0.00000	0.00000	5.13220	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										
H(1B)	0.29071	0.00000	0.00000	0.42024	0.00000	0.00000	0.23991	0.00000	0.00000	4.84270	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										
H(2A)	0.44331	0.00000	0.00000	0.13918	0.00000	0.00000	0.14950	0.00000	0.00000	4.60580	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										
H(2B)	0.31742	0.00000	0.00000	0.19390	0.00000	0.00000	0.20730	0.00000	0.00000	4.97430	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										
H(3A)	0.20936	0.00000	0.00000	0.35364	0.00000	0.00000	-0.02527	0.00000	0.00000	4.50050	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										
H(3B)	0.17213	0.00000	0.00000	0.32091	0.00000	0.00000	0.10070	0.00000	0.00000	3.92150	0.00000	0.00000	↙
	1.00000	0.00000	0.00000										

==> PROFILE PARAMETERS FOR PATTERN# 1

=> Overall scale factor: 0.000769464 0.000000243 0.000004678
=> Eta(p-Voigt) or m(Pearson VII): 0.000000 0.000000 0.000000
=> Overall tem. factor: 0.000000 0.000000 0.000000
=> Halfwidth parameters:
-0.014575 0.000012 0.004497
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Cell parameters:
11.545714 -0.000002 0.000240
10.665313 0.000007 0.000249
13.129634 0.000005 0.000308
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
=> Preferred orientation:
1.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Asymmetry parameters:
0.034020 0.000000 0.000000
0.049140 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> X and Y parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Strain parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Size parameters (G,L):
0.009228 0.000000 0.000107
0.003242 -0.000001 0.007229
=> Further shape parameters (S_L and D_L):
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> Spherical Harmonics coeff.(size):

0.003242	-0.000001	0.007229	-0.004081	0.000619	0.018743	0.077268	-0.000633	↙
0.014164								
0.118944	-0.000412	0.019819	-0.100242	0.000038	0.018840	0.021744	-0.000283	↙
0.015851								
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	↙
0.000000								

==> GLOBAL PARAMETERS FOR PATTERN# 1

=> Zero-point: -0.3110 0.0000 0.0008
=> Background Polynomial Parameters ==>
0.0000 0.0000 0.0000
0.0000 0.0000 0.0000
0.0000 0.0000 0.0000
0.0000 0.0000 0.0000
0.0000 0.0000 0.0000
0.0000 0.0000 0.0000

=> Cos(theta)-shift parameter : 0.0000 0.0000 0.0000
=> Sin(2theta)-shift parameter : 0.0000 0.0000 0.0000

==> RELIABILITY FACTORS WITH ALL NON-EXCLUDED POINTS FOR PATTERN: 1

=> R-Factors: 10.4 19.9 Chi2: 54.7 DW-Stat.: 1.0389 Patt#: 1
=> Expected : 2.69 1.9295
=> Deviance : 0.399E+06 Dev*: 110.6
=> GoF-index: 7.3 Sqrt(Residual/N)
=> N-P+C: 3591

SumYdif	SumYobs	SumYcal	SumYobsSQ	Residual	Condition
0.5173E+06	0.4951E+07	0.4772E+07	0.4950E+07	0.1964E+06	0.1010E+12

=> Conventional Rietveld Rp,Rwp,Re and Chi2: 10.4 19.9 2.69 54.70
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2): 0.4951E+07 0.4950E+07

=> N-sigma of the GoF: 2275.477

==> RELIABILITY FACTORS FOR POINTS WITH BRAGG CONTRIBUTIONS FOR PATTERN: 1

=> R-Factors: 10.4 19.9 Chi2: 54.7 DW-Stat.: 1.0389 Patt#: 1
=> Expected : 2.69 1.9295
=> Deviance : 0.399E+06 Dev*: 110.6
=> GoF-index: 7.3 Sqrt(Residual/N)
=> N-P+C: 3591

SumYdif	SumYobs	SumYcal	SumYobsSQ	Residual	Condition
0.5173E+06	0.4951E+07	0.4772E+07	0.4950E+07	0.1964E+06	0.1010E+12

=> Conventional Rietveld Rp,Rwp,Re and Chi2: 10.4 19.9 2.69 54.70
=> (Values obtained using Ynet, but true sigma(y))
=> SumYnet, Sum(w Ynet**2): 0.4951E+07 0.4950E+07

=> N-sigma of the GoF: 2275.477

=> Global user-weighted Chi2 (Bragg contrib.): 54.7

Pattern# 1 Phase No: 1 Phase name: rdx

No.	Code	H	K	L	Mult	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	✓
		d-hkl			CORR									
1	1	1	1	1	8	0.114452	13.149	1589.6	1602.9	21.583	0.111843	0.004870	0.057273	✓
		6.727660			598.186646									
2	1	0	0	2	2	0.119441	13.477	824.1	867.7	51.675	0.111766	0.014306	0.156956	✓
		6.564814			142.231522									
3	1	2	0	0	2	0.123020	15.336	83.2	89.4	18.485	0.111321	0.021631	0.226040	✓
		5.772858			109.342499									
4	1	1	0	2	4	0.114272	15.514	798.1	806.3	20.784	0.111278	0.005590	0.065698	✓
		5.706813			213.551315									
5	1	0	2	0	2	0.113511	16.610	494.6	543.5	54.025	0.111009	0.004669	0.055388	✓
		5.332653			92.888382									
6	1	2	1	0	4	0.119996	17.454	1405.2	1455.1	55.354	0.110799	0.017099	0.185281	✓
		5.076861			167.828903									
7	1	1	1	2	8	0.115043	17.611	162.0	179.2	19.069	0.110759	0.008003	0.092754	✓
		5.031765			329.485962									
8	1	0	2	1	4	0.114453	17.939	2073.1	2054.6	31.008	0.110677	0.007053	0.082398	✓
		4.940690			158.650269									
9	1	2	1	1	8	0.117198	18.724	12.8	23.0	21.357	0.110476	0.012541	0.140843	✓
		4.735196			290.503296									
10	1	1	2	1	8	0.114644	19.527	4.5	14.6	34.928	0.110269	0.008173	0.094998	✓
		4.542274			266.421509									
11	1	2	0	2	4	0.113556	20.470	1507.5	1482.5	44.012	0.110022	0.006601	0.077816	✓
		4.335131			120.817383									
12	1	0	2	2	4	0.116199	21.450	105.7	112.1	14.984	0.109761	0.012015	0.136269	✓
		4.139135			109.650375									
13	1	2	1	2	8	0.114268	22.116	1162.9	1165.7	21.433	0.109582	0.008755	0.101909	✓
		4.016045			205.785873									
14	1	2	2	0	4	0.116848	22.681	200.5	215.5	18.496	0.109427	0.013833	0.155209	✓
		3.917146			97.626900									
15	1	1	2	2	8	0.115385	22.804	41.2	45.3	4.926	0.109394	0.011185	0.128038	✓
		3.896320			193.053589									
16	1	1	1	3	8	0.116703	23.261	31.0	36.9	11.121	0.109267	0.013861	0.155696	✓
		3.820774			185.192505									
17	1	2	2	1	8	0.116079	23.683	210.4	220.4	20.453	0.109151	0.012923	0.146323	✓
		3.753652			178.385330									
18	1	3	1	1	8	0.119871	25.503	1454.2	1625.5	191.625	0.108635	0.020784	0.223082	✓
		3.489869			152.700531									
19	1	0	2	3	4	0.117643	26.322	102.7	126.9	29.776	0.108398	0.017178	0.189639	✓
		3.383067			71.417328									
20	1	2	2	2	8	0.115046	26.475	49.4	50.2	0.898	0.108353	0.012487	0.142785	✓
		3.363830			141.100296									
21	1	3	0	2	4	0.116247	26.830	68.0	75.7	8.631	0.108249	0.014896	0.167437	✓
		3.320104			68.585548									
22	1	2	1	3	8	0.114080	26.874	193.6	207.1	14.468	0.108236	0.010911	0.126383	✓
		3.314857			136.697861									
23	1	1	3	1	8	0.114507	27.086	766.4	803.5	38.882	0.108174	0.011820	0.136049	✓
		3.289326			134.458557									


```

67  1  4  1  3  8  0.115489  38.262  323.4  335.6  13.735  0.104508  0.020305  0.226021  ↗
    2.350333  63.689579
68  1  2  1  5  8  0.116062  38.568  7.4  9.7  5.100  0.104396  0.021530  0.237695  ↗
    2.332401  62.572159
69  1  1  2  5  8  0.118256  38.988  1.9  5.1  10.965  0.104242  0.025683  0.275304  ↗
    2.308236  61.089981

```

BRAGG R-Factors and weight fractions for Pattern # 1

```

=> Phase: 1      rdx
=> Bragg R-factor: 4.39      Vol: 1616.766( 0.063)  Fract(%): 100.00( 0.86)
=> Rf-factor= 3.29      ATZ: 1776.939  Brindley: 1.0000

```

SYMBOLIC NAMES AND FINAL VALUES AND SIGMA OF REFINED PARAMETERS:

```

-> Parameter number 1 :      L-Size_ph1_pat1  0.32420373E-02( +/-  0.72292127E-02 )
-> Parameter number 2 :      Size2_ph1_pat1  -0.40812818E-02( +/-  0.18743467E-01 )
-> Parameter number 3 :      Size3_ph1_pat1  0.77267610E-01( +/-  0.14163993E-01 )
-> Parameter number 4 :      Size4_ph1_pat1  0.11894368  ( +/-  0.19819405E-01 )
-> Parameter number 5 :      Size5_ph1_pat1  -0.10024197  ( +/-  0.18839633E-01 )
-> Parameter number 6 :      Size6_ph1_pat1  0.21744350E-01( +/-  0.15851058E-01 )
-> Parameter number 7 :      X_0(1)_ph1  0.57541239  ( +/-  0.11092700E-02 )
-> Parameter number 8 :      Y_0(1)_ph1  0.43966007  ( +/-  0.12116111E-02 )
-> Parameter number 9 :      Z_0(1)_ph1  0.27099708  ( +/-  0.11624396E-02 )
-> Parameter number 10 :     X_0(2)_ph1  0.59412211  ( +/-  0.10898095E-02 )
-> Parameter number 11 :     Y_0(2)_ph1  0.22895293  ( +/-  0.12537022E-02 )
-> Parameter number 12 :     Z_0(2)_ph1  0.22888340  ( +/-  0.11001484E-02 )
-> Parameter number 13 :     X_0(3)_ph1  0.47338510  ( +/-  0.12744585E-02 )
-> Parameter number 14 :     Y_0(3)_ph1  0.13057353  ( +/-  0.92790980E-03 )
-> Parameter number 15 :     Z_0(3)_ph1  -0.19450795E-01( +/-  0.10155203E-02 )
-> Parameter number 16 :     X_0(4)_ph1  0.34381583  ( +/-  0.14120982E-02 )
-> Parameter number 17 :     Y_0(4)_ph1  0.25728008  ( +/-  0.12697025E-02 )
-> Parameter number 18 :     Z_0(4)_ph1  -0.11679447  ( +/-  0.15248761E-02 )
-> Parameter number 19 :     X_0(5)_ph1  0.31070611  ( +/-  0.94801566E-03 )
-> Parameter number 20 :     Y_0(5)_ph1  0.51081645  ( +/-  0.12307854E-02 )
-> Parameter number 21 :     Z_0(5)_ph1  -0.79970337E-01( +/-  0.10943528E-02 )
-> Parameter number 22 :     X_0(6)_ph1  0.42943338  ( +/-  0.13071131E-02 )
-> Parameter number 23 :     Y_0(6)_ph1  0.59145427  ( +/-  0.18751499E-02 )
-> Parameter number 24 :     Z_0(6)_ph1  0.52474596E-01( +/-  0.96871122E-03 )
-> Parameter number 25 :     X_N(1)_ph1  0.44482139  ( +/-  0.17220172E-02 )
-> Parameter number 26 :     Y_N(1)_ph1  0.33536911  ( +/-  0.43182792E-02 )
-> Parameter number 27 :     Z_N(1)_ph1  0.17979442  ( +/-  0.17772377E-02 )
-> Parameter number 28 :     X_N(2)_ph1  0.33223259  ( +/-  0.32609324E-02 )
-> Parameter number 29 :     Y_N(2)_ph1  0.24144928  ( +/-  0.34579535E-02 )
-> Parameter number 30 :     Z_N(2)_ph1  0.51606905E-01( +/-  0.23675738E-02 )
-> Parameter number 31 :     X_N(3)_ph1  0.30316588  ( +/-  0.21229470E-02 )
-> Parameter number 32 :     Y_N(3)_ph1  0.45272210  ( +/-  0.28552911E-02 )
-> Parameter number 33 :     Z_N(3)_ph1  0.78225881E-01( +/-  0.29536241E-02 )
-> Parameter number 34 :     X_N(4)_ph1  0.54015791  ( +/-  0.11990828E-02 )
-> Parameter number 35 :     Y_N(4)_ph1  0.33695599  ( +/-  0.19951391E-02 )
-> Parameter number 36 :     Z_N(4)_ph1  0.23162104  ( +/-  0.14471047E-02 )
-> Parameter number 37 :     X_N(5)_ph1  0.38837519  ( +/-  0.16739216E-02 )
-> Parameter number 38 :     Y_N(5)_ph1  0.20530595  ( +/-  0.22275527E-02 )
-> Parameter number 39 :     Z_N(5)_ph1  -0.39772190E-01( +/-  0.16845398E-02 )
-> Parameter number 40 :     X_N(6)_ph1  0.35083801  ( +/-  0.17355493E-02 )
-> Parameter number 41 :     Y_N(6)_ph1  0.55482548  ( +/-  0.27362476E-02 )
-> Parameter number 42 :     Z_N(6)_ph1  0.11853519E-01( +/-  0.16991830E-02 )
-> Parameter number 43 :     X_C(1)_ph1  0.34745705  ( +/-  0.27718858E-02 )
-> Parameter number 44 :     Y_C(1)_ph1  0.43892241  ( +/-  0.30111372E-02 )
-> Parameter number 45 :     Z_C(1)_ph1  0.19351751  ( +/-  0.17470347E-02 )
-> Parameter number 46 :     X_C(2)_ph1  0.38531837  ( +/-  0.24003256E-02 )
-> Parameter number 47 :     Y_C(2)_ph1  0.21723603  ( +/-  0.21812750E-02 )
-> Parameter number 48 :     Z_C(2)_ph1  0.14879125  ( +/-  0.24698584E-02 )
-> Parameter number 49 :     X_C(3)_ph1  0.23212539  ( +/-  0.12938807E-02 )
-> Parameter number 50 :     Y_C(3)_ph1  0.33450860  ( +/-  0.39550792E-02 )
-> Parameter number 51 :     Z_C(3)_ph1  0.49307033E-01( +/-  0.11598649E-02 )
-> Parameter number 52 :     Scale_ph1_pat1  0.76946447E-03( +/-  0.46780219E-05 )
-> Parameter number 53 :     Cell_A_ph1_pat1  11.545714  ( +/-  0.23961758E-03 )
-> Parameter number 54 :     Zero_pat1  -0.31102592  ( +/-  0.82943856E-03 )
-> Parameter number 55 :     U-Cagl_ph1_pat1  -0.14575286E-01( +/-  0.44974512E-02 )
-> Parameter number 56 :     Cell_B_ph1_pat1  10.665313  ( +/-  0.24886982E-03 )
-> Parameter number 57 :     Cell_C_ph1_pat1  13.129634  ( +/-  0.30849580E-03 )
-> Parameter number 58 :     G-Size_ph1_pat1  0.92282938E-02( +/-  0.10682658E-03 )

```

=> Number of bytes for floating point variables: 4
=> Dimensions of dynamic allocated arrays in this run of FullProf:

=> Total approximate array memory (dynamic + static): 107719993 bytes

```

MaxPOINT= 60000 Max.num. of points(+int. Inten.)/diffraction pattern
MaxREFLT= 20000 Max.num. of reflections/diffraction pattern
MaxPARAM= 300 Max.num. of refinable parameters
MaxOVERL= 2096 Max.num. of overlapping reflections

```

```

-----
=> Number of bytes for floating point arrays: 4
=> Dimensions of fixed arrays in this release of FullProf:
-----

NPATT   =      80 Max.num. of powder diffraction patterns
NATS    =     830 Max.num. of atoms (all kind) in asymmetric unit
MPAR    =    1800 Max.num. of non atomic parameters/phase
LEXCL   =      30 Max.num. of excluded regions
IBACP   =     277 Max.num. of background points for interpolation
NPHT    =      16 Max.num. of phases
NMAGM   =       8 Max.num. of rotation-matrices sets for magnetic structure
NBASIS  =      12 Max.num. of basis functions associated to a single atom
NIREPS  =       9 Max.num. of irreducible representations to be combined
N_EQ    =     384 Max.num. of user-supplied symmetry operators/propagation vectors
NGL     =     300 Max.num. of global parameters/diffraction pattern
N_LINC  =      30 Max.num. of global linear restraints
NAT_P   =      64 Max.num. of atomic parameters per atom
NCONST  =     500 Max.num. of slack constraints per phase
N_SPE   =      16 Max.num. of different chemical species
N_FORM  =      60 Max.num. of scattering factor values in a table
NPR     =     150 Max.num. of points defining a numerical profile
INPR    =      25 Max.num. of different numerical peak shapes
NPRC    =     150 Max.num. of terms in the table for correcting intensities
NSOL    =      10 Max.num. of solutions to be stored in Montecarlo searches

CPU Time:   26.688 seconds
0.445 minutes

=> Run finished at:   Date: 06/07/2015   Time: 15:53:03.785

```

A.5 Sample of n-RDX processed with 10 wt% of PVP

```

*****
** PROGRAM FullProf.2k (Version 5.60 - Jan2015-ILL JRC) **
*****
M U L T I  -- P A T T E R N
Rietveld, Profile Matching & Integrated Intensity
Refinement of X-ray and/or Neutron Data

Date: 15/06/2015   Time: 14:26:29.403

=> PCR file code: rpvv102a
=> DAT file code: rpvv102a.dat           -> Relative contribution: 1.0000

==> CONDITIONS OF THIS RUN FOR PATTERN No.: 1

=> Global Refinement of X-ray powder diffraction data
=> Global Refinement of X-ray powder diffraction data
Flat plate with PSD
=> Title:RDX

=> Number of phases:      1
=> Number of excluded regions:      1
=> Number of scattering factors supplied:      0
=> March-Dollase model for preferred orientation
=> Conventional weights: w=1.0/Variance(yobs)
=> Asymmetry correction as in J.Appl.Cryst. 26,128(1993)
=> Background refined by polynomial function
=> The 5th default profile function was selected
=> Pseudo-Voigt function (ETA variable)
X-parameter correspond to: ETA=ETA0+X*2theta
pV(x)= ETA*L(x)+(1-ETA)*G(x)

==> INPUT/OUTPUT OPTIONS:

=> Generate file *.PRF for plot
=> Output Integrated Intensities
=> Generate new input file *.PCR

=> Data supplied in free format for pattern: 1
=> Plot pattern at each cycle
=> Wavelengths: 1.54056 1.54439
=> Alpha2/Alpha1 ratio: 0.5000
=> Cos(Monochromator angle)= 1.0000
=> Asymmetry correction for angles lower than 90.000 degrees
=> Absorption correction (AC), muR-eff = 0.0000 0.0000
=> Base of peaks: 2.0*HW* 20.00

=> Number of cycles: 10
=> Relaxation factors ==> for coordinates: 1.00
=> for anisotropic temperature factors: 1.00
=> for halfwidth/strain/size parameters: 1.00
=> for lattice constants and propagation vectors: 1.00

```



```

=> EPS-value for convergence:    0.0

=> Excluded regions for Pattern#  1
From      to
39.0000   50.0000

=> Instrumental Resolution read from file: xray-res.irf
=> Title of data: Approximate resolution function of a conventional X-ray diffractometer CuKalpha1,2

=> The resolution function is IRESOL:  1 for profile function #  5
Input resolution parameters:

U-inst    V-inst    W-inst    X-inst    Y-inst    Z-inst
0.00136   -0.00500   0.00391   0.06389   0.00008   0.00000
0.00136   -0.00500   0.00391   0.06389   0.00008   0.00000

=> Number of Least-Squares parameters varied:    10

=>----->
=>-----> PATTERN number:  1
=>----->
=> Global parameters and codes ==>
=> Zero-point:    -0.2646    0.0000
=> Background parameters and codes ==>
=> Origin of polynomial at 2theta/TOF/E(KeV):    40.000
499.36     17910.     54941.     47295.     0.0000     0.0000
101.00     91.00        81.00        71.00        0.00        0.00
=> Displacement peak-shift parameter and code:    0.00    0.00
=> Transparency peak-shift parameter and code:    0.00    0.00

=> Reading Intensity data  =>>

==> Angular range, step and number of points:
2Thmin:    12.000000  2Thmax:    43.012600  Step:    0.012900  No. of points:    2405
-----
=> Phase No.  1
rdx
-----
=>-----> Pattern#  1
=> Crystal Structure Refinement
=> The 7th profile function was selected for phase no.  1
=> Preferred orientation vector:    0.0000  0.0000  1.0000

=>-----> Data for PHASE:  1
=> Number of atoms:    21
=> Number of distance constraints:    0
=> Number of angle constraints:    0

=> Symmetry information on space group: P b c a
-> The multiplicity of the general position is:  8
-> The space group is Centric (-1 at origin)
-> Lattice type P: { 000 }
-> Reduced set of symmetry operators:

No.  IT  Symmetry symbol  Rotation part  Associated Translation
1: ( 1)  1  --> ( x, y, z) + { 0.0000  0.0000  0.0000}
2: ( 4)  2  ( x, 0, 0) --> ( x,-y,-z) + { 0.5000  0.5000  0.0000}
3: ( 3)  2  ( 0, y, 0) --> (-x, y,-z) + { 0.0000  0.5000  0.5000}
4: ( 2)  2  ( 0, 0, z) --> (-x,-y, z) + { 0.5000  0.0000  0.5000}

Information on Space Group:
-----
=> Number of Space group:  61
=> Hermann-Mauguin Symbol: P b c a
=> Hall Symbol: -P 2ac 2ab
=> Table Setting Choice:
=> Setting Type: IT (Generated from Hermann-Mauguin symbol)
=> Crystal System: Orthorhombic
=> Laue Class: mmm
=> Point Group: mmm
=> Bravais Lattice: P
=> Lattice Symbol: oP
=> Reduced Number of S.O.:  4
=> General multiplicity:  8
=> Centrosymmetry: Centric (-1 at origin)
=> Generators (exc. -1&L):  2
=> Asymmetric unit:  0.000 <= x <=  0.500
0.000 <= y <=  0.500
0.000 <= z <=  0.500

=> List of S.O. without inversion and lattice centring translations
=> SYMM(  1): x,y,z => SYMM(  2): x+1/2,-y+1/2,-z
=> SYMM(  3): -x,y+1/2,-z+1/2 => SYMM(  4): -x+1/2,-y,z+1/2

=> Initial parameters ==>
Atom  Ntyp  X  Y  Z  B  occ.  in  fin  Spc  Mult
B11  B22  B33  B12  B13  B23

```

O(1)	O	0.56112	0.44709	0.27123	3.70830	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
O(2)	O	0.58940	0.23581	0.22281	4.41110	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
O(3)	O	0.46916	0.14686	-0.03710	4.98480	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
O(4)	O	0.34711	0.25153	-0.11162	4.76640	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
O(5)	O	0.32210	0.52051	-0.08441	5.32170	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
O(6)	O	0.43381	0.59954	0.04827	5.10850	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
N(1)	N	0.44160	0.33969	0.18271	2.73980	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
N(2)	N	0.33383	0.24622	0.06392	2.40240	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
N(3)	N	0.30468	0.46123	0.06171	2.59240	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
N(4)	N	0.54554	0.33062	0.23341	2.76530	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
N(5)	N	0.38005	0.19333	-0.02755	3.09700	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
N(6)	N	0.35044	0.55394	0.00906	3.43200	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
C(1)	C	0.33877	0.43604	0.17023	2.89510	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
C(2)	C	0.38264	0.20846	0.14721	2.70030	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
C(3)	C	0.23896	0.33552	0.05796	2.55740	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
H(1A)	H	0.40289	0.52403	0.20773	5.13220	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
H(1B)	H	0.29071	0.42024	0.23991	4.84270	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
H(2A)	H	0.44331	0.13918	0.14950	4.60580	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
H(2B)	H	0.31742	0.19390	0.20730	4.97430	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
H(3A)	H	0.20936	0.35364	-0.02527	4.50050	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					
H(3B)	H	0.17213	0.32091	0.10070	3.92150	1.00000	0	0	0	8
Codes:	0.00000	0.00000	0.00000	0.00000	0.00000					

=> IT IS ASSUMED THAT THE FIRST GIVEN SITE IS FULLY OCCUPIED
OR THE FIRST AND SECOND ATOMS ARE IN THE SAME SITE WITH TOTAL FULL OCCUPATION
(If this is not the case, change the order of atoms to obtain correct values for the content of the unit cell)

The given occupation factors have been obtained multiplying m/M by 1.0000

```

-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: O , Chemical element: O Atomic Mass: 15.9994
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080

```

=> The given value of ATZ is 1776.94 the program has calculated: 1776.94

The value of ATZ given in the input PCR file will be used for quantitative analysis

=> The chemical content of the unit cell is:

```

8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 N + 8.0000 C + 8.0000 C + 8.0000 C + 8.0000 H + 8.0000 H +
8.0000 H + 8.0000 H + 8.0000 H +
8.0000 H

```

=> The normalized site occupation numbers in % are:

```

100.0000 O(1) : 100.0000 O(2) : 100.0000 O(3) : 100.0000 O(4) : 100.0000 O(5) :
100.0000 O(6) : 100.0000 N(1) : 100.0000 N(2) : 100.0000 N(3) : 100.0000 N(4) :
100.0000 N(5) : 100.0000 N(6) : 100.0000 C(1) : 100.0000 C(2) : 100.0000 C(3) :
100.0000 H(1A) : 100.0000 H(1B) : 100.0000 H(2A) : 100.0000 H(2B) : 100.0000 H(3A) :
100.0000 H(3B)

```

=> The density (volumic mass) of the compound is: 1.806 g/cm3

=>-----> PROFILE PARAMETERS FOR PATTERN: 1

=> Overall scale factor: 0.380410E-03

=> ETA (p-Voigt) OR M (Pearson VII): 0.0000

=> Overall temperature factor: 0.00000

=> Halfwidth U,V,W: 0.03415 0.00000 0.00000

```

=> X and Y parameters:      0.0000      0.0000
=> Direct cell parameters:  11.5898  10.7002  13.1733  90.0000  90.0000  90.0000
=> Preferred orientation parameters:  1.0000  0.0000
=> Asymmetry parameters    :      0.08378      0.04153      0.00000      0.00000
=> Strain parameters       :      0.00000      0.00000      0.00000
=> Size parameters        :      0.01062      0.00000
=> Further shape parameters (S_L and D_L):  0.00000  0.00000
S_L is source width/detector distance
D_L is detector width/detector distance

==> CODEWORDS FOR PROFILE PARAMETERS of PATTERN# 1

=> Overall scale factor:      0.000
=> ETA (p-Voigt) OR M (Pearson VII):  0.000
=> Overall temperature factor:  0.000
=> Halfwidth U,V,W:      0.000  0.000  0.000
=> X and Y parameters:      0.000  0.000
=> Direct cell parameters:  0.000  0.000  0.000  0.000  0.000  0.000  0.000
=> Preferred orientation parameters:  0.000  0.000
=> Asymmetry parameters    :      0.000  0.000  0.000  0.000
=> Strain parameters       :      0.000  0.000  0.000
=> Size parameters        :      0.000  11.000
=> The 18th model for size is used

=> Orthorhombic Anisotropic Broadening using Spherical Harmonics up
to 4-th order (Laue class: mmm, SPG:16-74, only lorentzian comp.)
Ylm's up to 4th order: Y00,Y20,Y22+,Y40,Y42+,Y44+
RJP - Ref: M. Jarvinen, J. Appl. C. (1993),p.527
=> Coefficients of Spherical Harmonics for anisotropic size
broadening for an orthorhombic lattice
Y00      Y20      Y22+      Y40      Y42+      Y44+
0.000000  0.000000  0.000000  0.000000  0.000000  0.000000
11.0000  21.0000  31.0000  41.0000  51.0000  61.0000

=> Cell constraints according to Laue symmetry: mmm

Metric information:
-----

=> Direct cell parameters:

a =      11.5898      b =      10.7002      c =      13.1733
alpha =      90.000      beta =      90.000      gamma =      90.000
Direct Cell Volume =      1633.6707

=> Reciprocal cell parameters:

a**=      0.086283      b**=      0.093456      c**=      0.075911
alpha**=      90.000      beta**=      90.000      gamma**=      90.000
Reciprocal Cell Volume =      0.00061212

=> Direct and Reciprocal Metric Tensors:

GD                                  GR
134.3239      0.0000      0.0000      0.007445      0.000000      0.000000
0.0000      114.4947      0.0000      0.000000      0.008734      0.000000
0.0000      0.0000      173.5363      0.000000      0.000000      0.005762

=> Cartesian frame: x // a; y is in the ab-plane; z is x ^ y

Crystal_to_Orthonormal_Matrix      Orthonormal_to_Crystal Matrix
Cr_Orth_cel                          Orth_Cr_cel
11.5898      0.0000      0.0000      0.086283      0.000000      0.000000
0.0000      10.7002      0.0000      0.000000      0.093456      0.000000
0.0000      0.0000      13.1733      0.000000      0.000000      0.075911

Busing-Levy B-matrix: Hc=B.H          Inverse of the Busing-Levy B-matrix
BL_M                                    BL_Minv
0.086283      0.000000      0.000000      11.5898      0.0000      0.0000
0.000000      0.093456      0.000000      0.0000      10.7002      0.0000
0.000000      0.000000      0.075911      0.0000      0.0000      13.1733

=> Laue symmetry mmm will be used to generate HKL for pattern# 1
=> Reflections generated between S(1/d)min: 0.1354 A-1 and S(1/d)max: 0.5222 A-1
=>                                     dmax: 7.3874 A and dmin: 1.9150 A
=> The number of reflections generated is: 120
=> The max. scatt. variable (gen.ref.) is: 47.4372
=> Scattering coefficients from internal table

=> X-ray scattering coeff. (A1, B1, A2,...C, f(0), Z, Dfp,Dfpp)

O      3.0485  13.2771  2.2868  5.7011  1.5463  0.3239  0.8670  32.9089  0.2508  7.9994  8.0000  0.0470  ↵
0.0320
N      12.2126  0.0057  3.1322  9.8933  2.0125  28.9975  1.1663  0.5826 -11.5290  6.9946  7.0000  0.0290  ↵
0.0180
C      2.3100  20.8439  1.0200  10.2075  1.5886  0.5687  0.8650  51.6512  0.2156  5.9992  6.0000  0.0170  ↵
0.0090
H      0.4930  10.5109  0.3229  26.1257  0.1402  3.1424  0.0408  57.7997  0.0030  1.0000  1.0000  0.0000  ↵
0.0000

```



```

=> Zero counts at step no. 1679 at 2theta/TOF/E(KeV): 33.6462 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1682 at 2theta/TOF/E(KeV): 33.6849 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1683 at 2theta/TOF/E(KeV): 33.6978 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1687 at 2theta/TOF/E(KeV): 33.7494 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1688 at 2theta/TOF/E(KeV): 33.7623 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1715 at 2theta/TOF/E(KeV): 34.1106 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1723 at 2theta/TOF/E(KeV): 34.2138 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1725 at 2theta/TOF/E(KeV): 34.2396 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1727 at 2theta/TOF/E(KeV): 34.2654 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1806 at 2theta/TOF/E(KeV): 35.2845 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1809 at 2theta/TOF/E(KeV): 35.3232 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1855 at 2theta/TOF/E(KeV): 35.9682 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1857 at 2theta/TOF/E(KeV): 35.9424 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1858 at 2theta/TOF/E(KeV): 35.9553 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1859 at 2theta/TOF/E(KeV): 35.9682 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1861 at 2theta/TOF/E(KeV): 35.9940 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1865 at 2theta/TOF/E(KeV): 36.0456 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1866 at 2theta/TOF/E(KeV): 36.0585 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1867 at 2theta/TOF/E(KeV): 36.0714 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1868 at 2theta/TOF/E(KeV): 36.0843 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1880 at 2theta/TOF/E(KeV): 36.2391 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1883 at 2theta/TOF/E(KeV): 36.2778 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1942 at 2theta/TOF/E(KeV): 37.0389 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1948 at 2theta/TOF/E(KeV): 37.1163 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2025 at 2theta/TOF/E(KeV): 38.1096 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2031 at 2theta/TOF/E(KeV): 38.1870 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2055 at 2theta/TOF/E(KeV): 38.4966 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2060 at 2theta/TOF/E(KeV): 38.5611 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2061 at 2theta/TOF/E(KeV): 38.5740 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2067 at 2theta/TOF/E(KeV): 38.6514 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2069 at 2theta/TOF/E(KeV): 38.6772 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2071 at 2theta/TOF/E(KeV): 38.7030 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2072 at 2theta/TOF/E(KeV): 38.7159 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2086 at 2theta/TOF/E(KeV): 38.8965 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2093 at 2theta/TOF/E(KeV): 38.9868 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2141 at 2theta/TOF/E(KeV): 39.6060 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2312 at 2theta/TOF/E(KeV): 41.8119 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2313 at 2theta/TOF/E(KeV): 41.8248 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2317 at 2theta/TOF/E(KeV): 41.8764 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2363 at 2theta/TOF/E(KeV): 42.4698 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2374 at 2theta/TOF/E(KeV): 42.6117 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2377 at 2theta/TOF/E(KeV): 42.6504 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2378 at 2theta/TOF/E(KeV): 42.6633 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2380 at 2theta/TOF/E(KeV): 42.6891 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2382 at 2theta/TOF/E(KeV): 42.7149 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2383 at 2theta/TOF/E(KeV): 42.7278 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2386 at 2theta/TOF/E(KeV): 42.7665 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2394 at 2theta/TOF/E(KeV): 42.8697 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2395 at 2theta/TOF/E(KeV): 42.8826 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2398 at 2theta/TOF/E(KeV): 42.9213 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2399 at 2theta/TOF/E(KeV): 42.9342 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2400 at 2theta/TOF/E(KeV): 42.9471 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2403 at 2theta/TOF/E(KeV): 42.9858 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2404 at 2theta/TOF/E(KeV): 42.9987 Intensity fixed to 1.0 and variance to 1E6

=> Optimizations for routine tasks applied:
=> Calculation mode for patter#: 1 CM_PSEUDO_VOIGT

```

Standard deviations have to be multiplied by: 2.6583
(correlated residuals) See references:
-J.F.Berar & P.Lelann, J. Appl. Cryst. 24, 1-5 (1991)
-J.F.Berar, Acc. in Pow. Diff. II, NIST Sp.Pub. 846, 63(1992)

```

+++++
=> CYCLE No.: 10
-----
=> Phase 1 Name: rdx
-----
=> New parameters, shifts, and standard deviations

Atom      x      dx      sx      y      dy      sy      z      dz      sz      B      dB      sB      occ.
      docc.  socc.
0(1)      0.56112 0.00000 0.00000 0.44709 0.00000 0.00000 0.27123 0.00000 0.00000 3.70830 0.00000 0.00000
1.00000 0.00000 0.00000
0(2)      0.58940 0.00000 0.00000 0.23581 0.00000 0.00000 0.22281 0.00000 0.00000 4.41110 0.00000 0.00000
1.00000 0.00000 0.00000
0(3)      0.46916 0.00000 0.00000 0.14686 0.00000 0.00000 -0.03710 0.00000 0.00000 4.98480 0.00000 0.00000
1.00000 0.00000 0.00000
0(4)      0.34711 0.00000 0.00000 0.25153 0.00000 0.00000 -0.11162 0.00000 0.00000 4.76640 0.00000 0.00000
1.00000 0.00000 0.00000
0(5)      0.32210 0.00000 0.00000 0.52051 0.00000 0.00000 -0.08441 0.00000 0.00000 5.32170 0.00000 0.00000
1.00000 0.00000 0.00000
0(6)      0.43381 0.00000 0.00000 0.59954 0.00000 0.00000 0.04827 0.00000 0.00000 5.10850 0.00000 0.00000
1.00000 0.00000 0.00000
N(1)      0.44160 0.00000 0.00000 0.33969 0.00000 0.00000 0.18271 0.00000 0.00000 2.73980 0.00000 0.00000

```

```

1.00000 0.00000 0.00000
N(2) 0.33383 0.00000 0.00000 0.24622 0.00000 0.00000 0.06392 0.00000 0.00000 2.40240 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(3) 0.30468 0.00000 0.00000 0.46123 0.00000 0.00000 0.06171 0.00000 0.00000 2.59240 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(4) 0.54554 0.00000 0.00000 0.33062 0.00000 0.00000 0.23341 0.00000 0.00000 2.76530 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(5) 0.38005 0.00000 0.00000 0.19333 0.00000 0.00000 -0.02755 0.00000 0.00000 3.09700 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
N(6) 0.35044 0.00000 0.00000 0.55394 0.00000 0.00000 0.00906 0.00000 0.00000 3.43200 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
C(1) 0.33877 0.00000 0.00000 0.43604 0.00000 0.00000 0.17023 0.00000 0.00000 2.89510 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
C(2) 0.38264 0.00000 0.00000 0.20846 0.00000 0.00000 0.14721 0.00000 0.00000 2.70030 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
C(3) 0.23896 0.00000 0.00000 0.33552 0.00000 0.00000 0.05796 0.00000 0.00000 2.55740 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(1A) 0.40289 0.00000 0.00000 0.52403 0.00000 0.00000 0.20773 0.00000 0.00000 5.13220 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(1B) 0.29071 0.00000 0.00000 0.42024 0.00000 0.00000 0.23991 0.00000 0.00000 4.84270 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(2A) 0.44331 0.00000 0.00000 0.13918 0.00000 0.00000 0.14950 0.00000 0.00000 4.60580 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(2B) 0.31742 0.00000 0.00000 0.19390 0.00000 0.00000 0.20730 0.00000 0.00000 4.97430 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(3A) 0.20936 0.00000 0.00000 0.35364 0.00000 0.00000 -0.02527 0.00000 0.00000 4.50050 0.00000 0.00000 ↵
1.00000 0.00000 0.00000
H(3B) 0.17213 0.00000 0.00000 0.32091 0.00000 0.00000 0.10070 0.00000 0.00000 3.92150 0.00000 0.00000 ↵
1.00000 0.00000 0.00000

```

==> PROFILE PARAMETERS FOR PATTERN# 1

```

=> Overall scale factor: 0.000380410 0.000000000 0.000000000
=> Eta(p-Voigt) or m(Pearson VII): 0.000000 0.000000 0.000000
=> Overall tem. factor: 0.000000 0.000000 0.000000
=> Halfwidth parameters:
0.034153 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Cell parameters:
11.589819 0.000000 0.000000
10.700219 0.000000 0.000000
13.173317 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
=> Preferred orientation:
1.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Asymmetry parameters:
0.083780 0.000000 0.000000
0.041530 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> X and Y parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Strain parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
=> Size parameters (G,L):
0.010621 0.000000 0.000000
0.047821 -0.000006 0.014780
=> Further shape parameters (S_L and D_L):
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

```

==> Spherical Harmonics coeff.(size):

```

0.047821 -0.000006 0.014780 0.072264 -0.000017 0.040111 0.124992 0.000011 ↵
0.029142
0.079216 0.000001 0.041181 0.006204 0.000018 0.040141 0.011800 0.000014 ↵
0.033870
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 ↵
0.000000

```

==> GLOBAL PARAMETERS FOR PATTERN# 1

```

=> Zero-point: -0.2646 0.0000 0.0000
=> Background Polynomial Parameters ==>
564.83 6.2519 5.4257
20303. 236.60 74.327
64170. 915.43 244.22
55266. 790.96 223.17
0.0000 0.0000 0.0000
0.0000 0.0000 0.0000

```

==> Cos(theta)-shift parameter : 0.0000 0.0000 0.0000

=> Sin(2theta)-shift parameter : 0.0000 0.0000 0.0000

==> RELIABILITY FACTORS WITH ALL NON-EXCLUDED POINTS FOR PATTERN: 1

=> R-Factors: 13.4 25.7 Chi2: 50.6 DW-Stat.: 1.0048 Patt#: 1
 => Expected : 3.62 1.8736
 => Deviance : 0.267E+06 Dev*: 127.5
 => GoF-index: 7.1 Sqrt(Residual/N)
 => N-P+C: 2083

SumYdif	SumYobs	SumYcal	SumYobsSQ	Residual	Condition
0.2129E+06	0.1592E+07	0.1483E+07	0.1592E+07	0.1055E+06	0.1514E+10

=> Conventional Rietveld Rp,Rwp,Re and Chi2: 13.4 25.7 3.62 50.64
 => (Values obtained using Ynet, but true sigma(y))
 => SumYnet, Sum(w Ynet**2): 0.1591E+07 0.1591E+07

=> N-sigma of the GoF: 1602.135

==> RELIABILITY FACTORS FOR POINTS WITH BRAGG CONTRIBUTIONS FOR PATTERN: 1

=> R-Factors: 13.4 25.7 Chi2: 50.6 DW-Stat.: 1.0048 Patt#: 1
 => Expected : 3.62 1.8736
 => Deviance : 0.267E+06 Dev*: 127.5
 => GoF-index: 7.1 Sqrt(Residual/N)
 => N-P+C: 2083

SumYdif	SumYobs	SumYcal	SumYobsSQ	Residual	Condition
0.2129E+06	0.1592E+07	0.1483E+07	0.1592E+07	0.1055E+06	0.1514E+10

=> Conventional Rietveld Rp,Rwp,Re and Chi2: 13.4 25.7 3.62 50.64
 => (Values obtained using Ynet, but true sigma(y))
 => SumYnet, Sum(w Ynet**2): 0.1591E+07 0.1591E+07

=> N-sigma of the GoF: 1602.135

=> Global user-weighted Chi2 (Bragg contrib.): 50.6

 Pattern# 1 Phase No: 1 Phase name: rdx

No.	Code	H d-hkl	K	L	Mult CORR	Hw	2theta	Icalc	Iobs	Sigma	HwG	HwL	ETA	✓
1	1	1	1	1	8	0.124715	13.103	1013.3	1116.2	113.426	0.120686	0.007526	0.080717	✓
		6.751026			602.658569									
2	1	0	0	2	2	0.130916	13.432	528.4	610.7	97.893	0.120755	0.018885	0.187455	✓
		6.586658			143.276764									
3	1	2	0	0	2	0.131142	15.277	63.2	78.4	21.222	0.121203	0.018481	0.183336	✓
		5.794909			110.243629									
4	1	1	0	2	4	0.130005	15.461	474.9	548.8	90.345	0.121253	0.016303	0.164017	✓
		5.726488			215.175110									
5	1	0	2	0	2	0.124560	16.556	297.7	301.5	15.913	0.121573	0.005575	0.060197	✓
		5.350110			93.542114									
6	1	2	1	0	4	0.130248	17.389	772.8	827.6	66.775	0.121841	0.015670	0.157633	✓
		5.095625			169.175110									
7	1	1	1	2	8	0.128551	17.551	93.6	107.6	16.133	0.121895	0.012427	0.127698	✓
		5.048918			331.966187									
8	1	0	2	1	4	0.125093	17.879	1148.7	1154.9	23.940	0.122008	0.005758	0.061881	✓
		4.956901			159.781006									
9	1	2	1	1	8	0.130353	18.655	0.1	2.5	45.038	0.122288	0.015038	0.151414	✓
		4.752470			292.823120									
10	1	1	2	1	8	0.127024	19.461	27.0	43.0	26.403	0.122597	0.008270	0.086942	✓
		4.557557			268.381683									
11	1	2	0	2	4	0.132416	20.395	892.2	1023.0	152.315	0.122981	0.017563	0.173044	✓
		4.350759			121.787003									
12	1	0	2	2	4	0.128230	21.379	55.8	56.5	13.314	0.123413	0.008998	0.093548	✓
		4.152773			110.454323									
13	1	2	1	2	8	0.132372	22.036	630.1	672.0	53.995	0.123719	0.016124	0.159519	✓
		4.030334			207.423492									
14	1	2	2	0	4	0.131499	22.601	109.2	120.0	18.338	0.123991	0.014008	0.140237	✓
		3.930954			98.388397									
15	1	1	2	2	8	0.129797	22.727	6.4	8.7	3.667	0.124054	0.010729	0.109720	✓
		3.909391			194.502167									
16	1	1	1	3	8	0.134321	23.182	0.0	0.0	0.200	0.124282	0.018670	0.180947	✓
		3.833667			186.614227									
17	1	2	2	1	8	0.131987	23.599	108.4	132.1	37.049	0.124498	0.013976	0.139429	✓
		3.766823			179.780441									
18	1	3	1	1	8	0.137002	25.406	750.9	876.6	150.280	0.125491	0.021358	0.201780	✓
		3.502875			153.983307									
19	1	0	2	3	4	0.133939	26.234	8.0	17.3	21.185	0.125979	0.014849	0.145729	✓
		3.394251			71.958969									
20	1	2	2	2	8	0.134201	26.382	2.7	5.2	7.080	0.126068	0.015167	0.148447	✓
		3.375513			142.214142									
21	1	3	0	2	4	0.138195	26.730	6.8	6.7	1.940	0.126281	0.022090	0.206614	✓
		3.332368			69.163780									
22	1	2	1	3	8	0.136993	26.778	111.3	117.4	12.184	0.126311	0.019851	0.188259	✓


```

  2.368560    64.859573
66  1      0    2    5    4  0.149967    38.039    57.6    58.0    1.712  0.135236  0.027209  0.232800  ↗
  2.363609    32.274525
67  1      4    1    3    8  0.150496    38.118    148.1    151.8    6.447  0.135312  0.028018  0.238495  ↗
  2.358914    64.255211
68  1      2    1    5    8  0.151800    38.432    3.0      5.6      7.937  0.135619  0.029797  0.250596  ↗
  2.340343    63.099045
69  1      1    2    5    8  0.150892    38.853    2.1      4.9     15.308  0.136034  0.027441  0.233313  ↗
  2.315939    61.594719

```

 BRAGG R-Factors and weight fractions for Pattern # 1

```

=> Phase: 1      rdx
=> Bragg R-factor: 7.51      Vol: 1633.671( 0.000)  Fract(%): 100.00( 0.00)
=> Rf-factor= 4.81      ATZ: 1776.939  Brindley: 1.0000

```

 SYMBOLIC NAMES AND FINAL VALUES AND SIGMA OF REFINED PARAMETERS:

```

-> Parameter number 1 :      L-Size_ph1_pat1  0.47820579E-01( +/- 0.14780403E-01 )
-> Parameter number 2 :      Size2_ph1_pat1  0.72263569E-01( +/- 0.40111270E-01 )
-> Parameter number 3 :      Size3_ph1_pat1  0.12499154 ( +/- 0.29142125E-01 )
-> Parameter number 4 :      Size4_ph1_pat1  0.79216398E-01( +/- 0.41180771E-01 )
-> Parameter number 5 :      Size5_ph1_pat1  0.62037650E-02( +/- 0.40140565E-01 )
-> Parameter number 6 :      Size6_ph1_pat1  0.11800204E-01( +/- 0.33870187E-01 )
-> Parameter number 7 :      Bck_3_pat1      55265.500 ( +/- 223.17101 )
-> Parameter number 8 :      Bck_2_pat1      64169.578 ( +/- 244.21664 )
-> Parameter number 9 :      Bck_1_pat1      20303.109 ( +/- 74.326691 )
-> Parameter number 10 :     Bck_0_pat1      564.83319 ( +/- 5.4257102 )

```

=> Number of bytes for floating point variables: 4
=> Dimensions of dynamic allocated arrays in this run of FullProf:

=> Total approximate array memory (dynamic + static): 107719993 bytes

```

MaxPOINT= 60000 Max.num. of points(+int. Inten.)/diffraction pattern
MaxREFLT= 20000 Max.num. of reflections/diffraction pattern
MaxPARAM= 300 Max.num. of refinable parameters
MaxOVERL= 2096 Max.num. of overlapping reflections

```

=> Number of bytes for floating point arrays: 4
=> Dimensions of fixed arrays in this release of FullProf:

```

NPATT = 80 Max.num. of powder diffraction patterns
NATS = 830 Max.num. of atoms (all kind) in asymmetric unit
MPAR = 1800 Max.num. of non atomic parameters/phase
IEXCL = 30 Max.num. of excluded regions
IBACP = 277 Max.num. of background points for interpolation
NPHT = 16 Max.num. of phases
NMAGM = 8 Max.num. of rotation-matrices sets for magnetic structure
NBASIS = 12 Max.num. of basis functions associated to a single atom
NIREPS = 9 Max.num. of irreducible representations to be combined
N_EQ = 384 Max.num. of user-supplied symmetry operators/propagation vectors
NGL = 300 Max.num. of global parameters/diffraction pattern
N_LINC = 30 Max.num. of global linear restraints
NAT_P = 64 Max.num. of atomic parameters per atom
NCONST = 500 Max.num. of slack constraints per phase
N_SPE = 16 Max.num. of different chemical species
N_FORM = 60 Max.num. of scattering factor values in a table
NPR = 150 Max.num. of points defining a numerical profile
INPR = 25 Max.num. of different numerical peak shapes
NPRC = 150 Max.num. of terms in the table for correcting intensities
NSOL = 10 Max.num. of solutions to be stored in Montecarlo searches

```

```

CPU Time: 6.805 seconds
0.113 minutes

```

=> Run finished at: Date: 15/06/2015 Time: 14:26:36.221

A.6 Sample of n-RDX with 1 wt% of PVP through a 80 micron nozzle

```

*****
** PROGRAM FullProf.2k (Version 5.50 - Dec2014-ILL JRC) **
*****
M U L T I  -- P A T T E R N
Rietveld, Profile Matching & Integrated Intensity
Refinement of X-ray and/or Neutron Data

```

Date: 20/02/2015 Time: 16:02:20.266

=> PCR file code: rvpv1_80_2a_woB_stillKa2_fullprof
=> DAT file code: rvpv1_80_2a_woB_stil -> Relative contribution: 1.0000

==> CONDITIONS OF THIS RUN FOR PATTERN No.: 1

=> Global Refinement of X-ray powder diffraction data
=> Global Refinement of X-ray powder diffraction data
Flat plate with PSD
=> Title:RDX

=> Number of phases: 1
=> Number of excluded regions: 0
=> Number of scattering factors supplied: 0
=> March-Dollase model for preferred orientation
=> Conventional weights: w=1.0/Variance(yobs)
=> Asymmetry correction as in J.Appl.Cryst. 26,128(1993)
=> Background linearly interpolated between the 2 points given
=> The 5th default profile function was selected
=> Pseudo-Voigt function (ETA variable)
X-parameter correspond to: ETA=ETA0+X*2theta
pV(x)= ETA*L(x)+(1-ETA)*G(x)

==> INPUT/OUTPUT OPTIONS:

=> Generate file *.PRF for plot
=> Output Integrated Intensities
=> Generate new input file *.PCR

=> Data supplied in free format for pattern: 1
=> Plot pattern at each cycle
=> Wavelengths: 1.54056 1.54439
=> Alpha2/Alpha1 ratio: 0.5000
=> Cos(Monochromator angle)= 1.0000
=> Asymmetry correction for angles lower than 90.000 degrees
=> Absorption correction (AC), muR-eff = 0.0000 0.0000
=> Base of peaks: 2.0*HW* 20.00

=> Number of cycles: 50
=> Relaxation factors ==> for coordinates: 1.00
=> for anisotropic temperature factors: 1.00
=> for halfwidth/strain/size parameters: 1.00
=> for lattice constants and propagation vectors: 1.00
=> EPS-value for convergence: 0.0
=> Instrumental Resolution read from file: xray-res.irf
=> Title of data: Approximate resolution function of a conventional X-ray diffractometer CuKalpha1,2

=> The resolution function is IRESOL: 1 for profile function # 5
Input resolution parameters:

U-inst	V-inst	W-inst	X-inst	Y-inst	Z-inst
0.00136	-0.00500	0.00391	0.06389	0.00008	0.00000
0.00136	-0.00500	0.00391	0.06389	0.00008	0.00000

=> Number of Least-Squares parameters varied: 6

=>----->
=>-----> PATTERN number: 1
=>----->
=> Global parameters and codes ==>
=> Zero-point: -0.0558 0.0000
=> Displacement peak-shift parameter and code: -0.12 11.00
=> Transparency peak-shift parameter and code: 0.25 31.00

=> Reading Intensity data =>>

==> Angular range, step and number of points:
2Thmin: 12.000000 2Thmax: 38.784801 Step: 0.012900 No. of points: 2077

=> Phase No. 1
rdx

=>-----> Pattern# 1
=> Crystal Structure Refinement
=> The 7th profile function was selected for phase no. 1
=> Preferred orientation vector: 0.0000 0.0000 1.0000

=>-----> Data for PHASE: 1
=> Number of atoms: 21
=> Number of distance constraints: 0
=> Number of angle constraints: 0

=> Symmetry information on space group: P b c a
-> The multiplicity of the general position is: 8
-> The space group is Centric (-1 at origin)
-> Lattice type P: { 000 }
-> Reduced set of symmetry operators:


```

-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: N , Chemical element: N Atomic Mass: 14.0067
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: C , Chemical element: C Atomic Mass: 12.0110
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
-> Atom: H , Chemical element: H Atomic Mass: 1.0080
=> The given value of ATZ is 1776.94 the program has calculated: 1776.94
The value of ATZ given in the input PCR file will be used for quantitative analysis
=> The chemical content of the unit cell is:
8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 O + 8.0000 N +
 8.0000 N + 8.0000 N + 8.0000 N +
8.0000 N + 8.0000 N + 8.0000 C + 8.0000 C + 8.0000 C + 8.0000 H + 8.0000 H +
 8.0000 H + 8.0000 H + 8.0000 H +
8.0000 H
=> The normalized site occupation numbers in % are:
100.0000 O(1) : 100.0000 O(2) : 100.0000 O(3) : 100.0000 O(4) : 100.0000 O(5) :
 100.0000 O(6) : 100.0000 N(1) : 100.0000 N(2) : 100.0000 N(3) : 100.0000 N(4) :
100.0000 N(5) : 100.0000 N(6) : 100.0000 C(1) : 100.0000 C(2) : 100.0000 C(3) :
 100.0000 H(1A) : 100.0000 H(1B) : 100.0000 H(2A) : 100.0000 H(2B) : 100.0000 H(3A) :
100.0000 H(3B)
=> The density (volumic mass) of the compound is: 1.785 g/cm3

=>-----> PROFILE PARAMETERS FOR PATTERN: 1

=> Overall scale factor: 0.484280E-03
=> ETA (p-Voigt) OR M (Pearson VII): 0.0000
=> Overall temperature factor: 0.00000
=> Halfwidth U,V,W: -0.00329 0.00000 0.00000
=> X and Y parameters: 0.0000 0.0000
=> Direct cell parameters: 11.6304 10.7431 13.2279 90.0000 90.0000 90.0000
=> Preferred orientation parameters: 1.0000 0.0000
=> Asymmetry parameters : 0.05091 0.04932 0.00000 0.00000
=> Strain parameters : 0.00000 0.00000 0.00000
=> Size parameters : 0.00901 0.05242
=> Further shape parameters (S_L and D_L): 0.00000 0.00000
S_L is source width/detector distance
D_L is detector width/detector distance

==> CODEWORDS FOR PROFILE PARAMETERS of PATTERN# 1

=> Overall scale factor: 0.000
=> ETA (p-Voigt) OR M (Pearson VII): 0.000
=> Overall temperature factor: 0.000
=> Halfwidth U,V,W: 21.000 0.000 0.000
=> X and Y parameters: 0.000 0.000
=> Direct cell parameters: 0.000 0.000 0.000 0.000 0.000 0.000
=> Preferred orientation parameters: 0.000 0.000
=> Asymmetry parameters : 41.000 61.000 0.000 0.000
=> Strain parameters : 0.000 0.000 0.000
=> Size parameters : 51.000 0.000
=> The 18th model for size is used

=> Orthorhombic Anisotropic Broadening using Spherical Harmonics up
to 4-th order (Laue class: mmm, SPG:16-74, only lorentzian comp.)
Ylm's up to 4th order: Y00,Y20,Y22+,Y40,Y42+,Y44+
RJP - Ref: M. Jarvinen, J. Appl. C. (1993),p.527
=> Coefficients of Spherical Harmonics for anisotropic size
broadening for an orthorhombic lattice
Y00 Y20 Y22+ Y40 Y42+ Y44+
0.052419 0.087274 0.142427 0.127726 -0.069125 -0.017749
0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

=> Cell constraints according to Laue symmetry: mmm

Metric information:
-----

=> Direct cell parameters:

a = 11.6304 b = 10.7431 c = 13.2279
alpha = 90.000 beta = 90.000 gamma = 90.000
Direct Cell Volume = 1652.7814

=> Reciprocal cell parameters:

a*= 0.085981 b*= 0.093083 c*= 0.075598
alpha**= 90.000 beta**= 90.000 gamma**= 90.000
Reciprocal Cell Volume = 0.00060504

=> Direct and Reciprocal Metric Tensors:

```

```

GD                                GR
135.2666      0.0000      0.0000      0.007393      0.000000      0.000000
0.0000      115.4133      0.0000      0.000000      0.008665      0.000000
0.0000      0.0000      174.9783      0.000000      0.000000      0.005715

=> Cartesian frame: x // a; y is in the ab-plane; z is x ^ y

Crystal_to_Orthonormal_Matrix      Orthonormal_to_Crystal Matrix
Cr_Orth_cel                        Orth_Cr_cel
11.6304      0.0000      0.0000      0.085981      0.000000      0.000000
0.0000      10.7431      0.0000      0.000000      0.093083      0.000000
0.0000      0.0000      13.2279      0.000000      0.000000      0.075598

Busing-Levy B-matrix: Hc=B.H      Inverse of the Busing-Levy B-matrix
BL_M                                BL_Minv
0.085981      0.000000      0.000000      11.6304      0.0000      0.0000
0.000000      0.093083      0.000000      0.0000      10.7431      0.0000
0.000000      0.000000      0.075598      0.0000      0.0000      13.2279

=> Laue symmetry mmm will be used to generate HKL for pattern# 1
=> Reflections generated between S(1/d)min: 0.1354 A-1 and S(1/d)max: 0.4718 A-1
=>                                     dmax: 7.3874 A and dmin: 2.1197 A
=> The number of reflections generated is: 91
=> The max. scatt. variable (gen.ref.) is: 42.6163
=> Scattering coefficients from internal table

=> X-ray scattering coeff. (A1, B1, A2,...C, f(0), Z, Dfp,Dfpp)

O      3.0485  13.2771  2.2868  5.7011  1.5463  0.3239  0.8670  32.9089  0.2508  7.9994  8.0000  0.0470  ↵
0.0320
N      12.2126  0.0057  3.1322  9.8933  2.0125  28.9975  1.1663  0.5826 -11.5290  6.9946  7.0000  0.0290  ↵
0.0180
C      2.3100  20.8439  1.0200  10.2075  1.5886  0.5687  0.8650  51.6512  0.2156  5.9992  6.0000  0.0170  ↵
0.0090
H      0.4930  10.5109  0.3229  26.1257  0.1402  3.1424  0.0408  57.7997  0.0030  1.0000  1.0000  0.0000  ↵
0.0000

-----
SYMBOLIC NAMES AND INITIAL VALUES OF PARAMETERS TO BE VARIED:
-----

-> Parameter number 1 -> Symbolic Name: SyCos_pat1 -0.12224000
-> Parameter number 2 -> Symbolic Name: U-Cag1_ph1_pat1 -0.32860001E-02
-> Parameter number 3 -> Symbolic Name: SySin_pat1 0.24594000
-> Parameter number 4 -> Symbolic Name: Asym1_ph1_pat1 0.50910000E-01
-> Parameter number 5 -> Symbolic Name: G-Size_ph1_pat1 0.90079997E-02
-> Parameter number 6 -> Symbolic Name: Asym2_ph1_pat1 0.49320001E-01

=> Zero counts at step no. 1 at 2theta/TOF/E(KeV): 12.0000 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2 at 2theta/TOF/E(KeV): 12.0129 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 5 at 2theta/TOF/E(KeV): 12.0516 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 8 at 2theta/TOF/E(KeV): 12.0903 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 12 at 2theta/TOF/E(KeV): 12.1419 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 13 at 2theta/TOF/E(KeV): 12.1548 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 14 at 2theta/TOF/E(KeV): 12.1677 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 15 at 2theta/TOF/E(KeV): 12.1806 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 16 at 2theta/TOF/E(KeV): 12.1935 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 19 at 2theta/TOF/E(KeV): 12.2322 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 22 at 2theta/TOF/E(KeV): 12.2709 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 28 at 2theta/TOF/E(KeV): 12.3483 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 35 at 2theta/TOF/E(KeV): 12.4386 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 36 at 2theta/TOF/E(KeV): 12.4515 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 37 at 2theta/TOF/E(KeV): 12.4644 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 38 at 2theta/TOF/E(KeV): 12.4773 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 41 at 2theta/TOF/E(KeV): 12.5160 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 119 at 2theta/TOF/E(KeV): 13.5222 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 125 at 2theta/TOF/E(KeV): 13.5996 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 126 at 2theta/TOF/E(KeV): 13.6125 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 127 at 2theta/TOF/E(KeV): 13.6254 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 133 at 2theta/TOF/E(KeV): 13.7028 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 137 at 2theta/TOF/E(KeV): 13.7544 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 139 at 2theta/TOF/E(KeV): 13.7802 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 144 at 2theta/TOF/E(KeV): 13.8447 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 147 at 2theta/TOF/E(KeV): 13.8834 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 150 at 2theta/TOF/E(KeV): 13.9221 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 157 at 2theta/TOF/E(KeV): 14.0124 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 159 at 2theta/TOF/E(KeV): 14.0382 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 161 at 2theta/TOF/E(KeV): 14.0640 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 162 at 2theta/TOF/E(KeV): 14.0769 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 164 at 2theta/TOF/E(KeV): 14.1027 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 169 at 2theta/TOF/E(KeV): 14.1672 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 170 at 2theta/TOF/E(KeV): 14.1801 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 174 at 2theta/TOF/E(KeV): 14.2317 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 177 at 2theta/TOF/E(KeV): 14.2704 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 179 at 2theta/TOF/E(KeV): 14.2962 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 182 at 2theta/TOF/E(KeV): 14.3349 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 187 at 2theta/TOF/E(KeV): 14.3994 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 189 at 2theta/TOF/E(KeV): 14.4252 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 194 at 2theta/TOF/E(KeV): 14.4897 Intensity fixed to 1.0 and variance to 1E6

```



```

=> Zero counts at step no. 1617 at 2theta/TOF/E(KeV): 32.8464 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1621 at 2theta/TOF/E(KeV): 32.8980 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1667 at 2theta/TOF/E(KeV): 33.4914 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1669 at 2theta/TOF/E(KeV): 33.5172 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1671 at 2theta/TOF/E(KeV): 33.5430 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1682 at 2theta/TOF/E(KeV): 33.6849 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1684 at 2theta/TOF/E(KeV): 33.7107 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1687 at 2theta/TOF/E(KeV): 33.7494 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1690 at 2theta/TOF/E(KeV): 33.7881 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1691 at 2theta/TOF/E(KeV): 33.8010 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1693 at 2theta/TOF/E(KeV): 33.8268 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1696 at 2theta/TOF/E(KeV): 33.8655 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1700 at 2theta/TOF/E(KeV): 33.9171 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1724 at 2theta/TOF/E(KeV): 34.2267 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1726 at 2theta/TOF/E(KeV): 34.2525 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1727 at 2theta/TOF/E(KeV): 34.2654 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1731 at 2theta/TOF/E(KeV): 34.3170 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1732 at 2theta/TOF/E(KeV): 34.3299 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1735 at 2theta/TOF/E(KeV): 34.3686 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1738 at 2theta/TOF/E(KeV): 34.4073 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1739 at 2theta/TOF/E(KeV): 34.4202 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1816 at 2theta/TOF/E(KeV): 35.4135 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1818 at 2theta/TOF/E(KeV): 35.4393 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1819 at 2theta/TOF/E(KeV): 35.4522 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1820 at 2theta/TOF/E(KeV): 35.4651 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1856 at 2theta/TOF/E(KeV): 35.9295 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1861 at 2theta/TOF/E(KeV): 35.9940 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1862 at 2theta/TOF/E(KeV): 36.0069 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1870 at 2theta/TOF/E(KeV): 36.1101 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1873 at 2theta/TOF/E(KeV): 36.1488 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1875 at 2theta/TOF/E(KeV): 36.1746 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1878 at 2theta/TOF/E(KeV): 36.2133 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1879 at 2theta/TOF/E(KeV): 36.2262 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1881 at 2theta/TOF/E(KeV): 36.2520 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1883 at 2theta/TOF/E(KeV): 36.2778 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1884 at 2theta/TOF/E(KeV): 36.2907 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1888 at 2theta/TOF/E(KeV): 36.3423 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1947 at 2theta/TOF/E(KeV): 37.1034 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1953 at 2theta/TOF/E(KeV): 37.1808 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1959 at 2theta/TOF/E(KeV): 37.2582 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1962 at 2theta/TOF/E(KeV): 37.2969 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1963 at 2theta/TOF/E(KeV): 37.3098 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 1965 at 2theta/TOF/E(KeV): 37.3356 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2041 at 2theta/TOF/E(KeV): 38.3160 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2042 at 2theta/TOF/E(KeV): 38.3289 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2043 at 2theta/TOF/E(KeV): 38.3418 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2045 at 2theta/TOF/E(KeV): 38.3676 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2047 at 2theta/TOF/E(KeV): 38.3934 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2050 at 2theta/TOF/E(KeV): 38.4321 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2057 at 2theta/TOF/E(KeV): 38.5224 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2059 at 2theta/TOF/E(KeV): 38.5482 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2062 at 2theta/TOF/E(KeV): 38.5869 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2066 at 2theta/TOF/E(KeV): 38.6385 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2068 at 2theta/TOF/E(KeV): 38.6643 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2071 at 2theta/TOF/E(KeV): 38.7030 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2074 at 2theta/TOF/E(KeV): 38.7417 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2075 at 2theta/TOF/E(KeV): 38.7546 Intensity fixed to 1.0 and variance to 1E6
=> Zero counts at step no. 2076 at 2theta/TOF/E(KeV): 38.7675 Intensity fixed to 1.0 and variance to 1E6

```

```

=> Optimizations for routine tasks applied:
=> Calculation mode for patter#: 1 CM_PSEUDO_VOIGT

```

```

Standard deviations have to be multiplied by: 4.9699
(correlated residuals) See references:
-J.F.Berar & P.Lelann, J. Appl. Cryst. 24, 1-5 (1991)
-J.F.Berar, Acc. in Pow. Diff. II, NIST Sp.Pub. 846, 63(1992)

```

```

+++++

```

```

=> CYCLE No.: 17
=> Convergence reached at this CYCLE !!!!
=> Parameter shifts set to zero

```

```

-----
=> Phase 1 Name: rdx
-----

```

```

=> New parameters, shifts, and standard deviations

```

Atom	x	dx	sx	y	dy	sy	z	dz	sz	B	dB	sB	occ.
	docc.	socc.											
0(1)	0.56846	0.00000	0.00000	0.43427	0.00000	0.00000	0.26465	0.00000	0.00000	3.70830	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
0(2)	0.59453	0.00000	0.00000	0.24040	0.00000	0.00000	0.23053	0.00000	0.00000	4.41110	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
0(3)	0.47340	0.00000	0.00000	0.13880	0.00000	0.00000	-0.02250	0.00000	0.00000	4.98480	0.00000	0.00000	✓
	1.00000	0.00000	0.00000										
0(4)	0.35580	0.00000	0.00000	0.24950	0.00000	0.00000	-0.11238	0.00000	0.00000	4.76640	0.00000	0.00000	✓

1.00000	0.00000	0.00000											
O(5)	0.31810	0.00000	0.00000	0.53030	0.00000	0.00000	-0.06806	0.00000	0.00000	5.32170	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
O(6)	0.42860	0.00000	0.00000	0.60110	0.00000	0.00000	0.04920	0.00000	0.00000	5.10850	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
N(1)	0.43638	0.00000	0.00000	0.33385	0.00000	0.00000	0.17584	0.00000	0.00000	2.73980	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
N(2)	0.32231	0.00000	0.00000	0.23197	0.00000	0.00000	0.05389	0.00000	0.00000	2.40240	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
N(3)	0.29900	0.00000	0.00000	0.45348	0.00000	0.00000	0.08838	0.00000	0.00000	2.59240	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
N(4)	0.53777	0.00000	0.00000	0.33516	0.00000	0.00000	0.22628	0.00000	0.00000	2.76530	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
N(5)	0.38834	0.00000	0.00000	0.20759	0.00000	0.00000	-0.03308	0.00000	0.00000	3.09700	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
N(6)	0.35299	0.00000	0.00000	0.52971	0.00000	0.00000	0.01650	0.00000	0.00000	3.43200	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
C(1)	0.35799	0.00000	0.00000	0.43950	0.00000	0.00000	0.18450	0.00000	0.00000	2.89510	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
C(2)	0.38140	0.00000	0.00000	0.21557	0.00000	0.00000	0.14950	0.00000	0.00000	2.70030	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
C(3)	0.24458	0.00000	0.00000	0.33936	0.00000	0.00000	0.05038	0.00000	0.00000	2.55740	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
H(1A)	0.40289	0.00000	0.00000	0.52403	0.00000	0.00000	0.20773	0.00000	0.00000	5.13220	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
H(1B)	0.29071	0.00000	0.00000	0.42024	0.00000	0.00000	0.23991	0.00000	0.00000	4.84270	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
H(2A)	0.44331	0.00000	0.00000	0.13918	0.00000	0.00000	0.14950	0.00000	0.00000	4.60580	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
H(2B)	0.31742	0.00000	0.00000	0.19390	0.00000	0.00000	0.20730	0.00000	0.00000	4.97430	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
H(3A)	0.20936	0.00000	0.00000	0.35364	0.00000	0.00000	-0.02527	0.00000	0.00000	4.50050	0.00000	0.00000	↙
1.00000	0.00000	0.00000											
H(3B)	0.17213	0.00000	0.00000	0.32091	0.00000	0.00000	0.10070	0.00000	0.00000	3.92150	0.00000	0.00000	↙
1.00000	0.00000	0.00000											

==> PROFILE PARAMETERS FOR PATTERN# 1

=> Overall scale factor: 0.000484280 0.000000000 0.000000000
=> Eta(p-Voigt) or m(Pearson VII): 0.000000 0.000000 0.000000
=> Overall tem. factor: 0.000000 0.000000 0.000000

=> Halfwidth parameters:
-0.021873 0.000000 0.008126
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> Cell parameters:
11.630419 0.000000 0.000000
10.743058 0.000000 0.000000
13.227938 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000
90.000000 0.000000 0.000000

=> Preferred orientation:
1.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> Asymmetry parameters:
0.016548 0.000000 0.022682
0.042495 0.000000 0.004085
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> X and Y parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> Strain parameters:
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> Size parameters (G,L):
0.009841 0.000000 0.000166
0.052419 0.000000 0.000000

=> Further shape parameters (S_L and D_L):
0.000000 0.000000 0.000000
0.000000 0.000000 0.000000

=> Spherical Harmonics coeff.(size):

0.052419	0.000000	0.000000	0.087274	0.000000	0.000000	0.142427	0.000000	↙
0.000000								
0.127726	0.000000	0.000000	-0.069125	0.000000	0.000000	-0.017749	0.000000	↙
0.000000								
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	↙
0.000000								

==> GLOBAL PARAMETERS FOR PATTERN# 1

=> Zero-point: -0.0558 0.0000 0.0000

=> Cos(theta)-shift parameter : -0.1317 0.0000 0.0059
=> Sin(2theta)-shift parameter : 0.2589 0.0000 0.0079

66	1	0	2	5	4	0.121164	37.877	50.7	62.8	15.171	0.103817	0.031435	0.324228	↙
						2.373343								
67	1	4	1	3	8	0.117489	37.971	177.6	217.2	49.240	0.103762	0.025174	0.271878	↙
						2.367672								
68	1	2	1	5	8	0.119694	38.272	1.4	3.4	6.285	0.103587	0.029308	0.307508	↙
						2.349785								
69	1	1	2	5	8	0.120194	38.689	1.2	3.3	13.353	0.103342	0.030582	0.318513	↙
						2.325420								

 BRAGG R-Factors and weight fractions for Pattern # 1

=> Phase: 1 rdx
 => Bragg R-factor: 13.0 Vol: 1652.781(0.000) Fract(%): 100.00(0.00)
 => Rf-factor= 7.18 ATZ: 1776.939 Brindley: 1.0000

 SYMBOLIC NAMES AND FINAL VALUES AND SIGMA OF REFINED PARAMETERS:

-> Parameter number	1 :	SyCos_pat1	-0.13173719	(+/-	0.58904295E-02)
-> Parameter number	2 :	U-Cagl_ph1_pat1	-0.21872528E-01	(+/-	0.81257941E-02)
-> Parameter number	3 :	SySin_pat1	0.25886813	(+/-	0.79076700E-02)
-> Parameter number	4 :	Asym1_ph1_pat1	0.16548268E-01	(+/-	0.22681832E-01)
-> Parameter number	5 :	G-Size_ph1_pat1	0.98405704E-02	(+/-	0.16556650E-03)
-> Parameter number	6 :	Asym2_ph1_pat1	0.42495131E-01	(+/-	0.40853349E-02)

 => Number of bytes for floating point variables: 4
 => Dimensions of dynamic allocated arrays in this run of FullProf:

=> Total approximate array memory (dynamic + static): 107719993 bytes

MaxPOINT=	60000	Max.num. of points(+int. Inten.)/diffraction pattern
MaxREFLT=	20000	Max.num. of reflections/diffraction pattern
MaxPARAM=	300	Max.num. of refinable parameters
MaxOVERL=	2096	Max.num. of overlapping reflections

 => Number of bytes for floating point arrays: 4
 => Dimensions of fixed arrays in this release of FullProf:

NPATT =	80	Max.num. of powder diffraction patterns
NATS =	830	Max.num. of atoms (all kind) in asymmetric unit
MPAR =	1800	Max.num. of non atomic parameters/phase
IEXCL =	30	Max.num. of excluded regions
IBACP =	277	Max.num. of background points for interpolation
NPHT =	16	Max.num. of phases
NMAGM =	8	Max.num. of rotation-matrices sets for magnetic structure
NBASIS =	12	Max.num. of basis functions associated to a single atom
NIREPS =	9	Max.num. of irreducible representations to be combined
N_EQ =	384	Max.num. of user-supplied symmetry operators/propagation vectors
NGL =	300	Max.num. of global parameters/diffraction pattern
N_LINC =	30	Max.num. of global linear restraints
NAT_P =	64	Max.num. of atomic parameters per atom
NCONST =	500	Max.num. of slack constraints per phase
N_SPE =	16	Max.num. of different chemical species
N_FORM =	60	Max.num. of scattering factor values in a table
NPR =	150	Max.num. of points defining a numerical profile
INPR =	25	Max.num. of different numerical peak shapes
NPRC =	150	Max.num. of terms in the table for correcting intensities
NSOL =	10	Max.num. of solutions to be stored in Montecarlo searches

CPU Time: 7.385 seconds
 0.123 minutes

=> Run finished at: Date: 20/02/2015 Time: 16:02:27.667

Glossary

- ADN** Ammonium DiNitramide 46
- AFM** Atomic Force Microscopy 4, 40, 66, 67, 97, 99, 102–105, 107, 108, 110, 116, 117, 119, 120, 138, 139, 170, 173, 282, 283, 285
- AN** Ammonium Nitrate 32, 66
- AP** Ammonium Perchlorate 32, 64
- API** Active Pharmaceutical Ingredient 134
- ASES** Aerosol Solvent Extraction System 68, 69, 73
- BAM** Bundesanstalt für Materialprüfung 43–45, 281
- BET** Brunauer–Emmett–Teller theory 40, 52, 95, 96, 103, 285
- CL-20** 2,4,6,8,10,12-hexanitro-2,4,6,8,10,12-hexaazaisowurtzitane 32, 35–38, 46, 47, 49, 54, 55, 62, 65, 70, 71, 138–141, 281, 283
- CL-20:HMX** co-crystal from CL-20 and HMX 36, 38, 65, 71, 130, 137, 139–141, 174, 283
- CNT** Classical Nucleation Theory 125, 141
- CTA** 2,4,6-triazido-1,3,5-triazine or cyanuric triazide 64
- CVD** Chemical Vapor Deposition 72
- DBTDL** Dibutyltin dilaurate 64
- DLS** Dynamic Light Scattering 53, 55, 62, 65, 73, 281, 285
- DMA** Differential Mobility Analysis 96
- DME** DiMethyl Ether 70

- DMF** DiMethylFormamide 33, 34, 63, 68
- DMSO** dimethylsulfoxide 33, 34, 149
- DSC** Differential Scanning Calorimetry 41
- ESD** Electrostatic Discharge 43–45, 47, 163, 281
- ESEM** Environmental Scanning Electron Microscopy 51, 55, 173, 281
- FOX-7** 1,1-diamino-2,2-dinitroethene 46, 62, 71
- FPM** Full Pattern Matching 50, 111
- FTIR** Fourier Transform Infrared Spectroscopy 42, 158, 162, 284
- FWHM** Full Width at Half Maximum 111, 113
- GAP** Glycidyl Azide Polymer 64
- GAS** Gas AntiSolvent 68
- HMX** octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine 32, 34, 36–38, 46–48, 55, 62, 63, 65, 66, 71, 138, 281
- IM** Insensitive Munitions 46
- IR** Infrared 81
- LASER** Light Amplification by Stimulated Emission of Radiation 66, 70, 72, 73, 75, 82, 96, 130
- MD** Molecular Dynamics 125
- MSF** Multi Stage Flash 75, 77
- NC** NitroCellulose 64, 68
- NMP** N-Methyl-2-pyrrolidone 33, 34
- NMR** Nuclear Magnetic Resonance 9, 42, 149, 150, 283
- NRTL** Non-Random Two-Liquid 128
- NTO** 5-nitro-1,2,4-triazol-3-one 68, 173

- ONC** Octanitrocubane 46
- PDA** Phase Doppler Analysis 5, 12, 96, 130–132, 141, 166, 169, 170, 175, 283
- PEG** PolyEthylene Glycol 5, 12, 107, 116, 118, 142, 147–149, 151–158, 160, 162–166, 174, 282, 284, 286
- PGSS** Particles from Gas-Saturated Solutions 69
- PhSD** Phase Solubility Diagram 134, 136, 137, 174
- PID** Proportional-Integral-Derivative 78, 139
- PIV** Particle Image Velocimetry 130
- PSD** Particle Size Distribution 22, 48, 53, 55, 65, 97, 98, 103, 106–108, 128, 129, 132, 133, 138, 153, 157, 160, 281, 283
- PVAc** Polyvinyl acetate 71
- PVD** Physical Vapor Deposition 66, 72, 73, 82
- PVOH** Polyvinyl alcohol 65
- PVP** PolyVinylPyrrolidone 5, 12, 52, 53, 70, 107–110, 116–119, 138, 142, 147–149, 151, 154, 157–165, 174, 281, 282, 284
- RDX** 1,3,5-trinitroperhydro-1,3,5-triazine 4, 11, 12, 31–34, 37, 45–48, 50, 51, 54–56, 61–73, 75, 81, 82, 95, 97–99, 103, 105, 108–110, 117–119, 126–129, 138, 147–150, 152–166, 173, 174, 281–286
- RESS** Rapid Expansion of Supercritical Solutions 47, 69, 70, 73, 82, 173
- RESS-AS** Rapid Expansion of Supercritical Solutions into an Aqueous Solution 70, 74
- RfD** reference dose 54
- SAS** Supercritical Anti-Solvent precipitation 68
- SATP** Standard Ambient Temperature and Pressure as a temperature of 298.15 K and an absolute pressure of 100 kPa (1 bar) 34, 35
- SAXS** Small-Angle X-ray Scattering 141, 166, 170
- SCF** SuperCritical Fluid 74, 75

SDBD Surface Dielectric Barrier Discharge 67

SEDS Solution Enhanced Dispersion by Supercritical fluids 68, 69, 73

SEM Scanning Electron Microscopy 39, 51, 62, 65, 70, 81, 96, 103, 106–110, 116–120, 128, 152–154, 159, 281, 282, 284, 285

SFE Spray Flash Evaporation 4, 46, 48, 72, 73, 75, 78–83, 98, 99, 105, 111, 112, 117, 120, 126–129, 132, 137–141, 147–149, 152–154, 156–159, 162, 163, 166, 173–175, 282–284

SHYMAN Sustainable Hydrothermal Manufacturing of Nanomaterials 72

SMPS Scanning Mobility Particle Sizer 70

SMRT-TEM single-molecule real-time transmission electron microscopy 125

STM Scanning Tunneling Microscopy 4, 173

TDI Toluene Dilsocyanate 64

TEM Transmission Electron Microscopy 120

TERS Tip Enhanced Raman Spectroscopy 164, 166

TIL Threshold Initiation Level 45

TNAZ 1,3,3-trinitroazetidine 46

TNT 2,4,6-trinitrotoluene 4, 11, 13, 64, 67, 69, 72

VLE Vapor-Liquid Equilibrium 127, 128, 283

XRD X-Ray Diffraction 36, 39, 40, 49, 50, 64–66, 73, 99, 111, 120, 138, 140, 153, 155, 158, 161, 170, 281, 283–285

List of Figures

0.1 Schéma du procédé Spray Flash Evaporation (SFE) 15

0.2	Illustration schématique des phénomènes d'évaporation et cristallisation en jeu dans le SFE. La limite de 500 nm correspond à la limite actuelle de détection possible par mesure directe en ligne en anémo-granulométrie Phase Doppler	16
0.3	Distribution en taille des gouttes pulvérisées à 100, 140 et 160 °C.	17
0.4	Régression des profils de distribution en taille des gouttes pulvérisées à 100, 140 et 160 °C.	18
0.5	Analyse Watershed illustrée sur une simulation de sphères de 200 nm.	19
0.6	Effet de la pression, sans micro coupe, 5 µm × 5 µm pour 1024 px × 1024 px, contraste amélioré.	21
0.7	Effet de la pression, avec une micro coupe, 5 µm × 5 µm pour 1024 px × 1024 px, contraste amélioré.	22
0.8	Illustration du principe de cristallisation <i>in situ</i> via multi-buses	24
0.9	Diagramme ternaire d'un cocrystal A :B 1 :1	25
1.1	RDX visual representations. H atoms have been omitted for clarity.	33
1.2	HMX visual representations. H atoms have been omitted for clarity.	34
1.3	CL-20 visual representations. H atoms have been omitted for clarity.	35
1.4	CL-20 polymorphism	36
1.5	CL-20:HMX 2:1 visual representations	38
1.6	Diagram highlighting the information available from the interpretation of an XRD pattern	39
1.7	DSC peak analysis	41
1.8	Apparatuses for testing the mechanical and electric sensitivity at small scale, in use at NS3E.	43
1.9	Sample holder for BAM Fall-Hammer	43
1.10	Schematic principle of the BAM friction sensitivity test.	44
1.11	Schematic principle of the OZM ESD 2008A tester.	45
1.12	Sensitivities of RDX with various PSD	48
1.13	Examples of computer generated XRD patterns, both with the same broadening.	49
1.14	High vacuum SEM imaging on a n-RDX pressed pellet coated with gold.	51
1.15	Comparison between high vacuum SEM imaging and at 2 Torr from ESEM on the same n-RDX sample	51
1.16	All DLS results acquired from n-RDX with 5wt% of PVP: even if this figure contains data with different experimental conditions such as duration of the ultrasonic bath or the dilution, none of the PSD could have been found reliable.	53
2.1	Solubility curves for different substances	62

2.2	Flashing in water liquid jet	76
2.3	Empirical diagram of the evaporation of a water drop	77
2.4	SFE installation as patented and used in this present work	78
2.5	Schematic insight of the nozzle and its heating system; from left to right, rear view, longitudinal cross-section and front view.	79
2.6	System for the product recovery: in orange the cyclonic separator for vacuum and in gray the interchangeable vessel.	80
2.7	Intricacy of the parameters and phenomena involved in the particle crystallisation by the SFE process.	83
3.1	Watershed analysis illustrated on simulated 200 nm spheres.	99
3.2	Parametric study based on the variation of the concentration in solvent.100	100
3.2	Parametric study based on the variation of the concentration in solvent.101	101
3.2	Parametric study based on the variation of the concentration in solvent.102	102
3.3	Effect of the weight; same face, no microtomy, 5 μm \times 5 μm for 1024 px \times 1024 px, enhanced contrast.	106
3.4	Effect of the weight; same face, processed by microtomy, 5 μm \times 5 μm for 1024 px \times 1024 px, enhanced contrast.	107
3.5	SEM imaging of a 97 MPa pellet of RDX processed with 5 wt% of PVP 40000.	109
3.6	SEM and AFM imaging of a 97 MPa pellet of RDX processed with 5 wt% of PVP 40000.	110
3.7	SEM imaging of one hole of a 97 MPa pellet compared to the loose powder of the same sample of RDX processed with 5 wt% of PVP 40000.110	110
3.8	Williamson-Hall of n-RDX processed by SFE at 2 wt% in acetone. . .	112
3.9	Rietveld refinement performed on LaB ₆	114
3.10	Sample of n-RDX processed pure at 2 wt% in acetone.	115
3.11	Sample of n-RDX processed pure at 3 wt% in acetone.	115
3.12	Sample of n-RDX processed with 0.1 wt% of PEG.	116
3.13	Sample of n-RDX processed with 10 wt% PVP.	116
3.14	Sample of n-RDX processed with 1 wt% PVP with a 80 μm nozzle . . .	117
3.15	One of the smallest particle (63x58 nm) observed by SEM on RDX processed with 10 wt% PVP.	118
3.16	n-RDX processed with 10 wt% PVP.	119
4.1	Rate of nucleation against the supersaturation.	125
4.2	Two possible scenarios from the two-step nucleation mechanism: the first one involves an intermediate state at a higher energy due to an unstable dense liquid existing as mesoscopic clusters, and the second lower curve applies if the dense liquid is stable ($\Delta G_{L-L}^0 < 0$)	126

4.3	VLE of the binary system acetone-hexane at 1 bar (solid lines) and 7 mbar (dashed lines): the data at 1 bar are obtained from the Dortmund Data Bank, and curves at 7 mbar are computed from ProSim.	127
4.4	The dual nozzle system.	129
4.5	PSD for RDX processed in the binary system acetone/n-hexane by SFE through one or two nozzles; the legend shows the molar ratio of acetone and in parenthesis the mean diameter in nm.	129
4.6	Principle of the Phase Doppler analysis (PDA) in a glance (Dantec Documentation).	131
4.7	PDA <i>in situ</i> measurements for SFE.	132
4.8	Preliminary measurements from a demonstration apparatus inside the SFE under vacuum while spraying acetone. Acquisitions were performed at two different axial distances from the nozzle orifice: at around 4 mm or quite far at around 1 cm	133
4.9	Particle Size Distribution of droplets of acetone sprayed at 100, 140 and 160 °C.	134
4.10	Peak fitting of the PSD of droplets of acetone sprayed at 100, 140 and 160 °C.	135
4.11	Phase Solubility Diagram (PSD) of a 1:1 AB cocrystal from co-formers A and B; in red the solubility curve of the A crystal, in blue the one of B, and in green the cocrystal. Arrows illustrate a possible crystallisation by addition of B to the solution followed by the cocrystallisation.	136
4.12	Ternary Diagram of a 1:1 AB cocrystal from co formers A and	137
4.13	First dual nozzle system with an orientation at 45°.	138
4.14	Mean Particle Size Distribution of the cocrystal CL-20:HMX 2:1 samples processed by SFE (first batch) and counted from pellets analysed by AFM.	139
4.15	XRD of a sample processed from dual nozzle system compared to CL-20:HMX and to β -CL-20 both from SFE via a single nozzle.	140
4.16	XRD of a sample processed from a solution of CL-20 in ethyl acetate and a solution of HMX in acetone sprayed at the constant stoichiometric ratio 2:1 by monitoring and controlling mass flow rate; the pattern is compared to the sample from the Figure 4.15, CL-20:HMX and to β -CL-20 both from SFE via a single nozzle.	140
5.1	Evaporation and crystallisation phenomena throughout the SFE process. The 500 nm limit displayed is roughly the detection limit for Phase Doppler Particle Analyzers, which allows <i>in situ</i> size and velocity measurements on both liquid and solid particles.	148
5.2	Test of the reliability of quantification by NMR.	150
5.3	NMR-H spectra of various representative samples	151

5.4	Sizes – using a logarithmic scale – of samples processed with PEG measured from SEM micrographs; solid lines represent the smallest lengths and the dotted lines the largest. Pure RDX processed by SFE and raw M5 RDX added here for comparison.	152
5.5	SEM micrographes of RDX samples processed by SFE in the same operating conditions.	154
5.6	(A) XRD patterns of RDX PEG-processed samples; only isolated peaks of major interest have been indexed for clarity. (B) inset of XRD patterns illustrating the broadening of peaks.	155
5.7	View of the 311 plane (in violet, almost perpendicular to the plane of the drawing) and RDX molecules on the surface: both nitro and methylene group are located at the surface (on the background, the unit cell).	155
5.8	DSC analysis of RDX samples processed with different wt% of PEG. .	156
5.9	FTIR spectra of two relevant RDX samples processed with PEG . . .	158
5.10	Particle size distribution and cumulative counts – using a logarithmic scale – of samples processed with PVP measured from SEM micrographs.	159
5.11	Particle size distribution of RDX processed with a 80 µm nozzle at only 20 bar.	160
5.12	DSC analysis of RDX samples processed with different wt% of PVP. .	161
5.13	FTIR spectra of the RDX samples processed with 10 wt% of PVP, compared to raw PVP 40K and pure RDX processed by SFE.	162
5.14	Sensitivities of RDX processed with PVP and PEG compared with pure nano-RDX and the raw micron size RDX.	163
5.15	DSC analysis of RDX samples processed with PVP and PEG: comparison of mechanical mixes with 10 wt% of PVP or PEG.	165
5.16	New model of SFE with a reduced size.	169

List of Tables

0.1	Poids utilisé et pression correspondante calculée : l'effet de levier suit la loi $P = 6 \cdot \frac{M}{A} + 31$ où $A = \frac{\pi}{4} \cdot \varnothing^2$ avec M la masse du poids. . . .	20
0.2	Diamètre moyen en nm selon la pression appliquée et le pré traitement par microtome ; par MEB, la taille moyenne est de 500 nm.	22

1.1	Characteristics of the most common crystalline forms of RDX, HMX, CL-20	37
1.2	Sensitivity towards impact, friction and ESD of micron-sized and nano-structured RDX	47
1.3	Comparison of the sensitivity levels of micro Hexolite with those of a nano-sized Hexolite	47
1.4	Comparison of the sensitivity levels of micro and nano CL-20	47
1.5	BET measurements on n-RDX with Kr	52
2.1	Comparison of the sensitivity levels of conventional and 400-nm large RDX.	67
2.2	Comparison of the sensitivity levels of conventional and 500-nm large RDX	67
2.3	Comparison . ¹ smallest pure RDX mean size reported in nm ² XRD measurement ³ freeze dried from a 64 nmRDX slurry ⁴ from DLS, no report about dried state *Not available in the references, so the value is based on usual operating conditions sCO ₂ : supercritical carbon dioxide	73
3.1	Several apparent densities of pellets pressed at 97 MPa.	97
3.2	One-way analysis of variance on the particle size from AFM pictures.	102
3.3	Tukey's multiple comparison test on the particle size from AFM pictures.	102
3.4	Watershed and threshold method tested on simulated data; the 'trimmed' results mean that the grains at the edge of the picture are removed since they are probably trimmed. The Watershed algorithm add a one pixel boundary at the edges too, so trimmed grains cannot be removed easily.	104
3.5	Weights used and their calculated corresponding pressures: the leverage follows the law $P = 6 \cdot \frac{M}{A} + 31$ where $A = \frac{\pi}{4} \cdot \varnothing^2$ with M the mass of the weight.	105
3.6	Mean Diameters (nm) according to the pressure applied and the pre-treatment by microtomy; by SEM, the mean size is 500 nm.	106
3.7	Particle size from pellet imaging by AFM of some samples at 97 MPa with microtomy.	108
3.8	Instrumental resolution determined from LaB ₆ pattern refinement.	113
3.9	Smallest particle imaged on SEM compared to the computed average apparent size from Rietveld refinement.	118
5.1	Mass percentage of RDX in the final products compared to the initial loading.	149

- 5.2 Melting (endo) and decomposition (exo) temperatures in °C and decomposition energy in J/g for all samples (T_e extrapolated peak onset, T_p peak maximum temperature, T_c extrapolated peak offset). See Material & Methods section for more details. 157
- 5.3 Sensitivities of the RDX processed with PEG, compared with pure nano-RDX and the raw micron size RDX. 163

Toward Particle Size Reduction by Spray Flash Evaporation

the case of organic energetic crystals and cocrystals

Résumé

La cristallisation en continu de nanoparticules énergétiques est un défi de longue date. Le Spray Flash Evaporation (SFE) est une technique majeure développée et brevetée en interne, pour la production en continu de matériaux énergétiques submicroniques ou nanométriques ; la technologie se base sur la surchauffe d'un solvant pulvérisé dans le vide et s'évaporant alors de manière flash.

Ce présent travail de recherche a pour but de comprendre et contrôler la cristallisation au sein du procédé SFE, ceci afin de réduire encore la taille de particules de cristaux énergétiques. Le RDX est choisi comme matériaux de référence ; le cocrystal CL-20:HMX 2:1 a été également étudié pour aller au-delà des limitations de mesures *in-situ*. La sursaturation gouverne la cristallisation, et concernant le SFE, est une fonction du temps et de l'espace liée aux tailles et vitesses de gouttes. La sursaturation fut variée par un anti-solvant et par l'amélioration du SFE avec un système double buse. Finalement, un Interféromètre Phase Doppler fut utilisé pour résoudre cette question de la sursaturation.

Dans un second temps, PVP 40K et PEG 400 ont été utilisés afin de contrôler les deux étapes de la cristallisation, nommément la nucléation et la croissance. Les particules ont pu être ajustées d'une taille de 160 nm à 5 µm, avec des morphologies facettées ou sphériques. De plus, les échantillons de RDX ainsi cristallisés furent aussi moins sensibles, notamment de manière très marquée à la décharge électrostatique.

Mots clés : Spray Flash Evaporation, 1,3,5-trinitroperhydro-1,3,5-triazine, RDX, CL-20, HMX, cristallisation, nanoparticules, particules fines, explosif, cocrystal

Résumé en anglais

The continuous formation of nanosized energetic material is a long-standing challenge. Spray Flash Evaporation (SFE) is a major technique, internally developed and patented, for continuously producing energetic materials at submicron or nano scale; it relies on the superheating of a solvent sprayed into vacuum and thus flashing.

This present research project aims to understand and control the crystallisation occurring in the SFE process, in order to reduce further the particle size of energetic crystals. RDX has been chosen as a reference material; the cocrystal CL-20:HMX 2:1 was studied overcome the limited *in situ* characterizations also. The supersaturation governs the crystallization and is a function of time and space in SFE, linked to the size distribution and velocity of droplets. Supersaturation was raised with an anti-solvent and by the enhancement of the SFE with a dual nozzle system. Later, a Phase Doppler Interferometer was used to elucidate the question of supersaturation.

Another route to control the crystallisation is the addition of chemical agent. PVP 40K and PEG 400 were successfully used to alter the two steps of the crystallisation, namely the nucleation and the growth. The particle was subsequently tuned from 160 nm spheres to 5 µm grains. Additionally, the synthesized RDX samples were less sensitive, especially toward electrostatic discharge.

Keywords: Spray Flash Evaporation, 1,3,5-trinitroperhydro-1,3,5-triazine, RDX, CL-20, HMX, crystallisation, nanoparticles, fine particles, nanoparticles, explosive, cocrystal